

High Thermal Conductivity, Mesophase Pitch-Derived Carbon Foams

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Keywords: Graphite Foam, Thermal Conductivity, Thermal Management

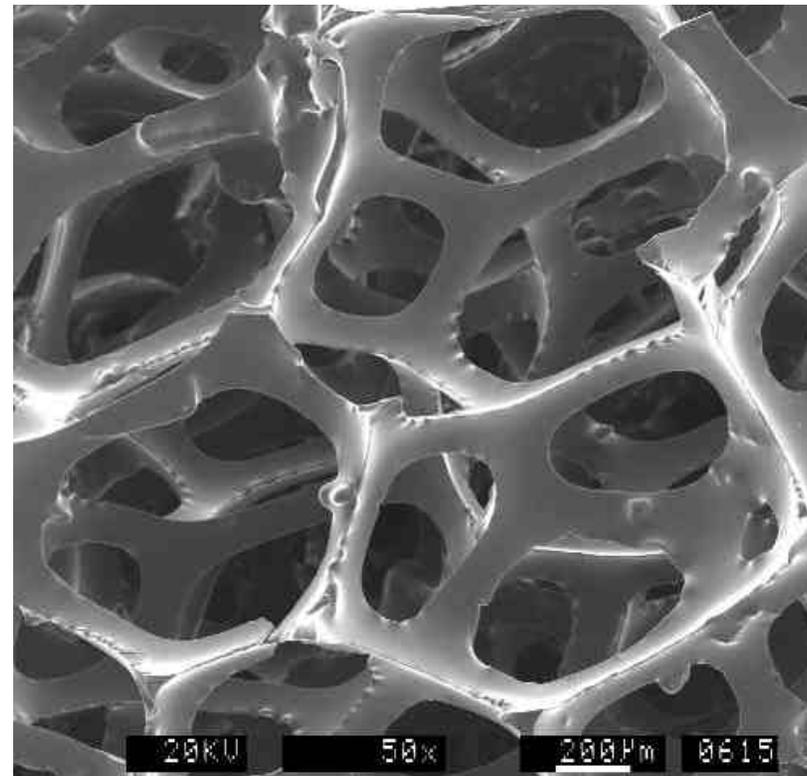


Outline

- Graphite Foams
- Foam Structure and Properties
 - ⇒ Scanning Electron Microscopy
 - ⇒ Optical Microscopy - cross polarized light interference patterns
 - ⇒ X-ray Analysis
 - ⇒ Thermal properties - Xenon Probe Flash Diffusivity Technique
 - ⇒ Mechanical Properties
- Engineered Graphite Foam Applications
 - ⇒ Heat sinks
 - ⇒ Heat Exchangers
 - ⇒ Satellites
 - ⇒ Heat Resistant Composites

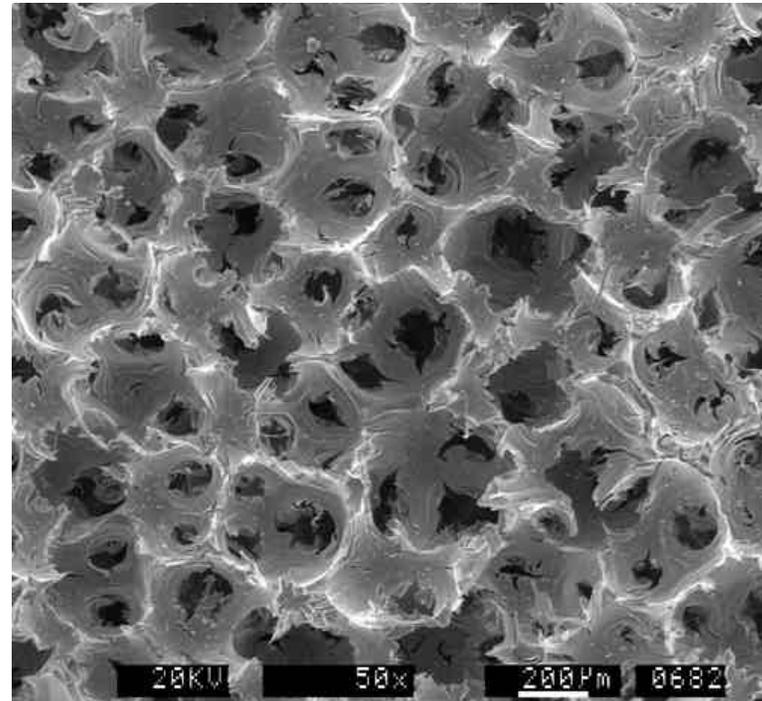
Typical Carbon Foams

- Made from amorphous carbons
- More recently made from pitches and mesophases
- 5-25% dense
- Thermal insulators
 - ⇒ $\kappa < 10 \text{ W/m}\cdot\text{K}$
- strengths similar to honeycomb materials
- ability to absorb tremendous amounts of impact energy



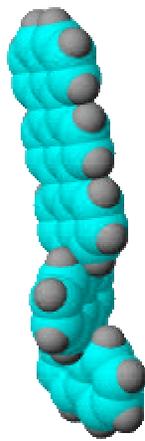
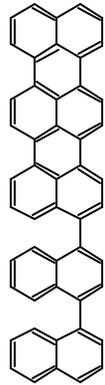
ORNL Mesophase-Derived Graphitic Foam

- Graphitic ligaments
 - ⇒ Graphitic-like properties (high κ , E, σ)
- Dimensionally stable, low CTE
- No outgassing
- Open Porosity
- Excellent thermal management material

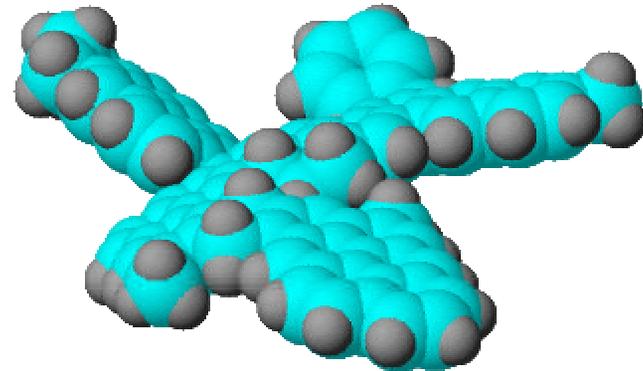
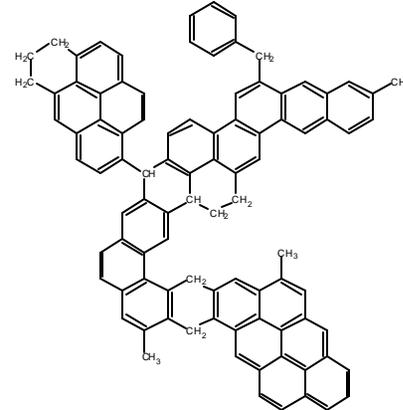


Mesophase Pitch

- Typical molecular structures are different
 - ⇒ may affect shear orientation during processing
 - ⇒ may affect mechanical and thermal properties



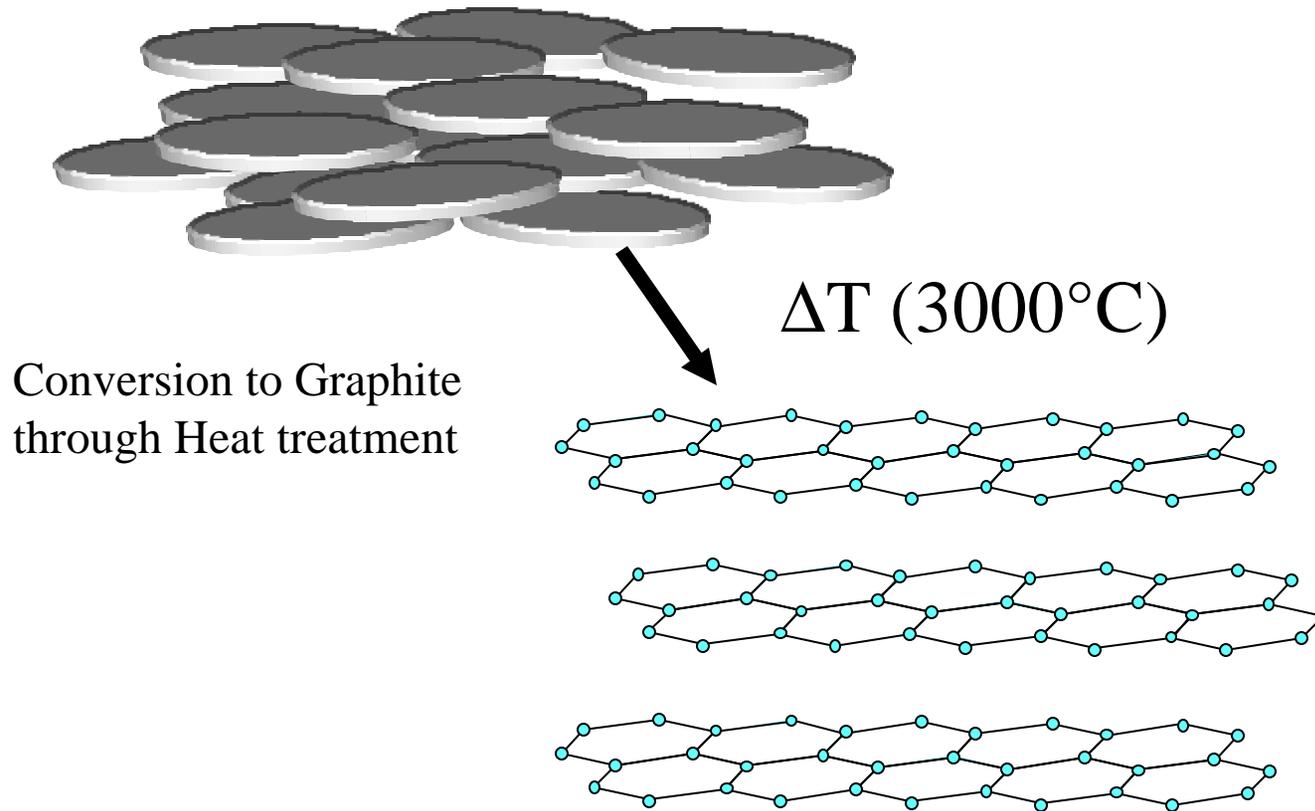
Mitsubishi AR Mesophase



Typical Petroleum Derived Mesophase

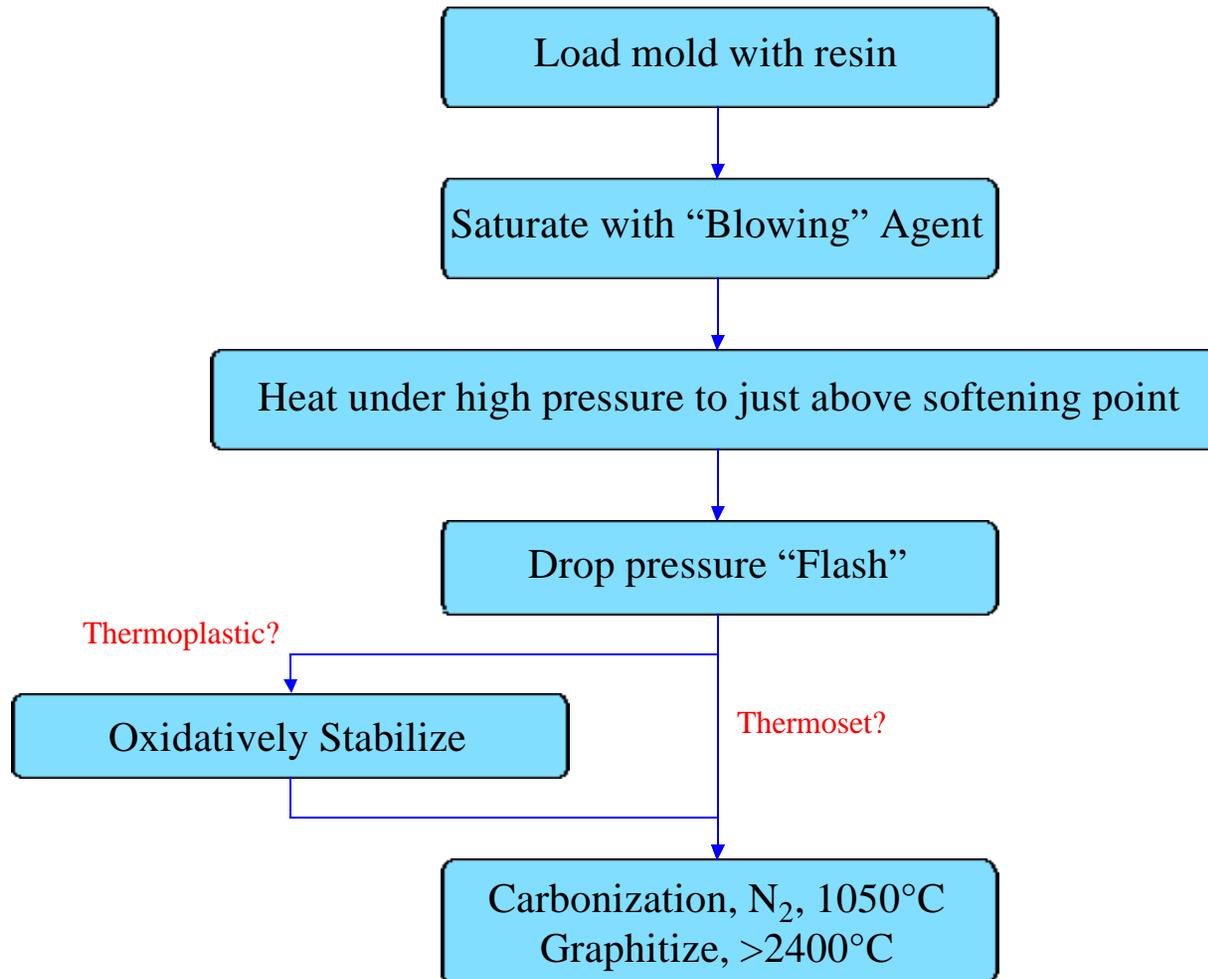
Mesophase Pitch

- Under proper processing and heat treatments, the mesophase molecules become a Discotic Nematic Liquid Crystal
 - ➔ (400°C, 40 hours, Nitrogen Cover)



