

# High Field Magnet Development and Prospects for an Energy Upgrade of the LHC



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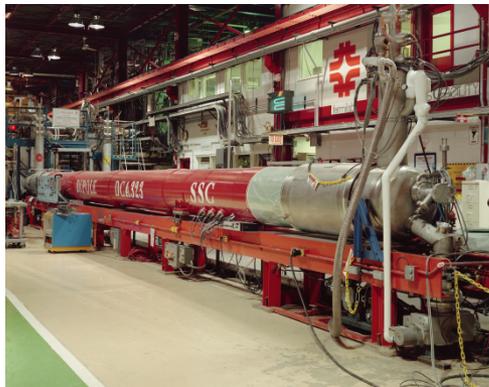
# Accelerator Magnets

## Then . . .

- The Tevatron (Fermilab) 1983
  - 4.4 T , NbTi, 4.2K

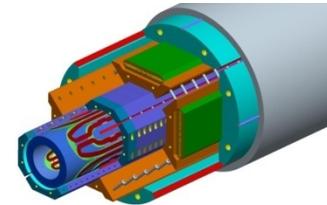


- HERA, SSC, UNK, RHIC



## And now . . .

- LHC 2007
  - 8.3 T , NbTi, 1.9K
  - Limit of NbTi
- US LHC Upgrade
  - Nb<sub>3</sub>Sn quadrupoles
- FAIR
  - High ramp-rate



# CERN Accelerator Strategy



- CERN is the energy frontier laboratory
- We have (almost)
  - LHC at 7 TeV/beam; the highest energy collider on the planet for the foreseeable future
  - HL-LHC; proposed luminosity upgrade for installation 2020-2021 and operating until around 2030 (including the upgrade of the LHC Injectors)

## High-priority large-scale scientific activities (2)

Roy Aleksan  
CERN  
Feb. 22, 2013

### Recommendation #2

d) To stay at the forefront of particle physics, Europe needs to be in a position to propose an ambitious post-LHC accelerator project at CERN by the time of the next Strategy update, when physics results from the LHC running at 14 TeV will be available. *CERN should undertake design studies for accelerator projects in a global context, with emphasis on proton-proton and electron-positron high-energy frontier machines. These design studies should be coupled to a vigorous accelerator R&D programme, including high-field magnets and high-gradient accelerating structures, in collaboration with national institutes, laboratories and universities worldwide.*

# So, what's new?



- LHC Energy Upgrade is now a topic of considerable discussion

EuCARD Workshop on a High Energy LHC

Malta

October 14, 2010

Joint Snowmass-EuCARD/AccNet-HiLumi LHC Workshop

CERN

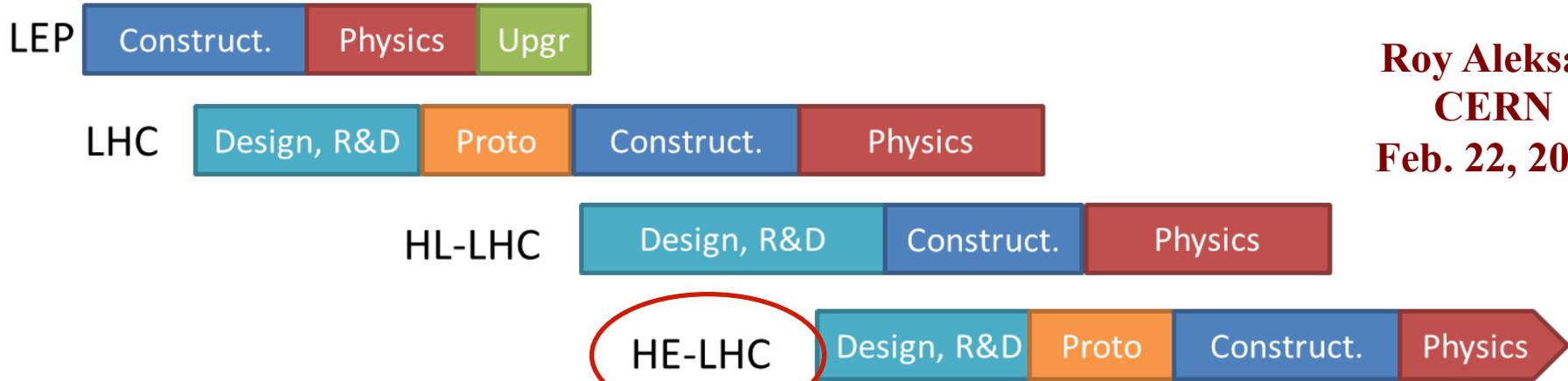
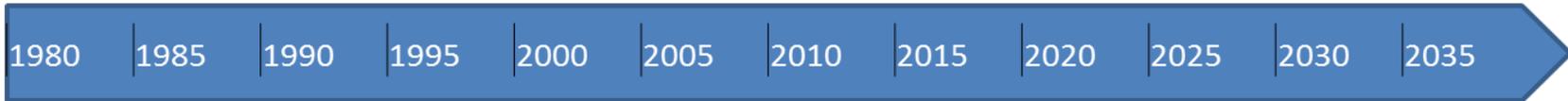
February 21-22, 2013

