Solve for convective film coefficient using: Principles of Heat Transfer by Kreith

$kJ := 1000J$ $mbar := 10^{-3} bar$ $\mu Pa := 10^{-6} Pa$

$T_i := (273.15 - 25)K$ $T_i = 248.15\,K$ $\mu_v := 10.28 \mu Pa \cdot s$ $\mu_{liq} := 267.5 \mu Pa \cdot s$

$c_{liq} := 1019 \frac{J}{kg \cdot K}$ $\rho_{liq} := 1565 \cdot \frac{kg}{m^3}$ $\rho_v := 16.39 \frac{kg}{m^3}$

$k_v := 0.009 \frac{W}{m \cdot K}$ $k_{liq} := 0.053 \frac{W}{m \cdot K}$ $\sigma := .014 \frac{N}{m}$ surface tension at 247K

$h_{liq} := 173.7 \frac{kJ}{kg}$ $h_v := 275.6 \frac{kJ}{kg}$ $\Delta h := h_v - h_{liq}$ $\Delta h = 101.9 \cdot \frac{kJ}{kg}$ $\lambda := \Delta h$

$Q := 240W$ $L1 := 2m$

$x_i := 0.05$ $x_o := 0.85$ $mdot := \frac{Q}{(x_o - x_i) \cdot \lambda}$ $mdot = 2.944 \times 10^{-3} \frac{kg}{s}$

Tube dimensions $t := .012in$ wall thickness

$c_h := 4.9mm - 2 \cdot t$ $c_r := \frac{4.9}{2} mm - t$ $w_c := 2mm$ $A_c := w_c \cdot c_h + \pi \cdot c_r^2$

$P_c := 2 \cdot w_c + 2 \cdot \pi \cdot c_r$ $D_h := 4 \cdot \frac{A_c}{P_c}$ $D_h = 5.272 \cdot mm$ $A_t := A_c$

$G1 := \frac{mdot}{A_t}$ $G1 = 127.791 \frac{kg}{m^2 \cdot s}$

$h_{flux} := \frac{240W}{P_c \cdot L1}$ $h_{flux} = 6.866 \times 10^3 \cdot \frac{W}{m^2}$ $T_{sat} := T_i$ $T_{sat} = 248.15\,K$ fluid saturation temperature

$k_w := 200 \frac{W}{m \cdot K}$ aluminum tube wall for T_{sat} = 238K the saturation pressure is 1.67bar

$P := 1.671bar$ $P = 1.671 \times 10^5 Pa$ $Pr_{liq} := \frac{\mu_{liq} \cdot c_{liq}}{k_{liq}}$ $Pr_{liq} = 5.143$

$\alpha_{liq} := \frac{k_{liq}}{\rho_{liq} \cdot c_{liq}}$ $\alpha_{liq} = 3.323 \times 10^{-8} \frac{m^2}{s}$ thermal diffusivity

Condition for nucleate boiling to occur

$$\Delta T_n := \left(\frac{8 \cdot \sigma \cdot h_{flux} \cdot T_{sat}}{\lambda \cdot \rho_v \cdot k_{liq}} \right)^{0.5}$$ $\Delta T_n = 1.468\,K$ any differential film temp above this

Reference: Kreith really method by Chen

$i := 0..6$

$$x := \begin{pmatrix} .05 \\ .1 \\ .3 \\ .5 \\ .6 \\ .7 \\ .85 \end{pmatrix}$$

this a linear change flow quality along the tube length

$$X_{ttinverse_i} := \left(\frac{x_i}{1 - x_i}\right)^{0.9} \cdot \left(\frac{\rho_{liq}}{\rho_v}\right)^{0.5} \cdot \left(\frac{\mu_v}{\mu_{liq}}\right)^{0.1} \qquad X_{ttinverse} = \begin{pmatrix} 0.498 \\ 0.976 \\ 3.29 \\ 7.054 \\ 10.161 \\ 15.122 \\ 33.607 \end{pmatrix}$$

$$Ftt_i := 2.35 \cdot \left(X_{ttinverse_i} + 0.213\right)^{0.736} \qquad Ftt = \begin{pmatrix} 1.829 \\ 2.67 \\ 5.913 \\ 10.116 \\ 13.146 \\ 17.528 \\ 31.372 \end{pmatrix}$$

convective cooling

$$h_{c_i} := 0.023 \cdot \left[\frac{G1 \cdot \left(1 - x_i\right) \cdot D_h}{\mu_{liq}}\right]^{0.8} \cdot Pr_{liq}^{\ 0.4} \cdot \frac{k_{liq}}{D_h} \cdot Ftt_i \qquad h_c = \begin{pmatrix} 410.986 \\ 574.555 \\ 1040.713 \\ 1360.304 \\ 1478.678 \\ 1566.271 \\ 1610.082 \end{pmatrix} \cdot \frac{W}{m^2 \cdot K}$$

h_c is the cooling from forced convection. The next step is to calculate the cooling from evaporation.