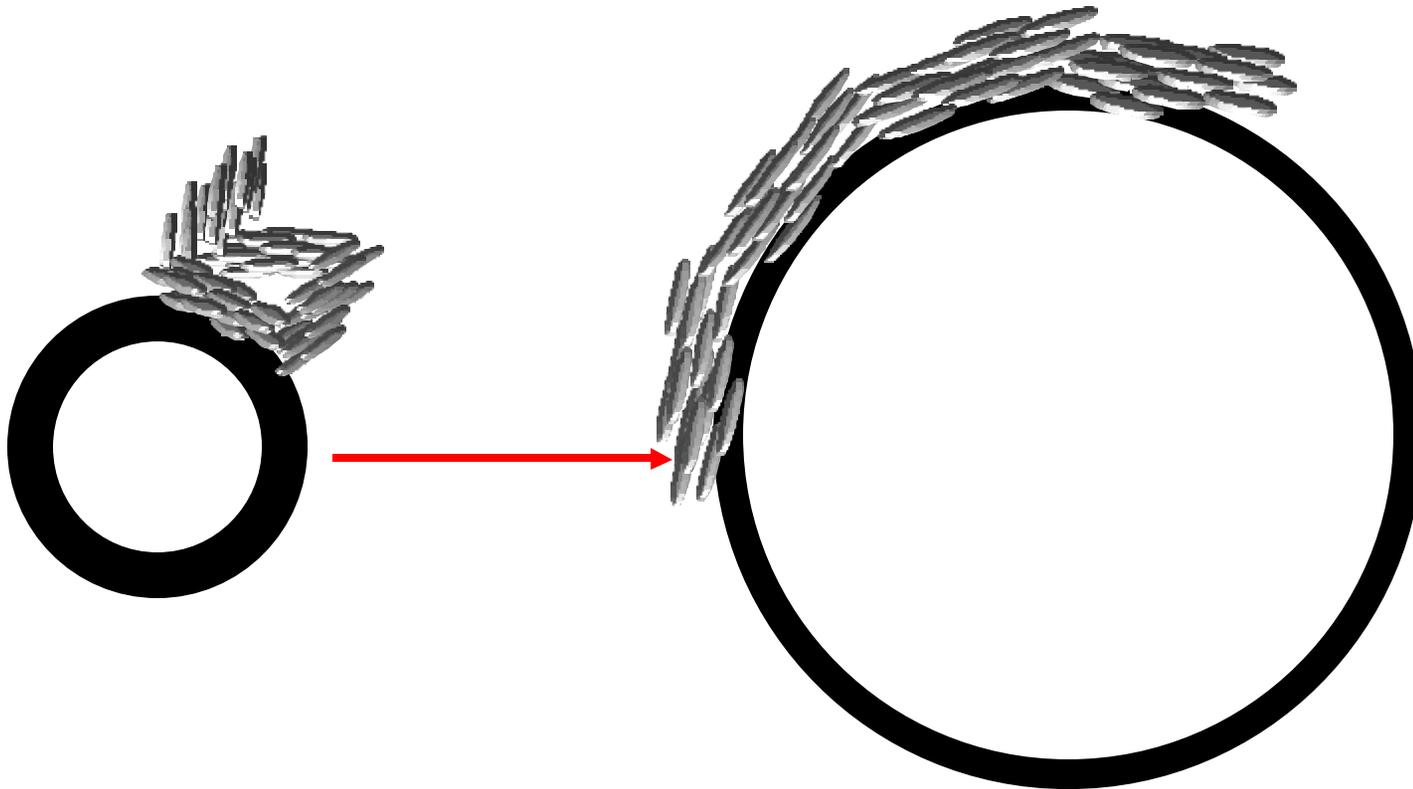
Traditional Carbon Foams - Manufacture

- Traditional “Blowing” techniques



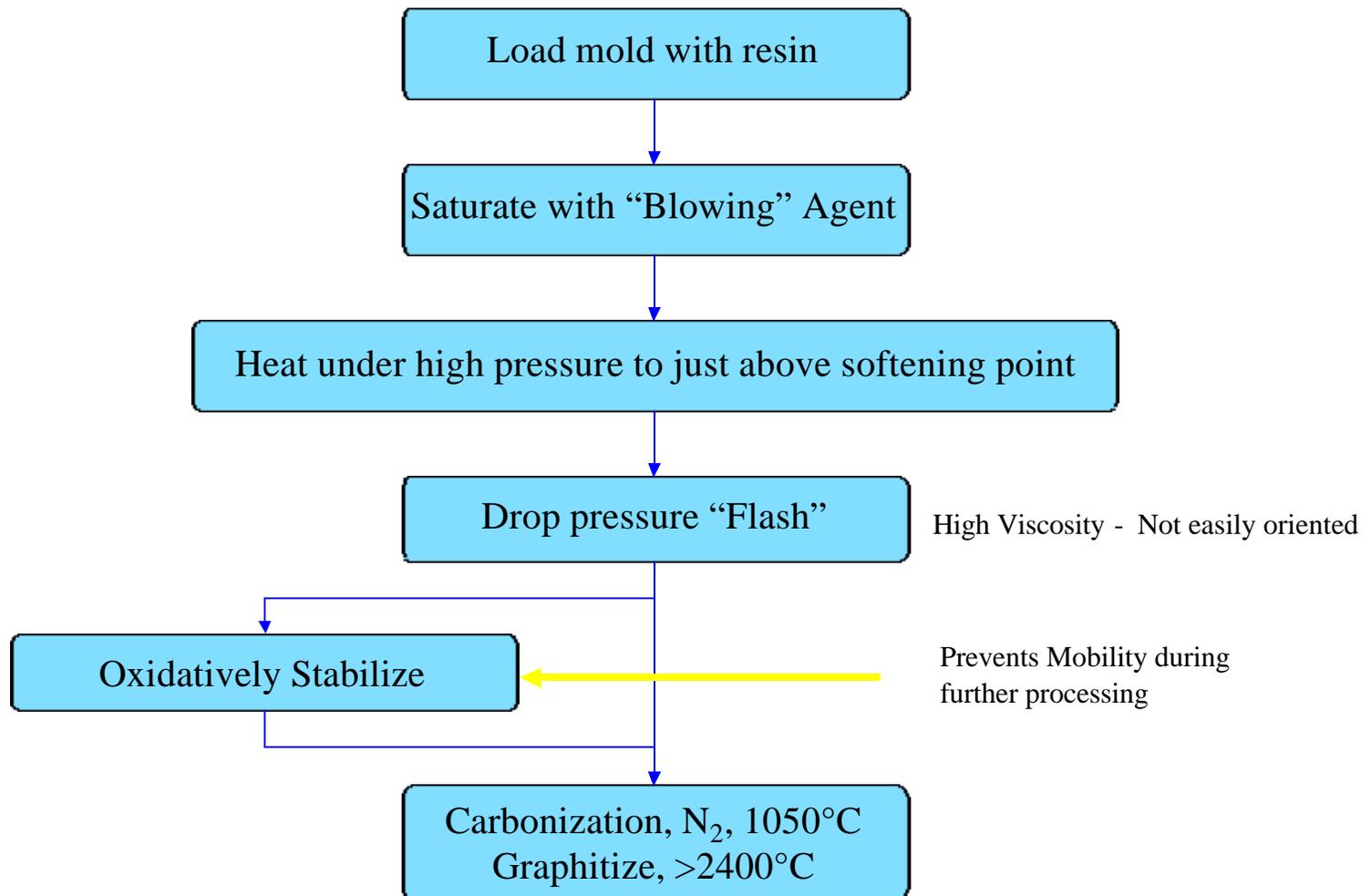
Bubble Growth

- Bi-Axial Extension causes liquid crystal to orient parallel to surface of bubble
 - ➔ similar to extension caused during formation of fibers.



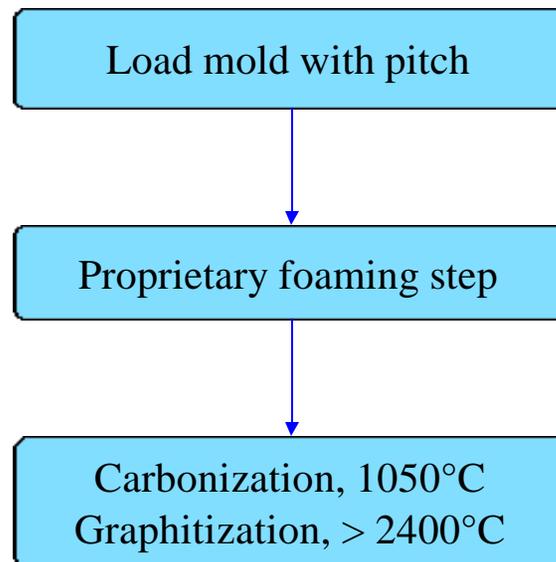
Traditional Carbon Foams - Problems

- Traditional “Blowing” techniques



Novel Production Method

- Proprietary method (many patents filed)
- Unlike traditional foaming techniques
 - ⇒ No blowing (flashing) or pressure drop required
 - ➔ saves steps
 - ⇒ No oxidative stabilization required
 - ➔ improved thermal properties



Mesophase Pitch Precursors

- Two separate 100% mesophase pitches
 - ⇒ Synthetic mesophase from naphthalene
 - ⇒ Proprietary high melting point mesophase from petroleum pitch

Mesophase	Softening Point [°C]	Mesophase Content [°C]	Carbon Yield @1000°C, N ₂
Mitsubishi ARA 24	237	100	78
Conoco	355	100	87

Foam Processing

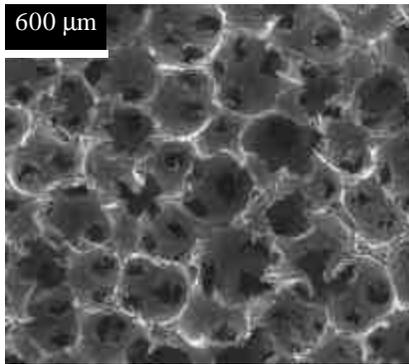
- Proprietary foaming method developed at ORNL
- Foams of both pitches were produced under 4 different processing conditions
 - ⇒ A, B, C, D.
- The goal was to produce foams with varying density
 - ⇒ properties as a function of density could be determined.
- Foams carbonized at 1000°C at 0.2°C/min
- Foams graphitized at 2800°C at 9°C/min

Properties of Graphitized Foams

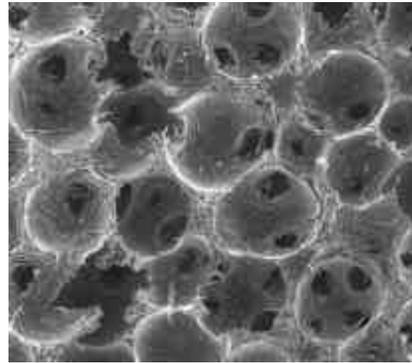
Processing Condition	AR Derived Foam		Conoco Derived Foam	
	Density [g/cm ³]	Mean Pore Diameter* [mm]	Density [g/cm ³]	Mean Pore Diameter* [mm]
A	0.25	354 ± 115	0.32	89 ± 79
B	0.39	361 ± 150	0.43	70 ± 54
C	0.48	293 ± 136	0.54	66 ± 65
D	0.57	275 ± 120	0.59	60 ± 49

*From optical image analysis

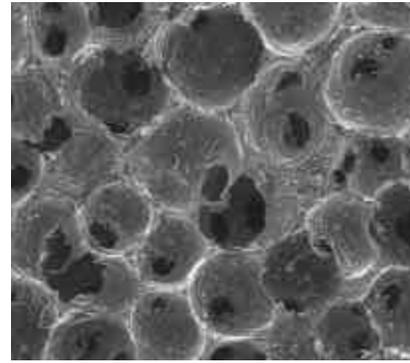
Foam Microstructure - AR Pitch



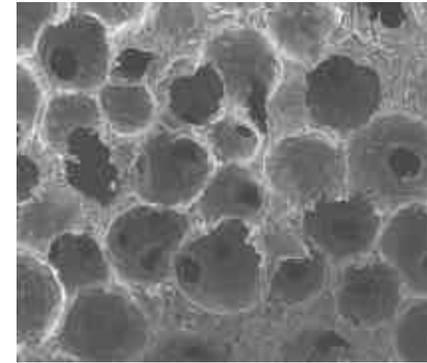
A



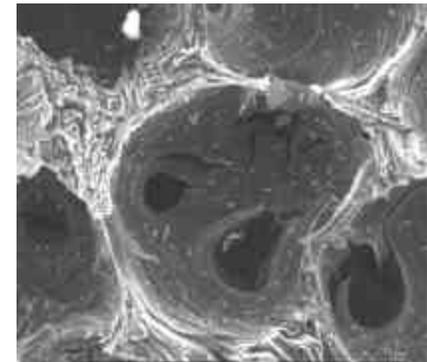
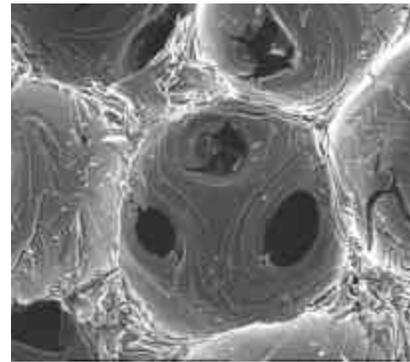
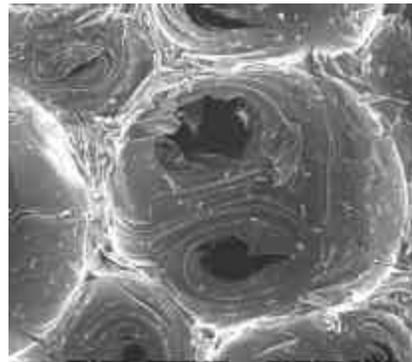
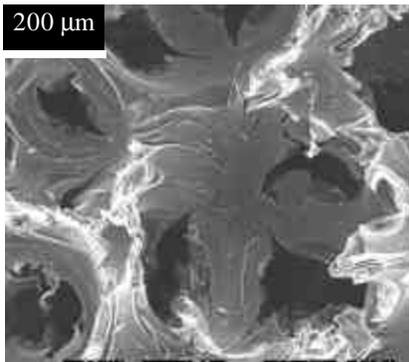
B



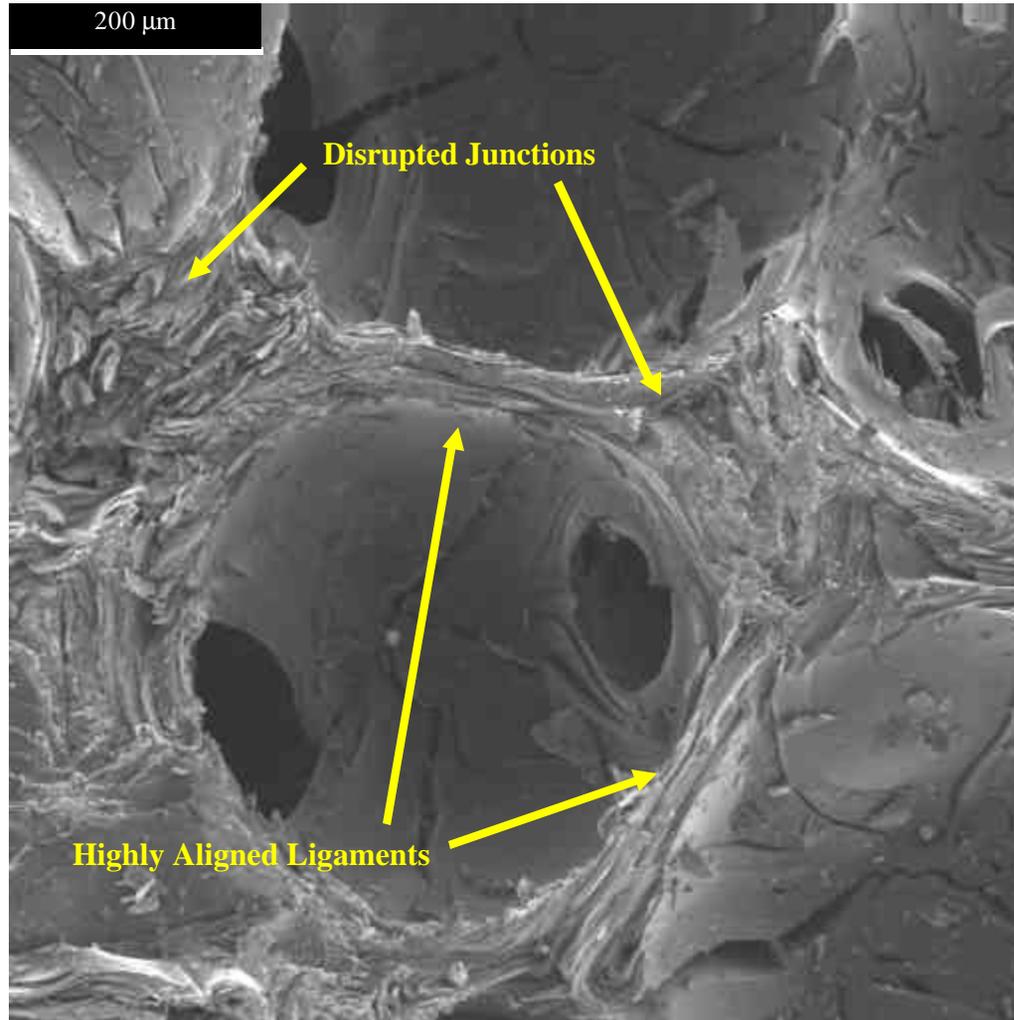
C



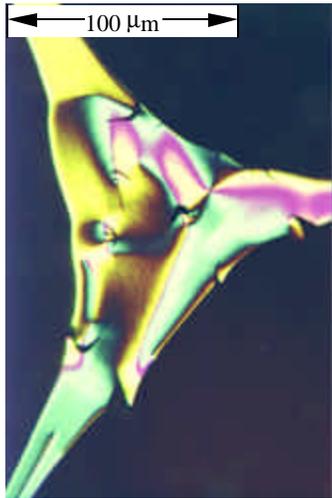
D



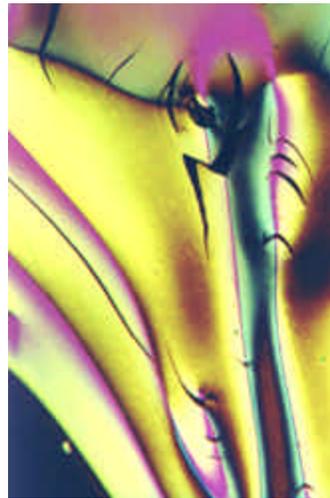
Graphitic Structure - AR Pitch -D



Graphitic Alignment and Structure - AR Pitch



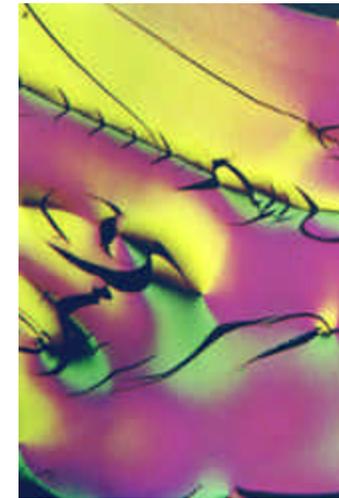
A



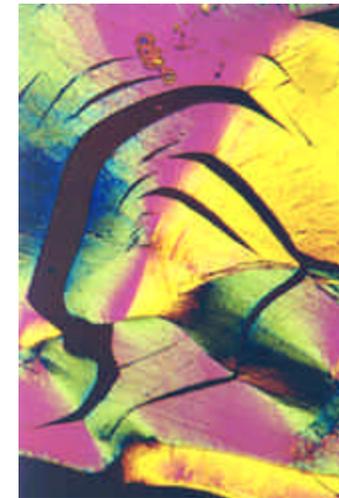
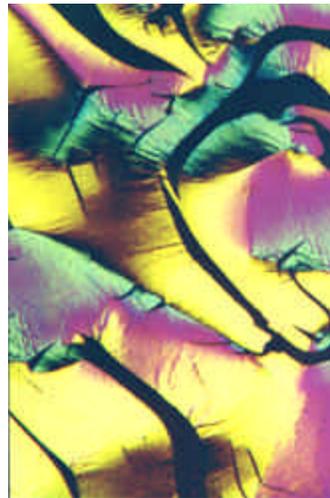
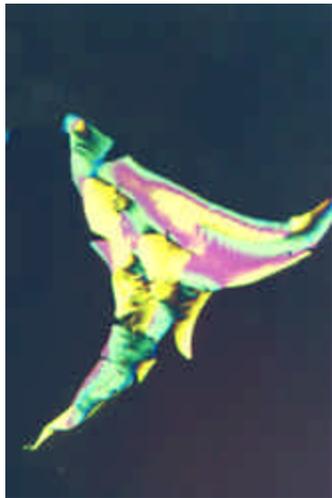
B