[Contributing to the interest . . .](#)

LBNL Magnet R&D Program in High Field Magnets

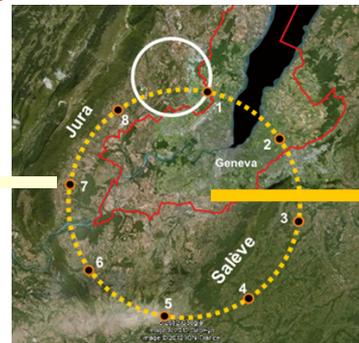
LHC Accelerator R&D Program (LARP)

# The super-exploitation of the CERN complex: Injectors, LEP/LHC tunnel, infrastructures



**Roy Aleksan**  
**CERN**  
**Feb. 22, 2013**

**Either using existing LEP/LHC tunnel to reach 26-32 TeV collisions**



**Or build (or reuse) an 80km tunnel to reach 80-100 TeV collisions**  
⇒ **more detailed study of such a tunnel needed**

**In both cases, SC challenge to develop 16-20 Tesla magnets!  
Magnets for HL\_LHC is an indispensable first step**

# HE-LHC Parameters



	nominal LHC	HE-LHC	
beam energy [TeV]	7	16.5	
dipole field [T]	8.33	20	
dipole coil aperture [mm]	56	40	
beam half aperture [cm]	2.2 (x), 1.8 (y)	1.3	
injection energy [TeV]	0.45	>1.0	
#bunches	2808	1404	
bunch population [ $10^{11}$ ]	1.15	1.29	1.30
initial transverse normalized emittance	3.75	3.75 (x), 1.84 (y)	2.59 (x & y)
initial longitudinal emittance [eVs]	2.5	4.0	
number of IPs contributing to tune shift	3	2	
initial total beam-beam tune shift	0.01	0.01 (x & y)	
maximum total beam-beam tune shift	0.01	0.01	
beam circulating current [A]	0.584	0.328	
RF voltage [MV]	16	32	
rms bunch length [cm]	7.55	6.5	
rms momentum spread [ $10^{-4}$ ]	1.13	0.9	
IP beta function [m]	0.55	1 (x), 0.43 (y)	0.6 (x & y)
initial rms IP spot size [ $\mu\text{m}$ ]	16.7	14.6 (x), 6.3 (y)	9.4 (x & y)
full crossing angle [ $\mu\text{rad}$ ]	285 (9.5 $\sigma_{x,y}$ )	175 (12 $\sigma_{x0}$ )	188.1 (12)
Piwiński angle	0.65	0.39	0.65
geometric luminosity loss from crossing	0.84	0.93	0.84
stored beam energy [MJ]	362	478.5	480.7
SR power per ring [kW]	3.6	65.7	66.0
arc SR heat load dW/ds [W/m/aperture]	0.17	2.8	2.8
energy loss per turn [keV]	6.7	201.3	
critical photon energy [eV]	44	575	
photon flux [ $10^{17}/\text{m/s}$ ]	1.0	1.3	
longitudinal SR emittance damping time [h]	12.9	0.98	
horizontal SR emittance damping time [h]	25.8	1.97	
initial longitudinal IBS emittance rise time	61	64	~68
initial horizontal IBS emittance rise time [h]	80	~80	~60
initial vertical IBS emittance rise time [h]	~400	~400	~300
events per crossing	19	76	
initial luminosity [ $10^{34} \text{ cm}^{-2} \text{ s}^{-1}$ ]	1.0	2.0	
peak luminosity [ $10^{34} \text{ cm}^{-2} \text{ s}^{-1}$ ]	1.0	2.0	
beam lifetime due to $p$ consumption [h]	46	12.6	
optimum run time $t_r$ [h]	15.2	10.4	
integrated luminosity after $t_r$ [ $\text{fb}^{-1}$ ]	0.41	0.50	0.51
opt. av. int. luminosity per day [ $\text{fb}^{-1}$ ]	0.47	0.78	0.79