Solving for evaporation requires assuming a temperature difference between the tube wall and the saturation temperature of the fluid. After calculating this contribution we can solve for this temperature difference through the combination of both cooling mechanisms. If the end result agrees with the assumption, the process stops otherwise the process is repeated with a new assumed ΔT_{sat}

$$Re_{TP_i} := \frac{G1 \cdot \left(1 - x_i\right) \cdot D_h}{\mu_{liq}} \cdot \left(Ftt_i\right)^{1.25} \cdot 10^{-4}$$

needed to calculate S_{tt}

$$Re_{TP} = \begin{pmatrix} 0.509 \\ 0.774 \\ 1.626 \\ 2.272 \\ 2.522 \\ 2.71 \\ 2.805 \end{pmatrix} \qquad Stt_i := \left[1 + 0.12\cdot\left(Re_{TP_i}\right)^{1.14}\right]^{-0.1} \qquad Stt = \begin{pmatrix} 0.995 \\ 0.991 \\ 0.981 \\ 0.974 \\ 0.971 \\ 0.969 \\ 0.968 \end{pmatrix}$$

essentially constant over the tube length

For the assumed ΔT_{sat} (wall temp-fluid saturation temp) we calculate the value of ΔP_{sat} for C3F8. This value is the change in saturation pressure corresponding to the change in fluid temperature. At -25C the change in saturation pressure per degree C is 6800Pa, or for 5C ΔT_{sat}, the change is 34000Pa

$\Delta T_{sat} := 4.77K$ temperature difference between wall and fluid, assumed to start the process.

$\Delta p_{sat} := \Delta T_{sat}\cdot 6800\frac{Pa}{K}$ $\qquad \Delta p_{sat} = 324.36\cdot mbar$ pressure difference for temperature difference

$$h_{b_0} := .00122\cdot\left(\frac{k_{liq}^{0.79}\cdot c_{liq}^{0.45}\cdot \rho_{liq}^{0.49}}{\sigma^{0.5}\cdot \mu_{liq}^{0.29}\cdot \lambda^{0.24}\cdot \rho_v^{0.24}}\right)\cdot \Delta T_{sat}^{0.24}\cdot \Delta p_{sat}^{0.75}\cdot Stt_0$$

Chen

$h_{b_0} = 1025.288\cdot\frac{W}{m^2\cdot K}$ $\qquad h_0 := h_{b_0} + h_{c_0}$ $\qquad h_0 = 1.436\times 10^3\cdot\frac{W}{m^2\cdot K}$

$\Delta t_{b_0} := \frac{h_{flux}}{h_0}$ $\qquad \Delta t_{b_0} = 4.78K$ $\qquad$ ΔT assumed was 4.77C

For the next quality 0.1

$\Delta T_{sat} := 4.5K$ temperature difference between wall and fluid, assumed to start the process.

$\Delta p_{sat} := \Delta T_{sat}\cdot 6800\frac{Pa}{K}$ $\qquad \Delta p_{sat} = 306\cdot mbar$ pressure difference for temperature difference

$$h_{b_1} := .00122\cdot\left(\frac{k_{liq}^{0.79}\cdot c_{liq}^{0.45}\cdot \rho_{liq}^{0.49}}{\sigma^{0.5}\cdot \mu_{liq}^{0.29}\cdot \lambda^{0.24}\cdot \rho_v^{0.24}}\right)\cdot \Delta T_{sat}^{0.24}\cdot \Delta p_{sat}^{0.75}\cdot Stt_1$$

Chen

$h_{b_1} = 964.754\cdot\frac{W}{m^2\cdot K}$ $\qquad h_1 := h_{b_1} + h_{c_1}$ $\qquad h_1 = 1.539\times 10^3\cdot\frac{W}{m^2\cdot K}$

$\Delta t_{b_1} := \frac{h_{flux}}{h_1}$ $\qquad \Delta t_{b_1} = 4.46K$ $\qquad$ ΔT assumed was 4.5C

For the next quality 0.3

$\Delta T_{sat} := 3.74K$ temperature difference between wall and fluid, assumed to start the process.

$\Delta p_{sat} := \Delta T_{sat} \cdot 6800 \frac{Pa}{K}$ $\Delta p_{sat} = 254.32 \cdot mbar$ pressure difference for temperature difference

$$h_{b_2} := .00122 \cdot \left(\frac{k_{liq}^{0.79} \cdot c_{liq}^{0.45} \cdot \rho_{liq}^{0.49}}{\sigma^{0.5} \cdot \mu_{liq}^{0.29} \cdot \lambda^{0.24} \cdot \rho_v^{0.24}} \right) \cdot \Delta T_{sat}^{0.24} \cdot \Delta p_{sat}^{0.75} \cdot Stt_2$$ Chen

$h_{b_2} = 795.001 \cdot \frac{W}{m^2 \cdot K}$ $h_2 := h_{b_2} + h_{c_2}$ $h_2 = 1.836 \times 10^3 \cdot \frac{W}{m^2 \cdot K}$

$\Delta t_{b_2} := \frac{h_{flux}}{h_2}$ $\Delta t_{b_2} = 3.74 K$ ΔT assumed was 3.74C

For the next quality 0.5

$\Delta T_{sat} := 3.32K$ temperature difference between wall and fluid, assumed to start the process.