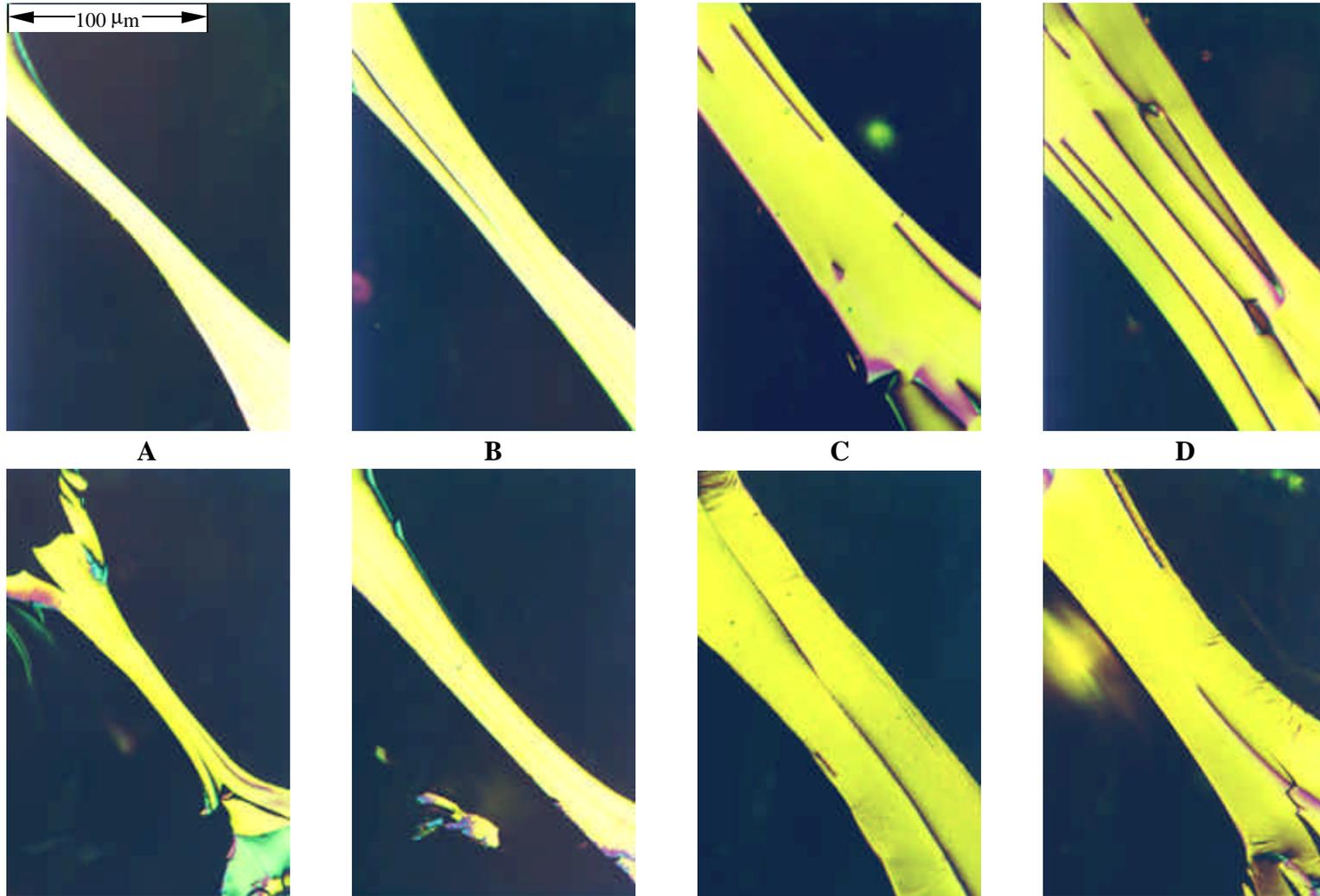
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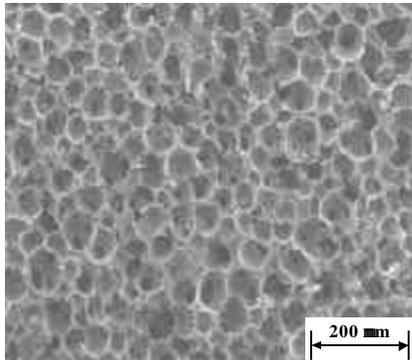
D



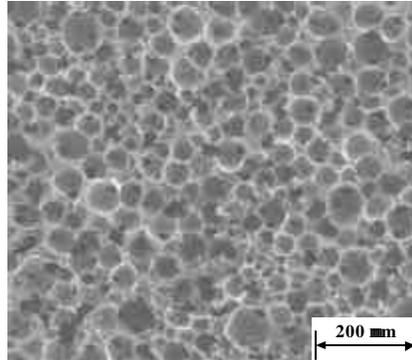
Graphitic Alignment and Structure - AR Pitch



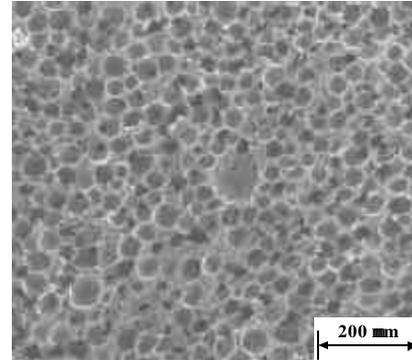
Foam Microstructure - Conoco Pitch



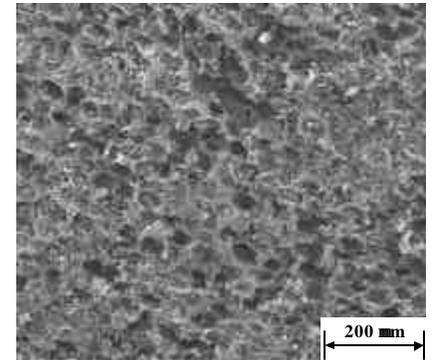
A



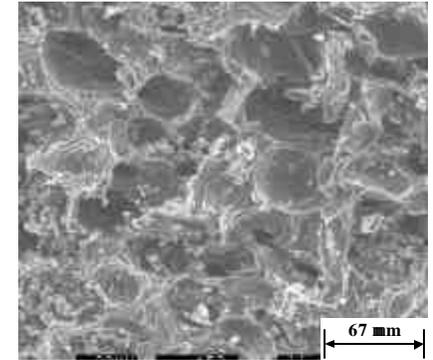
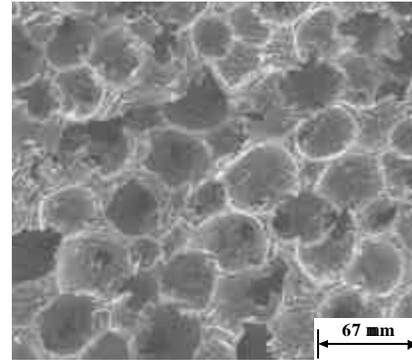
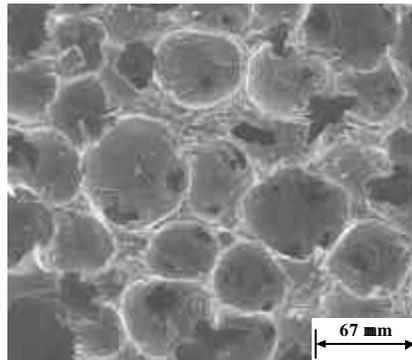
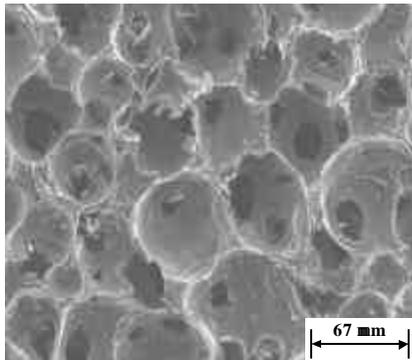
B