$\Delta p_{sat} := \Delta T_{sat} \cdot 6800 \frac{Pa}{K}$ $\Delta p_{sat} = 225.76 \cdot mbar$ pressure difference for temperature difference

$$h_{b_3} := .00122 \cdot \left(\frac{k_{liq}^{0.79} \cdot c_{liq}^{0.45} \cdot \rho_{liq}^{0.49}}{\sigma^{0.5} \cdot \mu_{liq}^{0.29} \cdot \lambda^{0.24} \cdot \rho_v^{0.24}} \right) \cdot \Delta T_{sat}^{0.24} \cdot \Delta p_{sat}^{0.75} \cdot Stt_3$$ Chen

$h_{b_3} = 701.13 \cdot \frac{W}{m^2 \cdot K}$ $h_3 := h_{b_3} + h_{c_3}$ $h_3 = 2.061 \times 10^3 \cdot \frac{W}{m^2 \cdot K}$

$\Delta t_{b_3} := \frac{h_{flux}}{h_3}$ $\Delta t_{b_3} = 3.33 K$ ΔT assumed was 3.32C

For the next quality 0.6

$\Delta T_{sat} := 3.19K$ temperature difference between wall and fluid, assumed to start the process.

$\Delta p_{sat} := \Delta T_{sat} \cdot 6800 \frac{Pa}{K}$ $\Delta p_{sat} = 216.92 \cdot mbar$ pressure difference for temperature difference

$$h_{b_4} := .00122 \cdot \left(\frac{k_{liq}^{0.79} \cdot c_{liq}^{0.45} \cdot \rho_{liq}^{0.49}}{\sigma^{0.5} \cdot \mu_{liq}^{0.29} \cdot \lambda^{0.24} \cdot \rho_v^{0.24}} \right) \cdot \Delta T_{sat}^{0.24} \cdot \Delta p_{sat}^{0.75} \cdot Stt_4$$

$h_{b_4} = 671.984 \cdot \frac{W}{m^2 \cdot K}$ $h_4 := h_{b_4} + h_{c_4}$ $h_4 = 2.151 \times 10^3 \cdot \frac{W}{m^2 \cdot K}$

$\Delta t_{b_4} := \frac{h_{flux}}{h_4}$ $\Delta t_{b_4} = 3.192 K$ ΔT assumed was 3.19C

For the next quality 0.7

$\Delta T_{sat} := 3.1K$ temperature difference between wall and fluid, assumed to start the process.

$\Delta p_{sat} := \Delta T_{sat} \cdot 6800 \frac{Pa}{K}$ $\Delta p_{sat} = 210.8 \cdot mbar$ pressure difference for temperature difference

$$h_{b_5} := .00122 \cdot \left(\frac{k_{liq}^{0.79} \cdot c_{liq}^{0.45} \cdot \rho_{liq}^{0.49}}{\sigma^{0.5} \cdot \mu_{liq}^{0.29} \cdot \lambda^{0.24} \cdot \rho_v^{0.24}} \right) \cdot \Delta T_{sat}^{0.24} \cdot \Delta p_{sat}^{0.75} \cdot Stt_5$$

$h_{b_5} = 651.799 \cdot \frac{W}{m^2 \cdot K}$ $h_5 := h_{b_5} + h_{c_5}$ $h_5 = 2.218 \times 10^3 \cdot \frac{W}{m^2 \cdot K}$

$\Delta t_{b_5} := \frac{h_{flux}}{h_5}$ $\Delta t_{b_5} = 3.095 K$ ΔT assumed was 3.1C

For the next quality 0.85

$\Delta T_{sat} := 3.05K$ temperature difference between wall and fluid, assumed to start the process.

$\Delta p_{sat} := \Delta T_{sat} \cdot 6800 \frac{Pa}{K}$ $\Delta p_{sat} = 207.4 \cdot mbar$ pressure difference for temperature difference

$$h_{b_6} := .00122 \cdot \left(\frac{k_{liq}^{0.79} \cdot c_{liq}^{0.45} \cdot \rho_{liq}^{0.49}}{\sigma^{0.5} \cdot \mu_{liq}^{0.29} \cdot \lambda^{0.24} \cdot \rho_v^{0.24}} \right) \cdot \Delta T_{sat}^{0.24} \cdot \Delta p_{sat}^{0.75} \cdot Stt_6$$

$h_{b_6} = 640.695 \cdot \frac{W}{m^2 \cdot K}$ $\qquad h_6 := h_{b_6} + h_{c_6}$ $\qquad h_6 = 2.251 \times 10^3 \cdot \frac{W}{m^2 \cdot K}$

$\Delta t_{b_6} := \frac{h_{flux}}{h_6}$ $\qquad \Delta t_{b_6} = 3.05\,K$ $\qquad \Delta T$ assumed was 3.05C