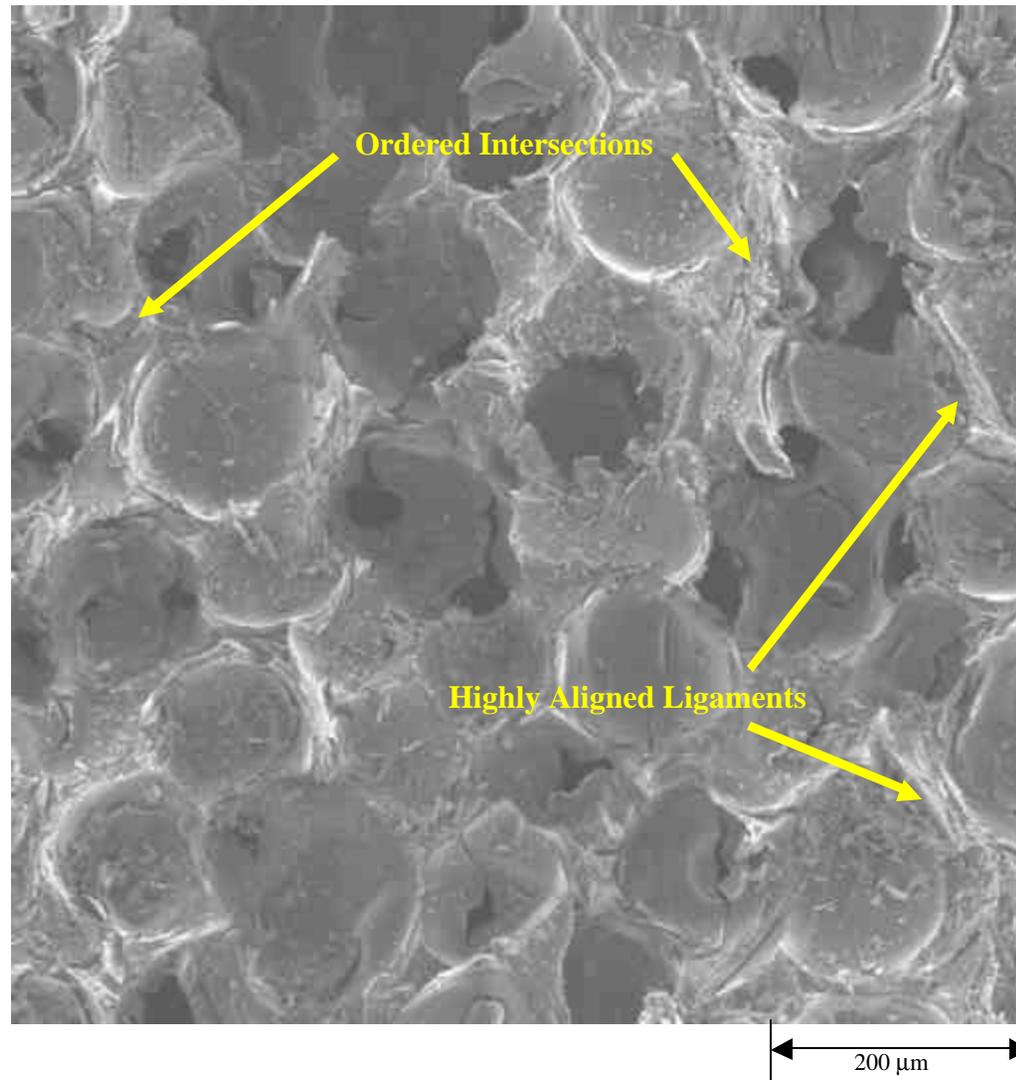
C



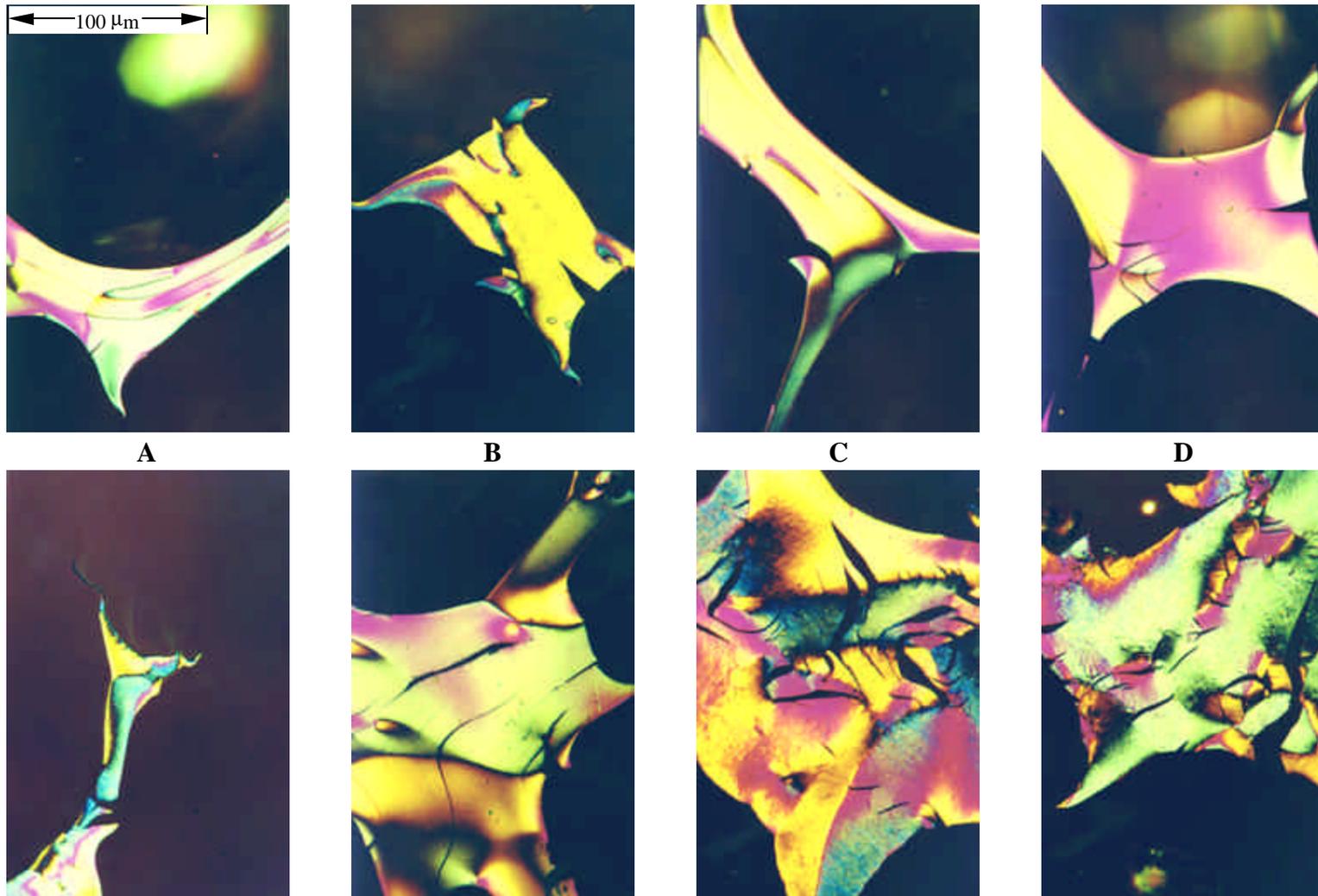
D



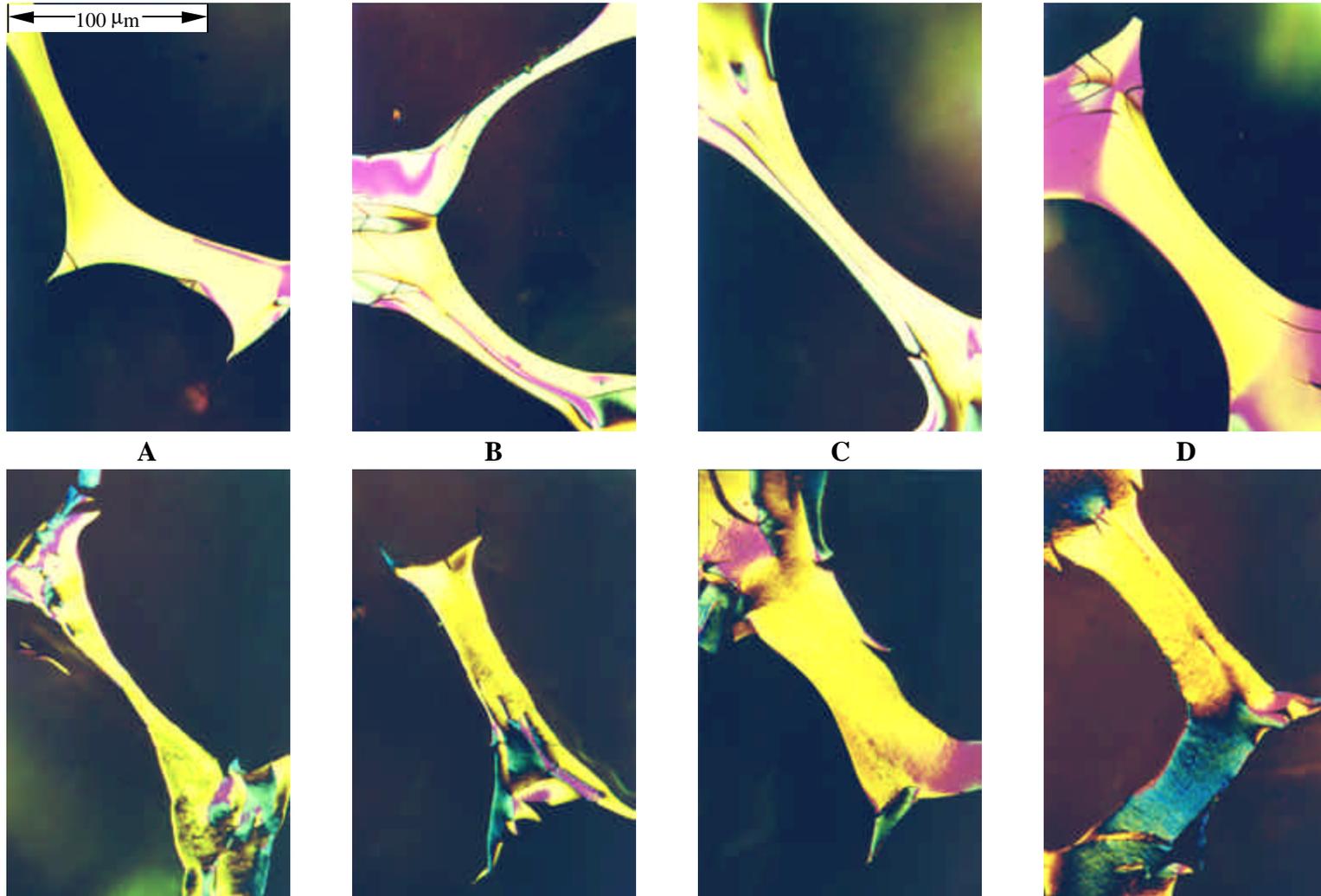
Graphitic Structure - Conoco Pitch -D



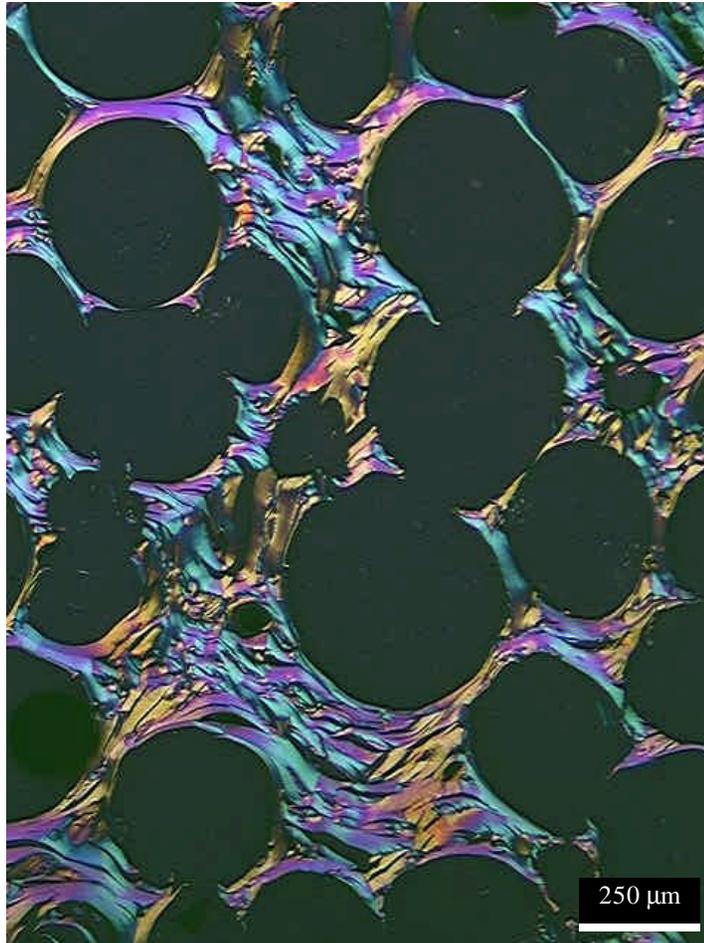
Graphitic Alignment and Structure - Conoco Pitch



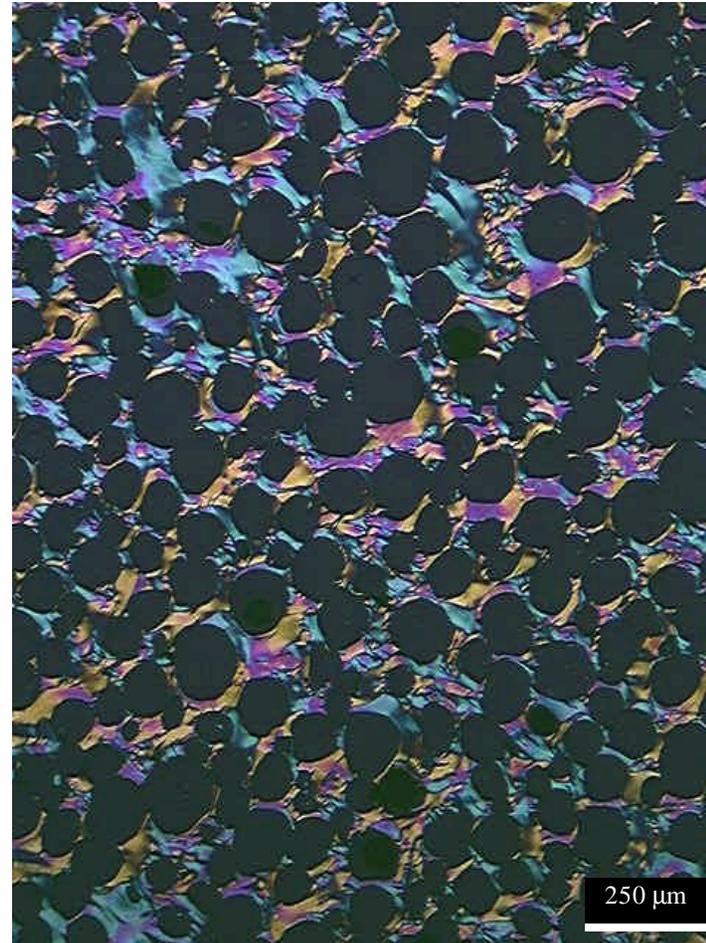
Graphitic Alignment and Structure - Conoco Pitch



Microstructures



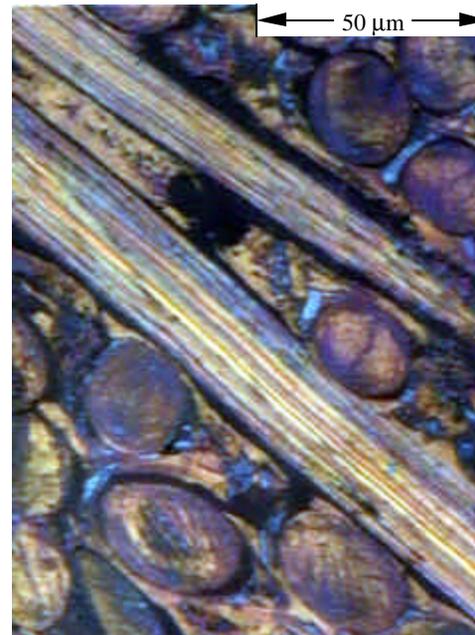
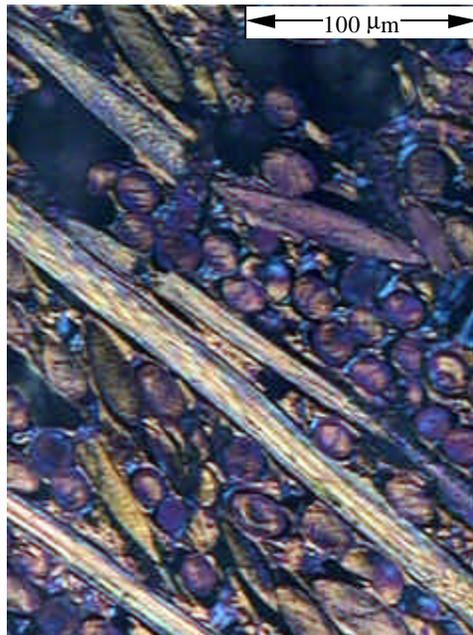
AR Derived Foam (D)



Conoco Derived Foam (D)

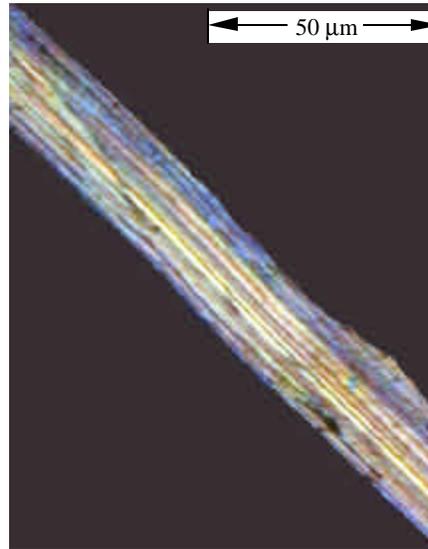
Comparison of Ligaments to High Performance Fibers

- Composites made with DKD-x fibers graphitized at 2800°C for 1 hour
- After high heat treatment DKD-x fibers very similar to K1100
- Estimated thermal conductivity is ~600-800 W/m·K



Comparison of Ligaments to High Performance Fibers

DKD-x® Fiber
2800°C



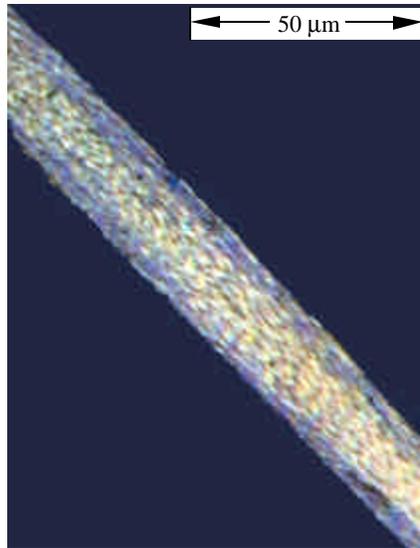
ORNL
Graphite Foam
2800°C



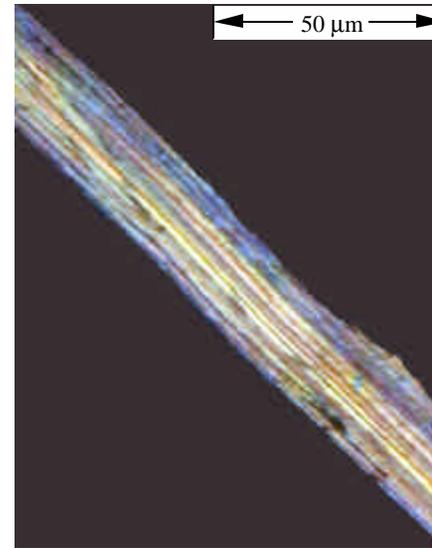
Comparison of Ligaments to High Performance Fibers



PAN Fiber
2800°C
 $\kappa \sim 50 \text{ W/m}\cdot\text{K}$



P-55 Fiber
2800°C
 $\kappa \sim 150 \text{ W/m}\cdot\text{K}$

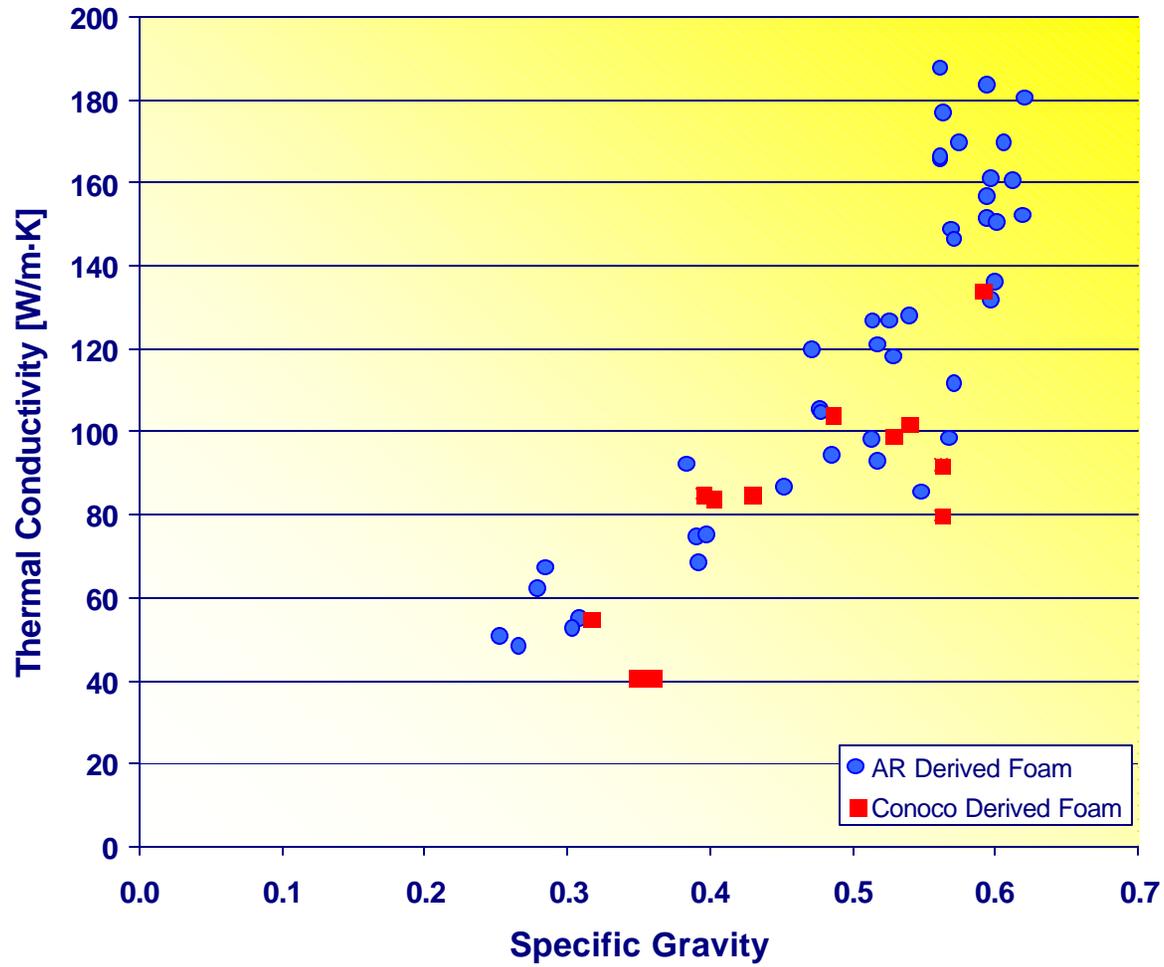


DKD-x® Fiber
2800°C
 $\kappa \sim 600 \text{ W/m}\cdot\text{K}$



ORNL Graphite Foam
2800°C
 $\kappa \sim ?$

Thermal Properties - Graphitized Foams



Helium Pycnometry - skeletal density

Material	Density	Thermal Conductivity
	[g/cm ³]	[W/m·K]
P55 fiber	2.00	120
P120 fiber	2.17	640
K1100 fiber	2.20	1000
ORNL Graphite Foam	2.23	?

Thermally Conductive Foams

$$\mathbf{k}_{bulk} \approx 0.35 \left(\frac{\mathbf{r}}{\mathbf{r}_{skel}} \right) \mathbf{k}_{ligament}$$

	Relative Density [%]	Ligament Conductivity [W/m·K]	Bulk Conductivity [W/m·K]
Aluminum foam	25	180	~15
Copper foam	25	400	~40
Foam with P55 type ligament	25	120	~12
Foam with P120 type ligament	25	640	~60
ORNL Graphite Foam	25		180

Crystal Parameters of Foams

Foam	Specific Gravity	Interlayer Spacing d_{002}^* [nm]	Crystal Size L_a [nm]	Stack Height L_c [nm]
<i>Mitsubishi ARA24</i>				
A	0.25	.3364	11.8	48.2
B	0.39	.3362	17.8	46.6
C	0.48	.3360	21.5	79.3
D	0.57	.3355	18.4	82.4
<i>Conoco B</i>				
A	0.35	.3357	16.7	29.5
B	0.40	.3363	13.0	38.7
C	0.49	.3358	19.5	97.6
D	0.59	.3360	19.8	50.8

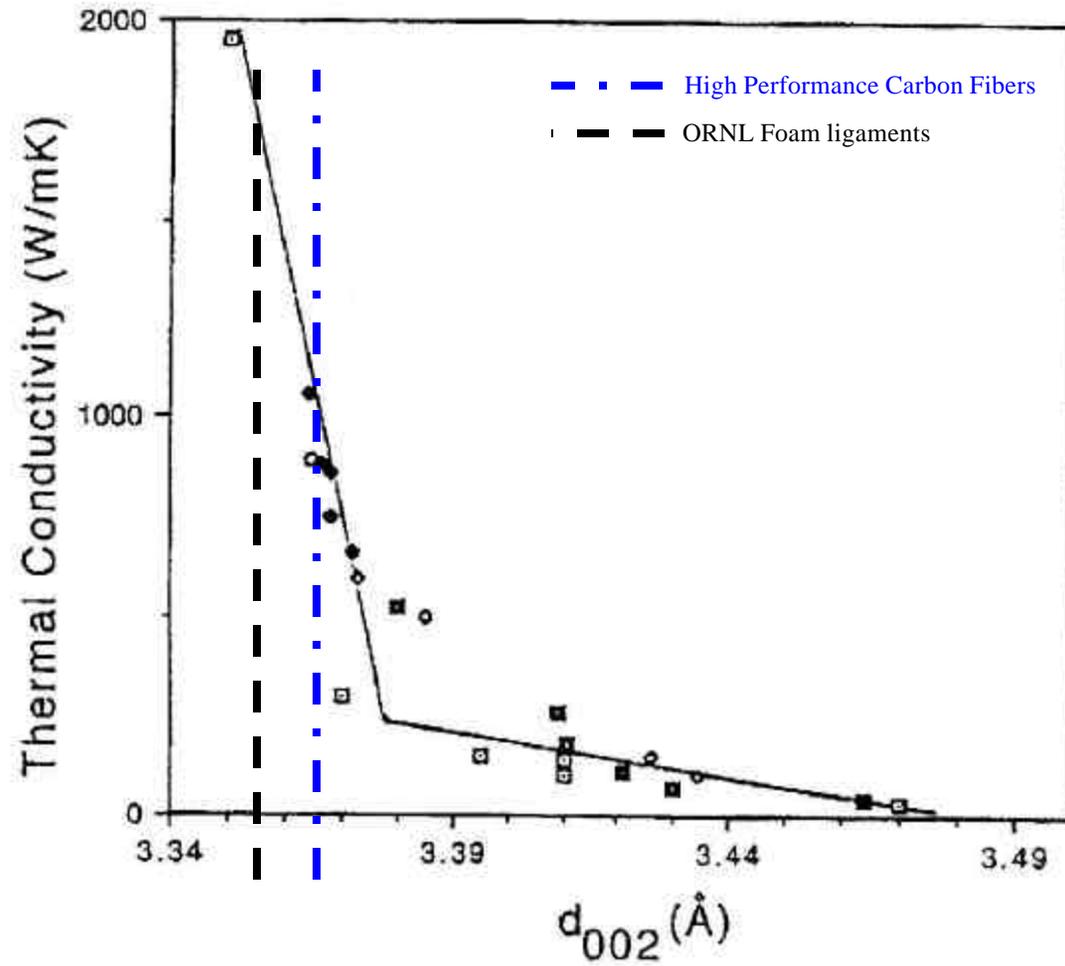
*perfect graphite is 0.3354

Comparison of Crystal Parameters to Fibers

Material	HTT	d_{002} -spacing*	L_a (crystal size)	L_c (stack height)	κ
	[°C]	[nm]	[nm]	[nm]	[W/m·K]
P30-x fiber ⁽⁶⁾	2500	0.3375	50	32	>500
K321 fiber ⁽⁶⁾	2500	0.3376	33	50	>500
EWC-600 ⁽⁶⁾	--	0.3374	55	32	640
Clemson Ribbon ⁽²⁾	2400	0.3380	32	12	950
K1100 ⁽³⁾	--	0.3366	85	51	1000
Fixed catalyst VGCF ⁽¹⁾	2800	0.3366	40 ⁽⁴⁾	37 ⁽⁴⁾	1950
<i>AR Foam Ligament</i>	2800	0.3355	19	82	>1750
<i>Conoco Foam Ligament</i>	2800	0.3360	20	51	>1750

* Turbostratic graphite = >0.3440 nm
 Single crystal graphite = 0.3354 nm

Crystal Effects on Thermal Conductivity



(data from Rellick, et. al., (6))

Ligament Conductivity

- Compelling evidence to extremely high thermal conductivity in ligaments of ORNL Graphite Foam
 - ⇒ optical microscopy
 - significantly larger monochromatic regions than K1100 fibers
 - ⇒ Helium Pycnometry
 - higher skeletal density than K1100 fibers
 - ⇒ X-ray analysis
 - d-spacing closer to pure graphite than K1100 fibers
 - plot of d-spacing indicates conductivity about 1800 W/m·K
 - ⇒ Bulk thermal conductivity
 - order of magnitude greater than aluminum foams of similar relative density
 - anticipate ligaments to be order of magnitude greater than aluminum

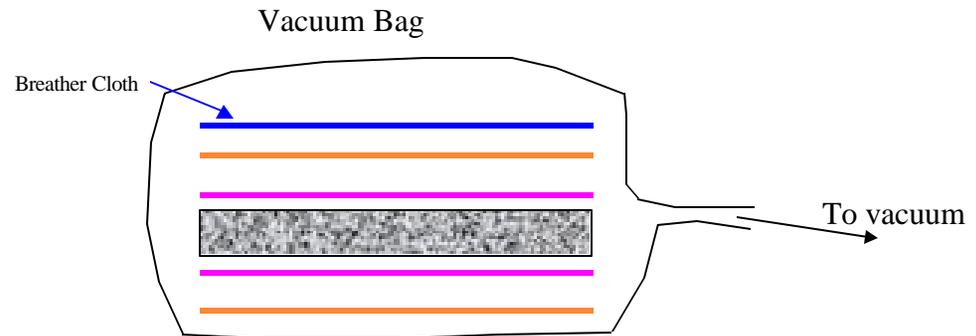
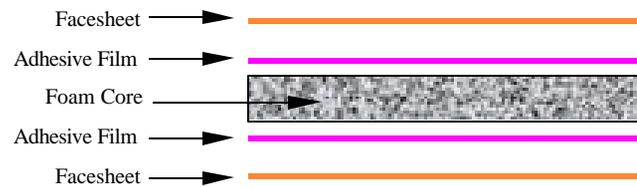
Thermal Properties vs Other Materials

Material	Specific Gravity	Thermal Conductivity		Specific Conductivity	
		//	⊥	//	⊥
		[W/m·K]	[W/m·K]	[W/m·K]	[W/m·K]
AR Derived Foam D-2800	0.56	187	187	334	334
Conoco Derived Foam D-2800	0.59	134	134	227	227
Copper	8.9	400	400	45	45
Aluminum 6061	2.8	180	180	64	64
EWC-300/Epoxy Resin	1.72	109	1	63	1
K321/AR Pitch Carbon/Carbon	1.77	233	20	132	11
Amoco SRG	1.76	650	20	369	11
Aluminum Foam	0.5	12	12	24	24

†Specific Conductivity = Thermal Conductivity/Specific Gravity

Laminate Fabrication and Joining Techniques

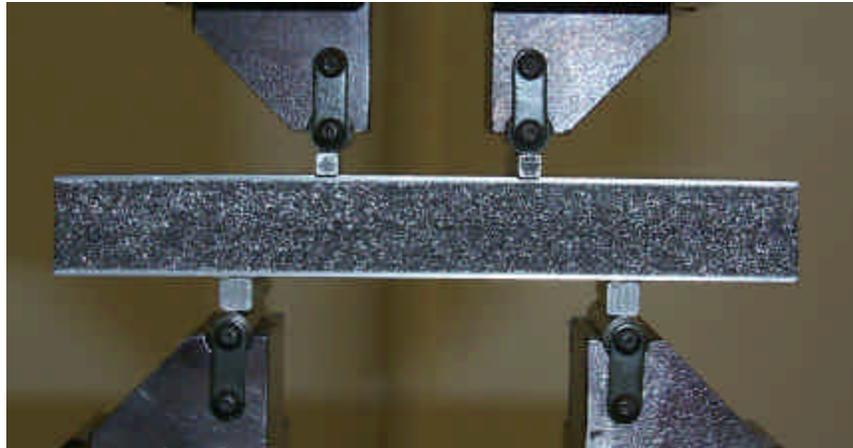
➤ Autoclave process



Cure at 35 psi, 150°C, 30 minutes

Flexural Testing

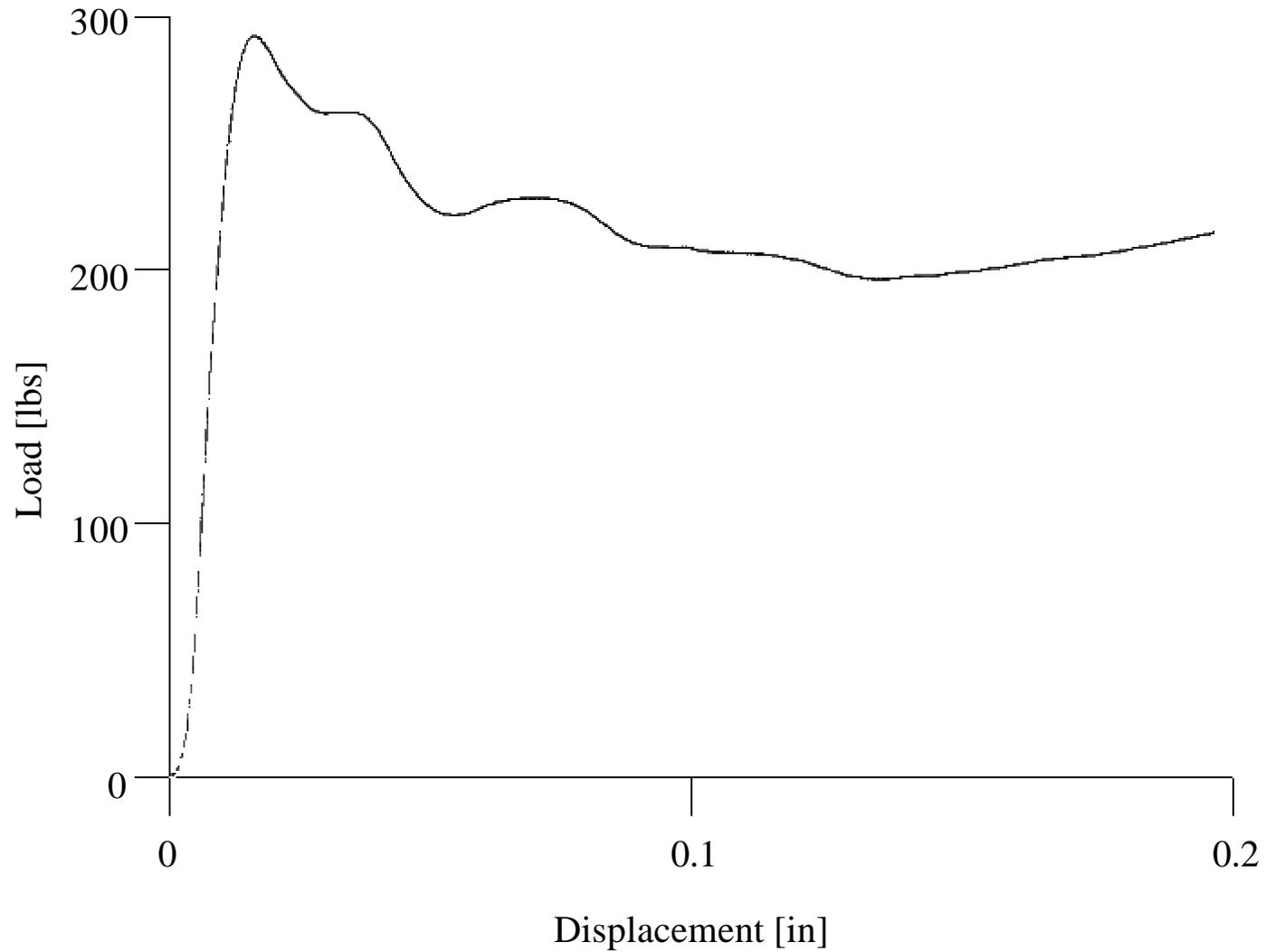
No Load



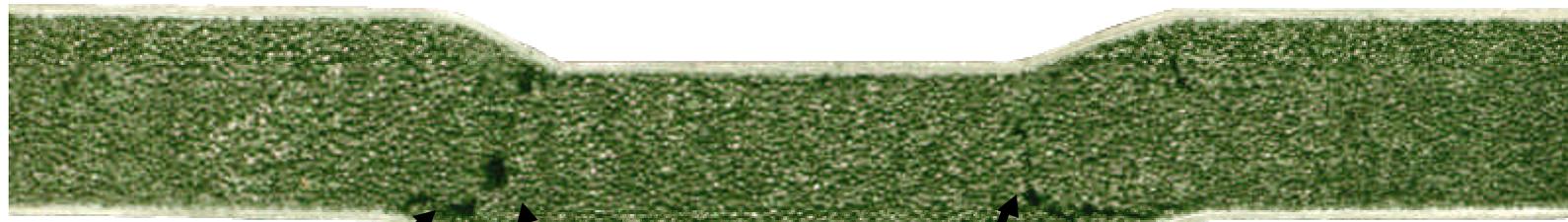
Load = 200 lb
Displacement = 0.17 in



Typical Flexural Testing Results



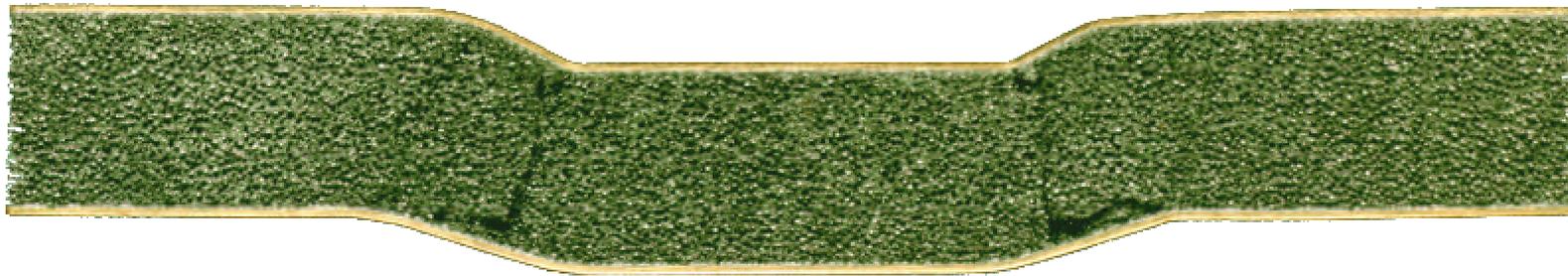
Flexural Testing Results



Delamination

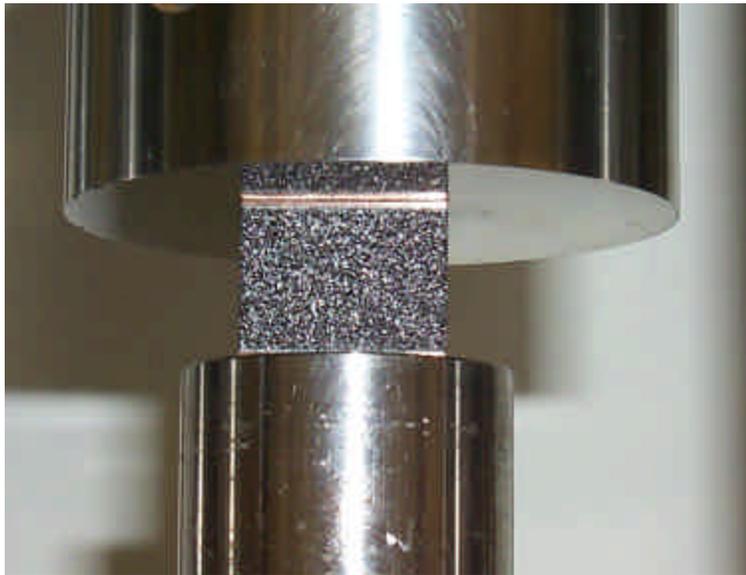
Classic Shear Failure

Aluminum Facesheets

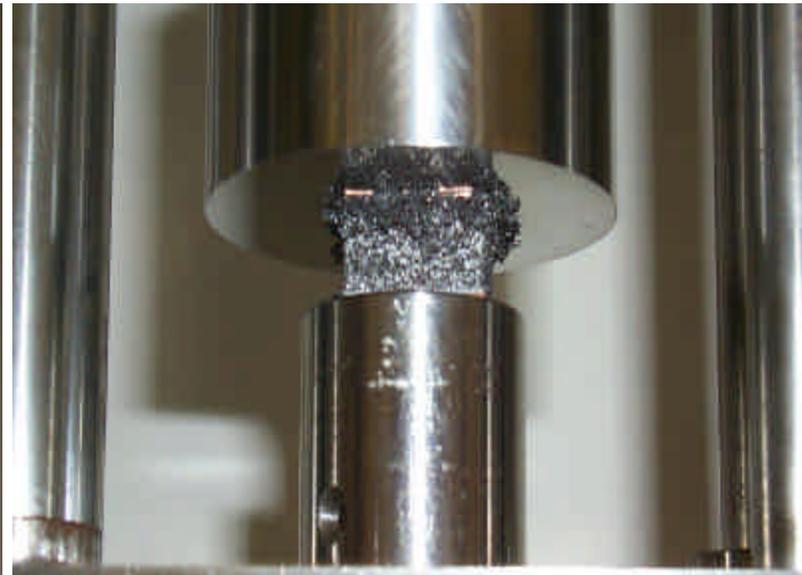


Copper Facesheets

Compression Testing

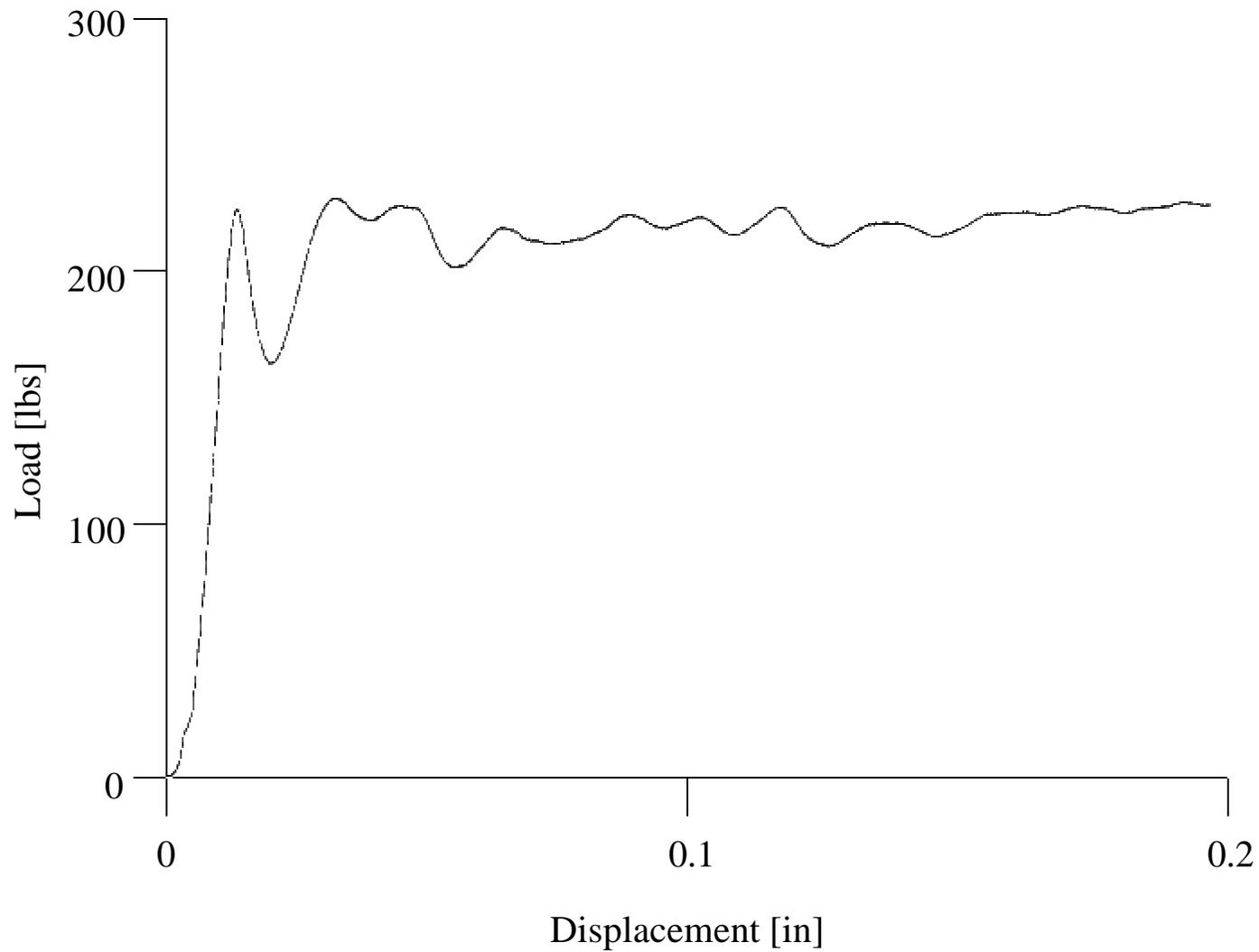


No Load



Load = 220 lb
Deflection = 0.2 in

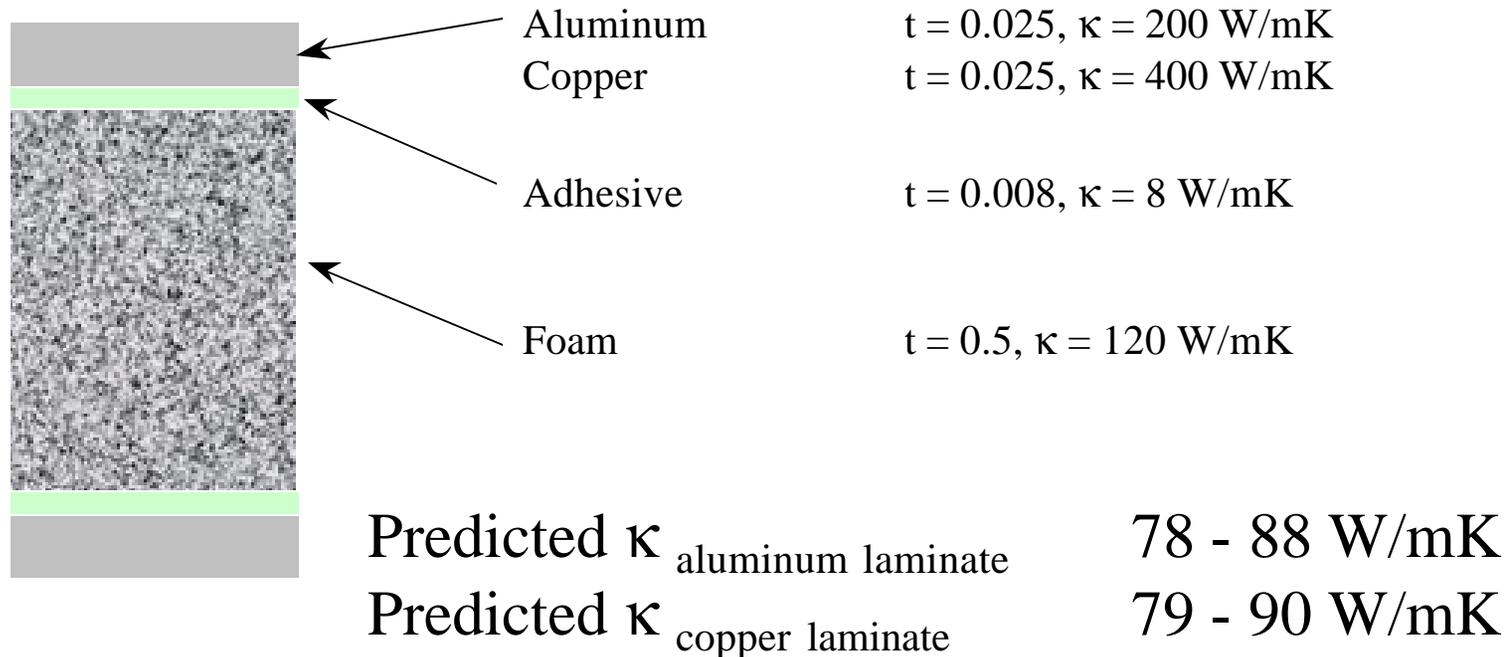
Typical Compression Testing Results



Thermal Testing of Laminates

Material	Specific Gravity	Thermal Conductivity		Specific Conductivity	
		//	⊥	//	⊥
		[W/m·K]	[W/m·K]	[W/m·K]	[W/m·K]
<i>Al-A</i>	<i>0.75</i>	<i>~150</i>	<i>51</i>	<i>200</i>	<i>68</i>
<i>Al-B</i>	<i>0.75</i>	<i>~150</i>	<i>64</i>	<i>200</i>	<i>86</i>
<i>Cu-A</i>	<i>1.17</i>	<i>~150</i>	<i>60</i>	<i>128</i>	<i>51</i>
<i>Cu-B</i>	<i>1.21</i>	<i>~150</i>	<i>55</i>	<i>124</i>	<i>45</i>
EWC-300/Epoxy resin ⁽¹⁾	1.72	109	1	63	0.6
K321/AR Pitch Carbon-Carbon ⁽²⁾	1.88	233	20	124	10.6
Aluminum	2.77	150-200	150-200	54-72	54-72
Aluminum Foam ⁽³⁾	0.50	12	12	24	24
Aluminum Honeycomb ⁽⁴⁾	0.19	--	~10	--	52

Predicted Thermal Conductivity



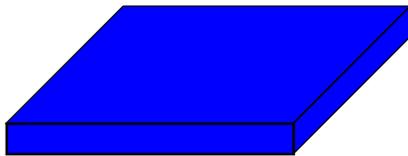
The limiting factor in the thermal conductivity is the adhesive.

Potential Applications

“Out of the Box” Thinking

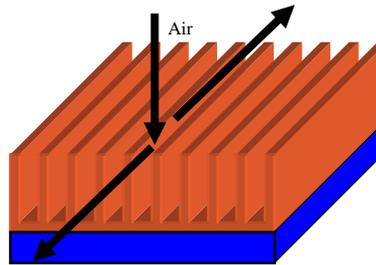
Foams as Heat Sinks

Heater @ 90% output



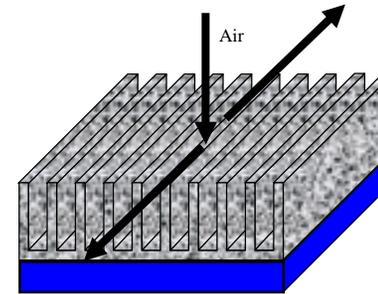
Mass of Sink = 0 g
Temperature = 170°F

Standard Aluminum
Heat Sink



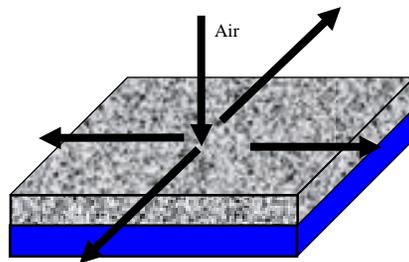
Mass of Sink = 44 g
Temperature = 99°F

Finned Foam
Heat Sink



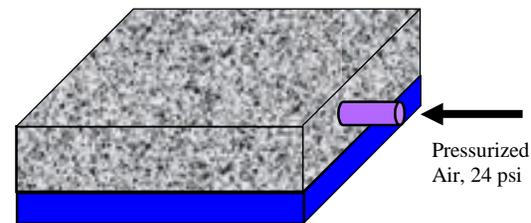
Mass of Sink = 8 g
Temperature = 93°F

Thin Foam
Heat Sink



Mass of Sink = 4 g
Temperature = 103°F

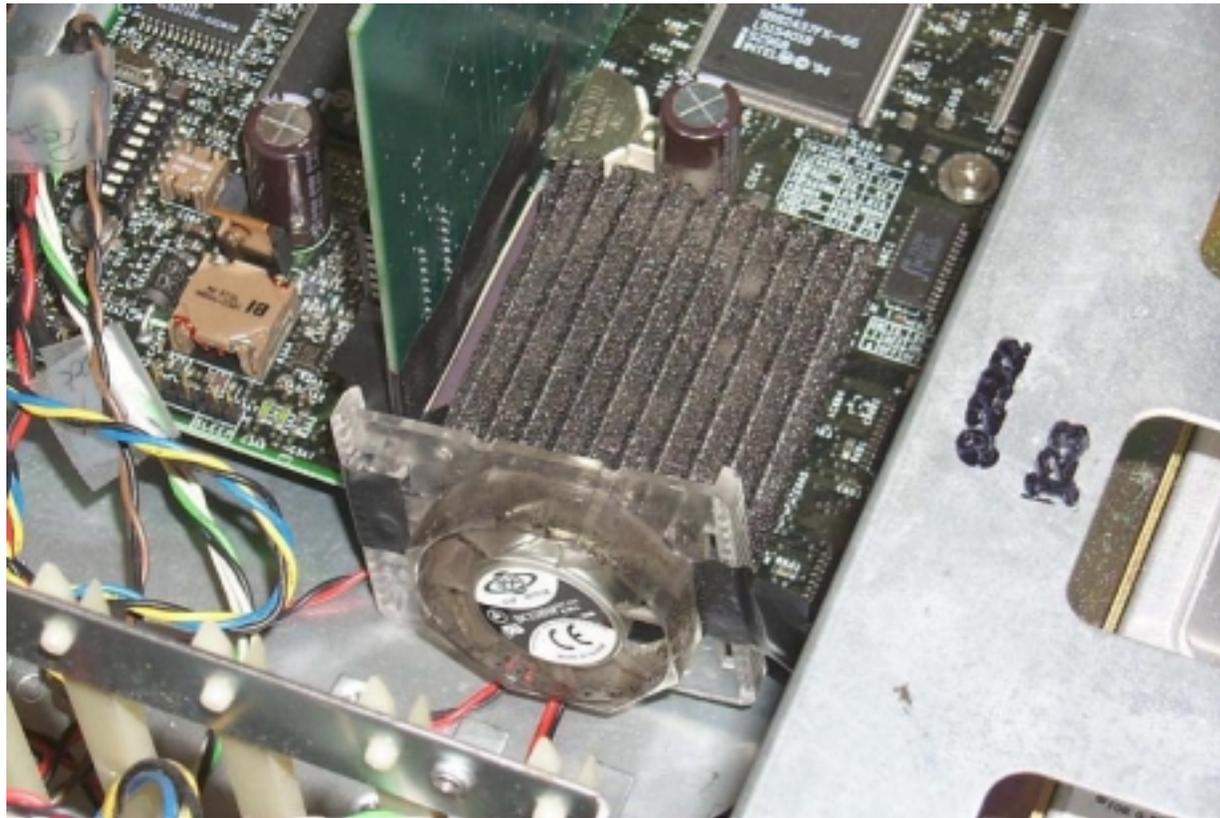
Foam Heat Sink
with Forced Flow



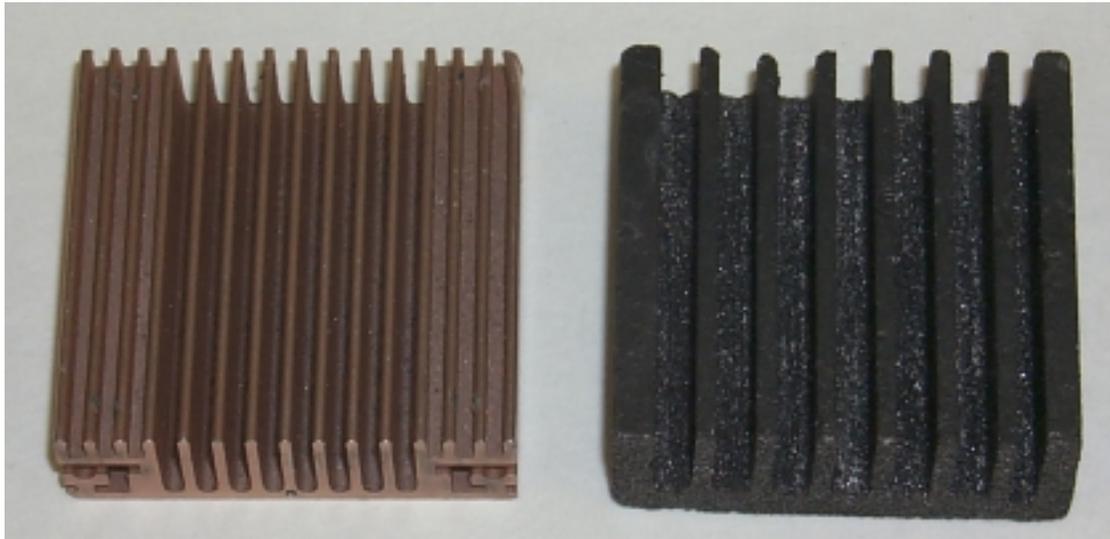
Mass of Sink = 11 g
Temperature = 99°F

Actual devices

- Finned foam heat sink running in Pentium 133 computer since December 12, 1998.

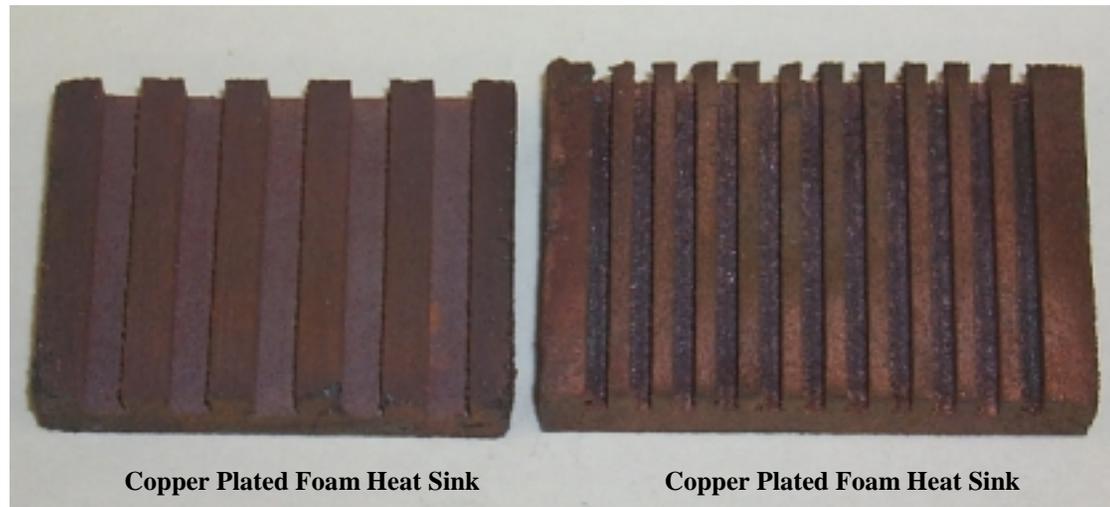


Other Finned Heat Sinks



Aluminum Heat Sink from P133 Computer

Finned Foam Heat Sink

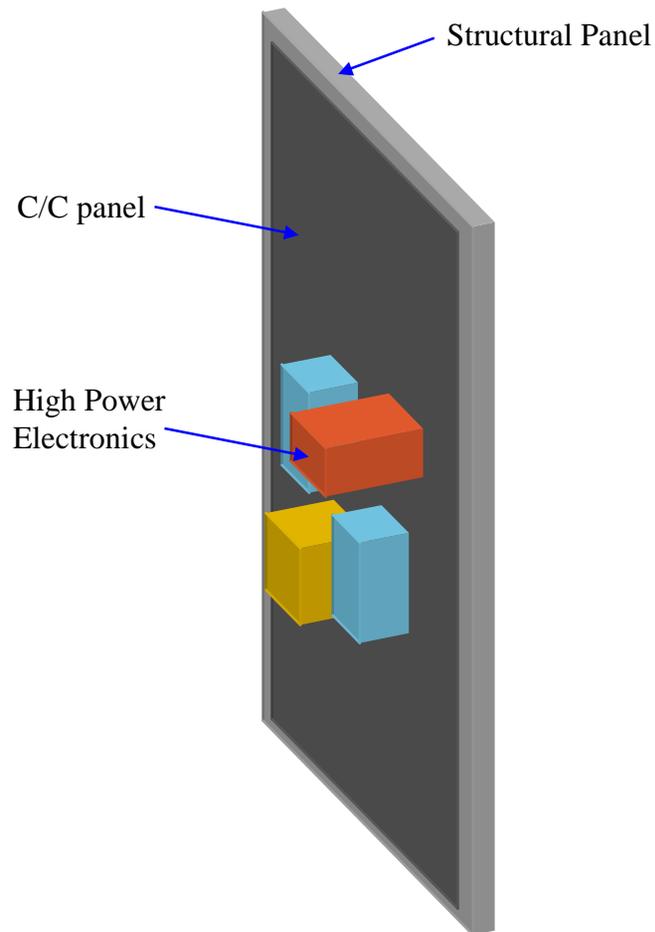


Copper Plated Foam Heat Sink

Copper Plated Foam Heat Sink

Satellite Applications?

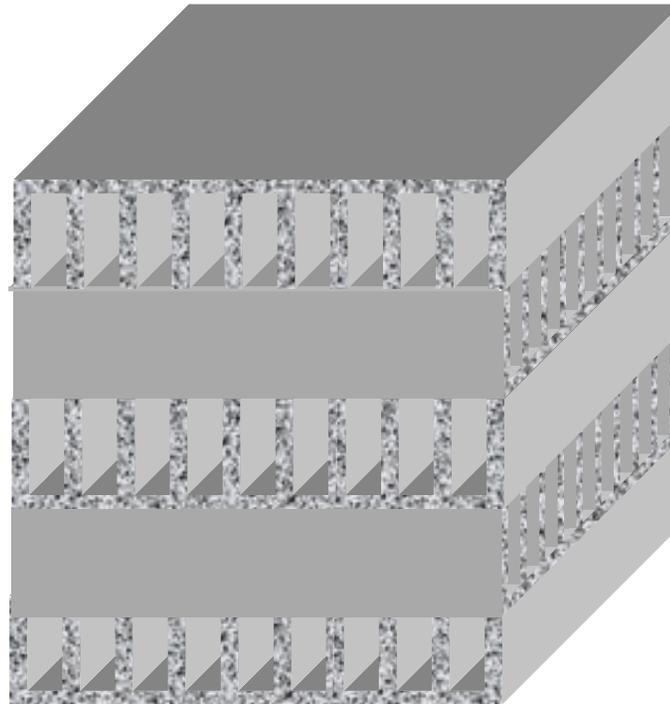
Thermal Doubler Panel



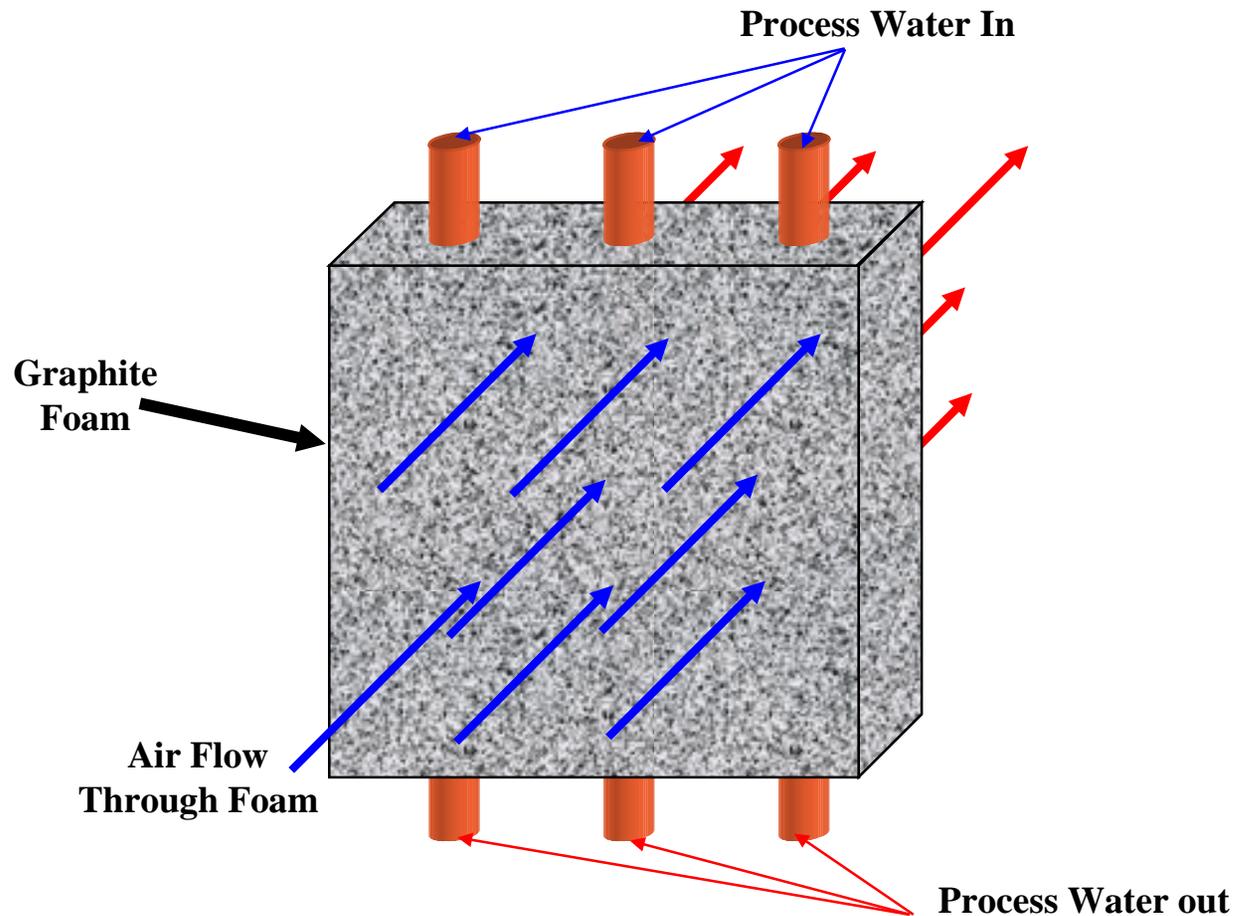
- Current concept spreads heat across larger area & reduces temperature
- Heat is rejected to space with T^4 relationship
- A very low through thickness thermal conductivity of current carbon-carbon (20 W/m·K) and honeycomb core limits heat rejection
- The higher through-thickness thermal conductivity of the foam (180 W/m·K) will increase temperature on outside surface
- High temperature on outside surface will increase radiation
- Smaller panel footprint, or more electronics can be utilized.

Cross Flow Heat Exchangers

- Foam rigidized with Carbon CVI for dramatic improvement in durability
- Surface skin produced during manufacture would become impermeable to H_2 (already demonstrated in Fuel Cell Bi-polar plate testing)
- Can be bonded together or “Glued” together during the CVI Process
 - ⇒ porous structure allowed deposition to bond structure together

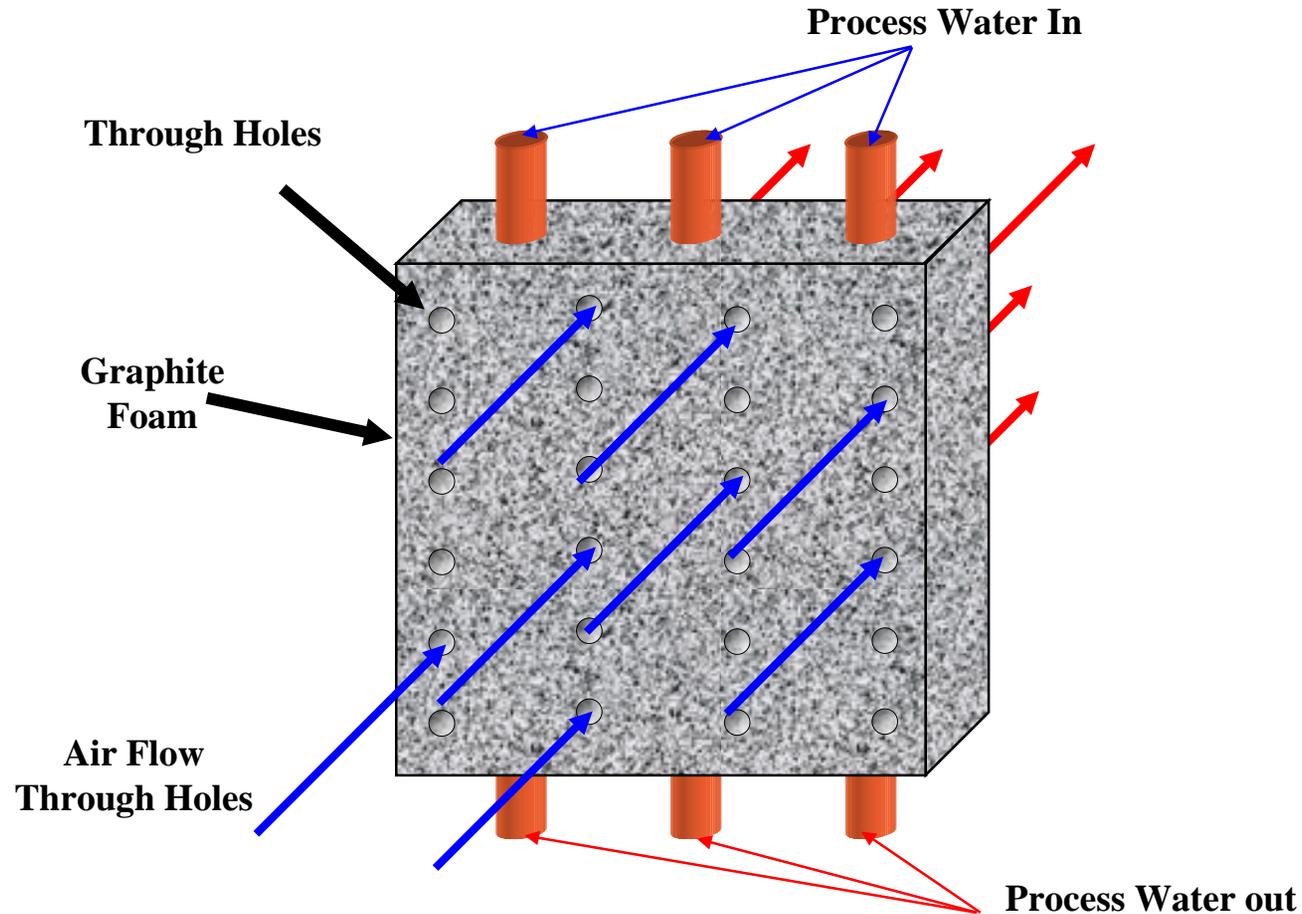


Heat Transport - Forced Diffusion



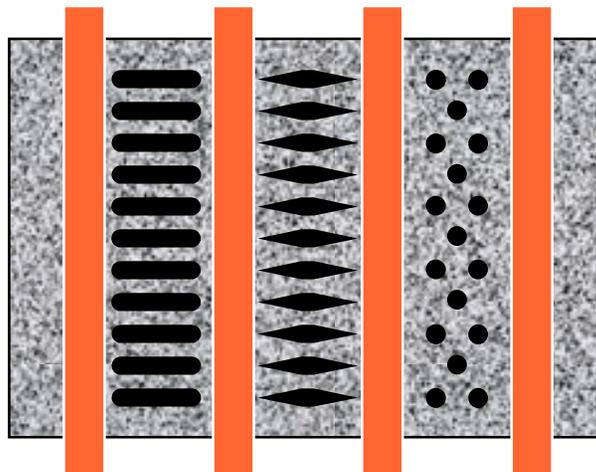
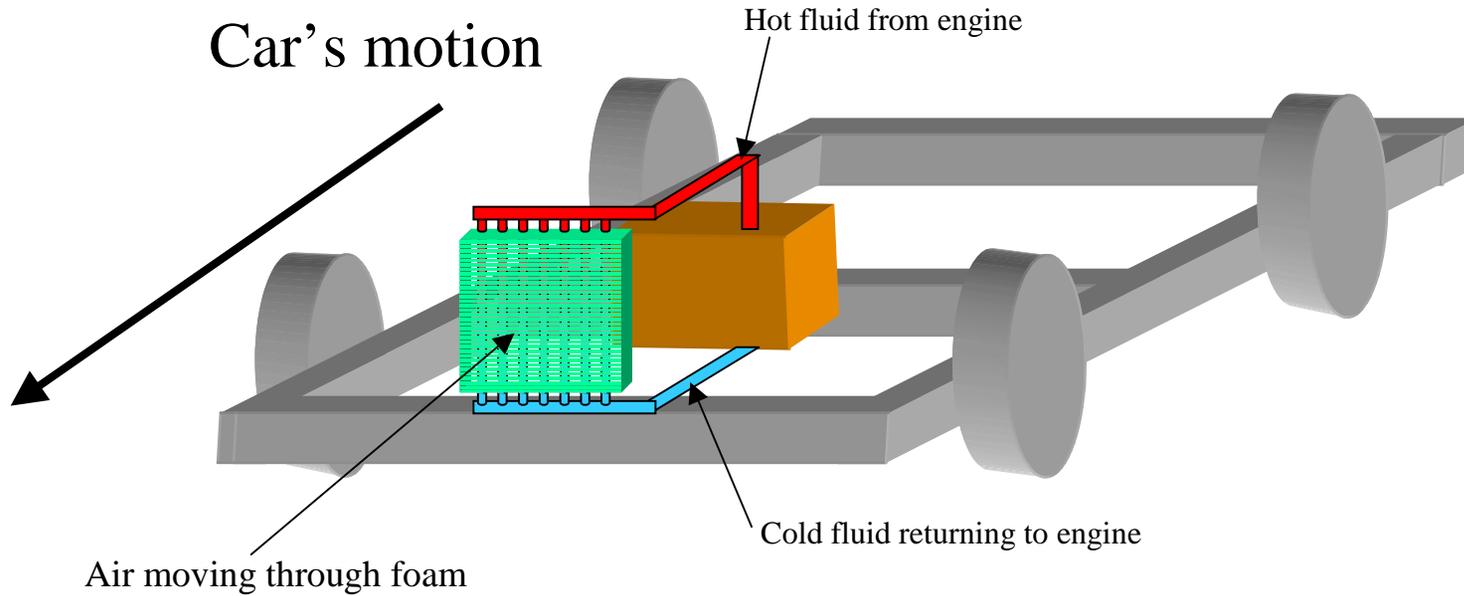
***Measured $U_o = 6,000 - 11,000 \text{ W/m}^2 \cdot \text{K}$ depending on air humidity
an increase by a factor of more than 2 orders-of-magnitude
over typical radiators***

Heat Transport - Forced Convection

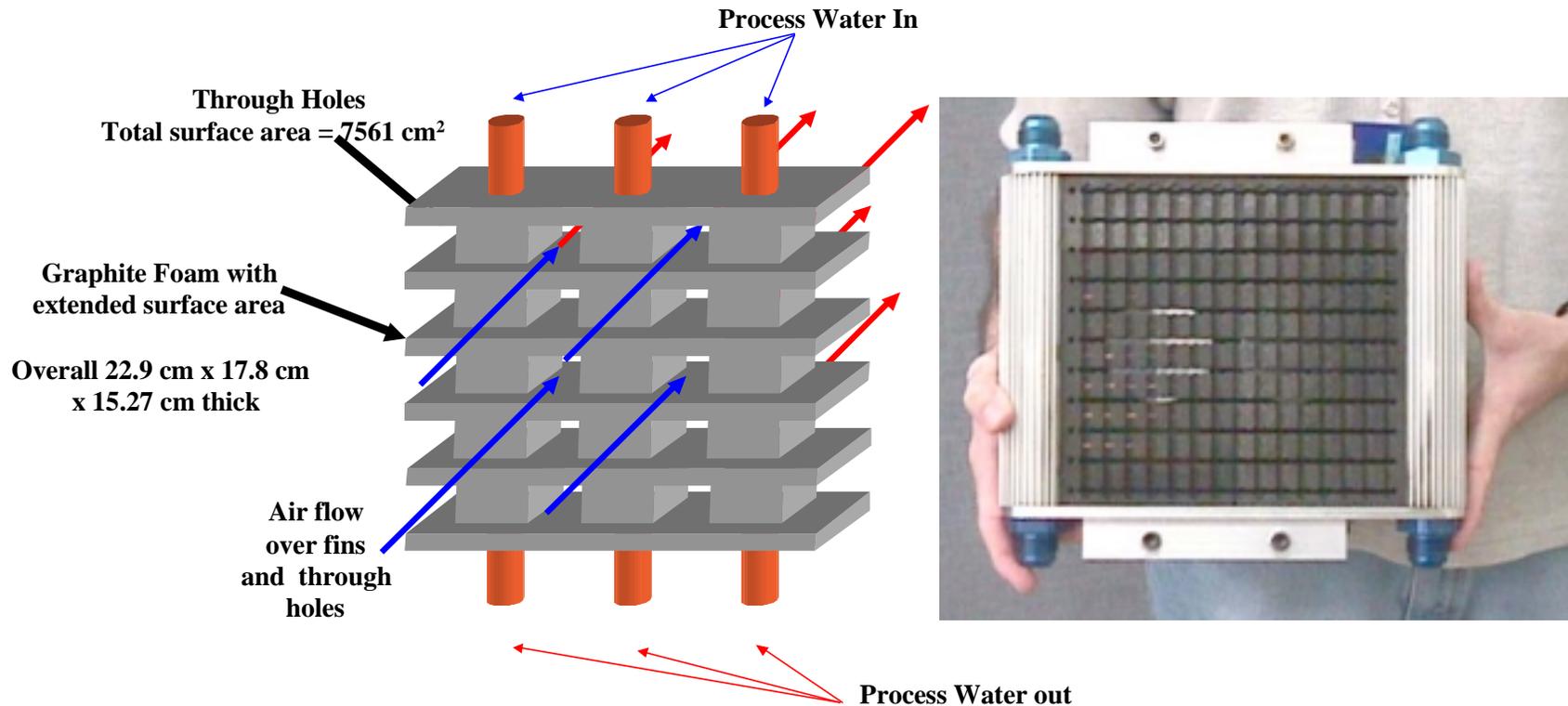


Measured $U_o = 1000 \text{ W/m}^2 \cdot \text{K}$ depending on air humidity
1 order-of-magnitude improvement

Heat Exchangers- Forced Convection



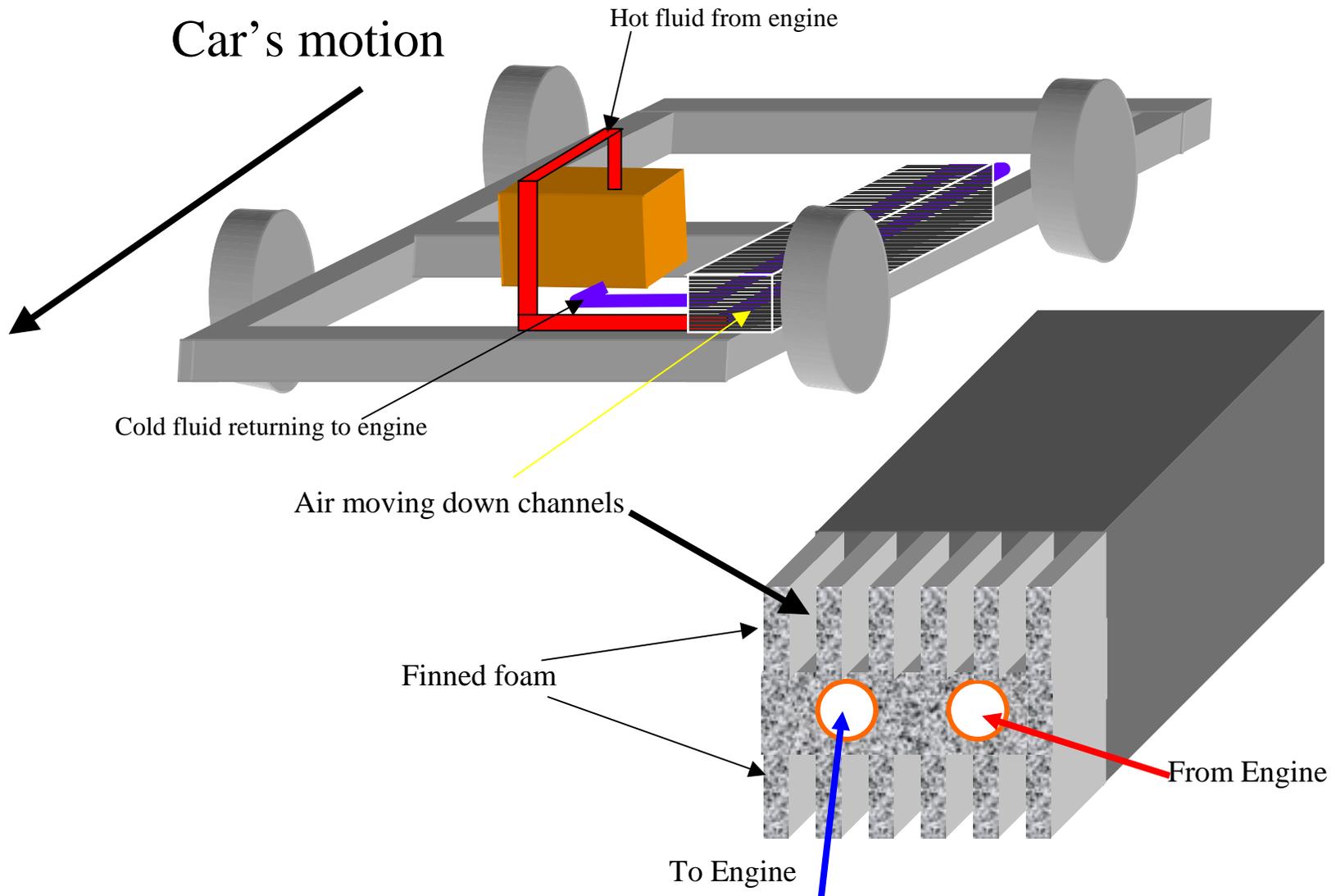
Current Radiator Demonstrated



Measured $U_o = 1000 \text{ W/m}^2 \cdot \text{K}$ depending on air humidity

Similar design tested for 800 hp racing engine

Heat Exchangers- Forced Convection



Energy Balance

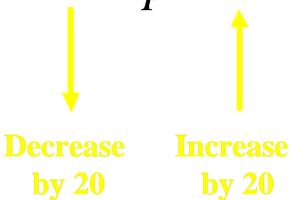
- Current heat exchanger utilize high flow rates and low temperature changes.

$$q = \dot{m} c_p \Delta T$$

⇒ for example: automotive radiator for 150 hp engine

- Current: $\Delta T < 5^\circ\text{F}$
- Target: $\Delta T \sim 100^\circ\text{F}$
 - ◆ radiator fluid temperature cannot fall below $\sim 200^\circ\text{F}$
- Allows for a decrease in mass flow (\dot{m}) of air by a factor of at least 20.

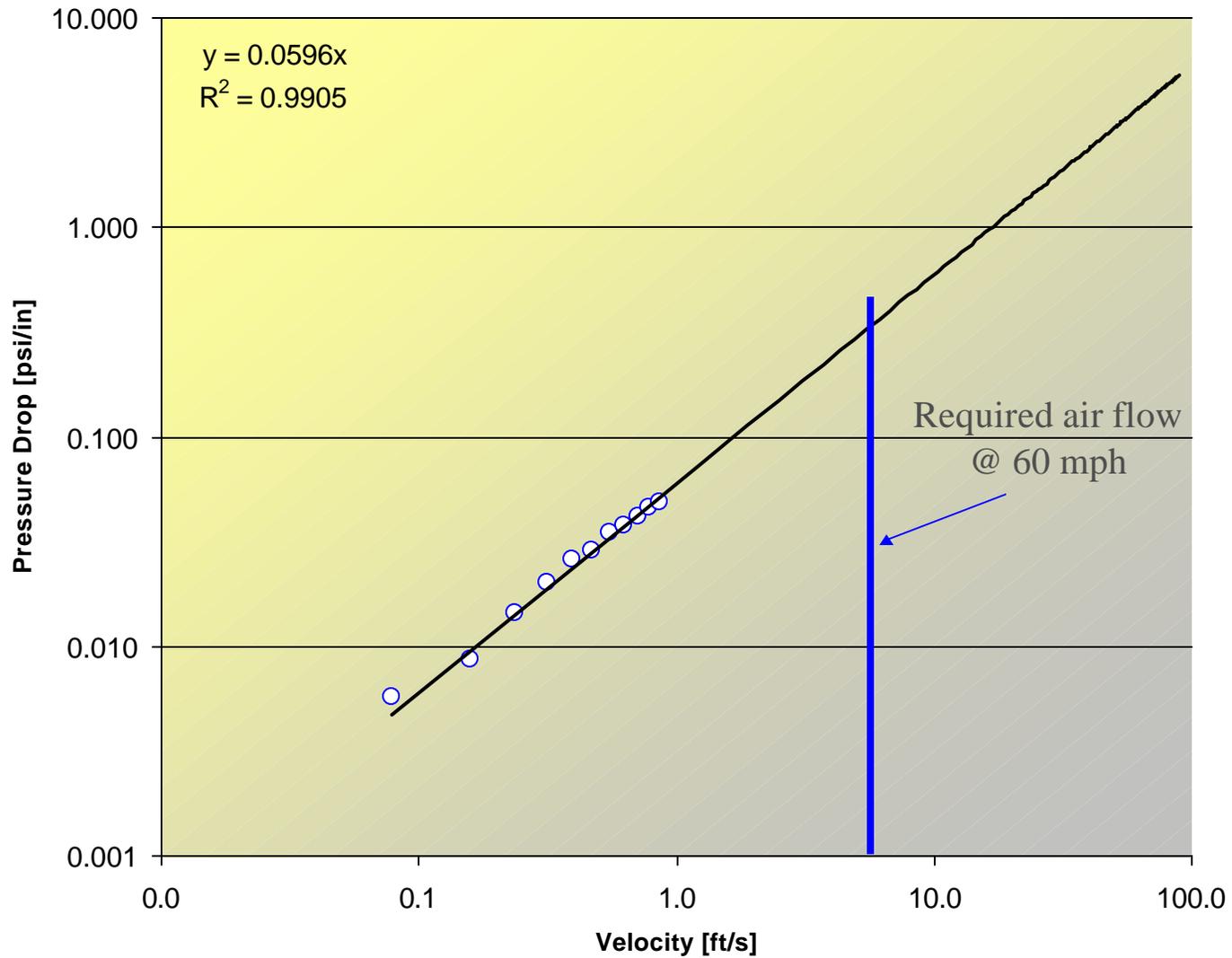
$$q = \dot{m} c_p \Delta T$$



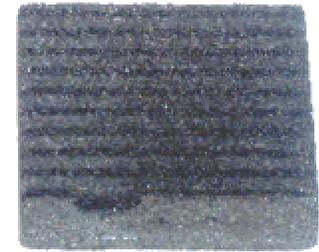
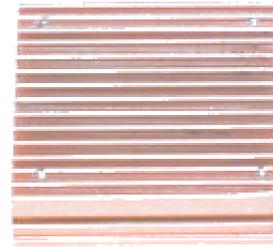
Decrease
by 20

Increase
by 20

Pressure drop through graphitic foam



Workability



Heat Resistant Composites



Standard Polymer



Foam/Polymer

Conclusions

- By engineering process of producing pitch foams, thermal conductivity can be varied with density to achieve desired targets
- Light weight materials with thermal conductivities as high as aluminum can be produced
- Porous media heat exchangers can be designed that are dramatically smaller
- Out-of-the-Box designs can be used for the development of novel and radically different heat exchange devices
- Laminated foams can be used for structural members where high thermal conductivity and light weight are necessary.

Acknowledgements

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