Consider:

*Round case*

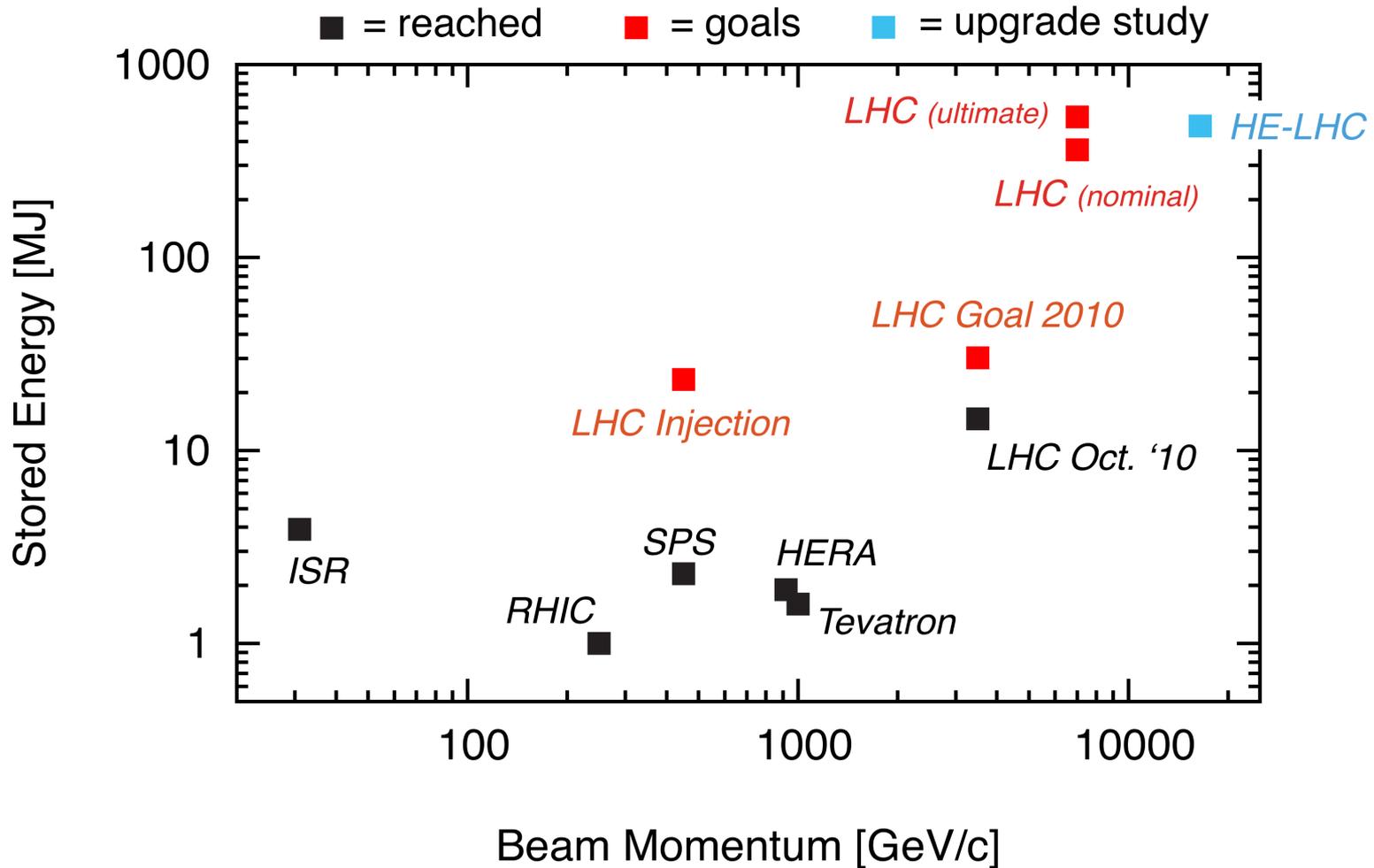
*Compare to nominal LHC*

*Typical collimator location  $\beta = 80\text{m}$*

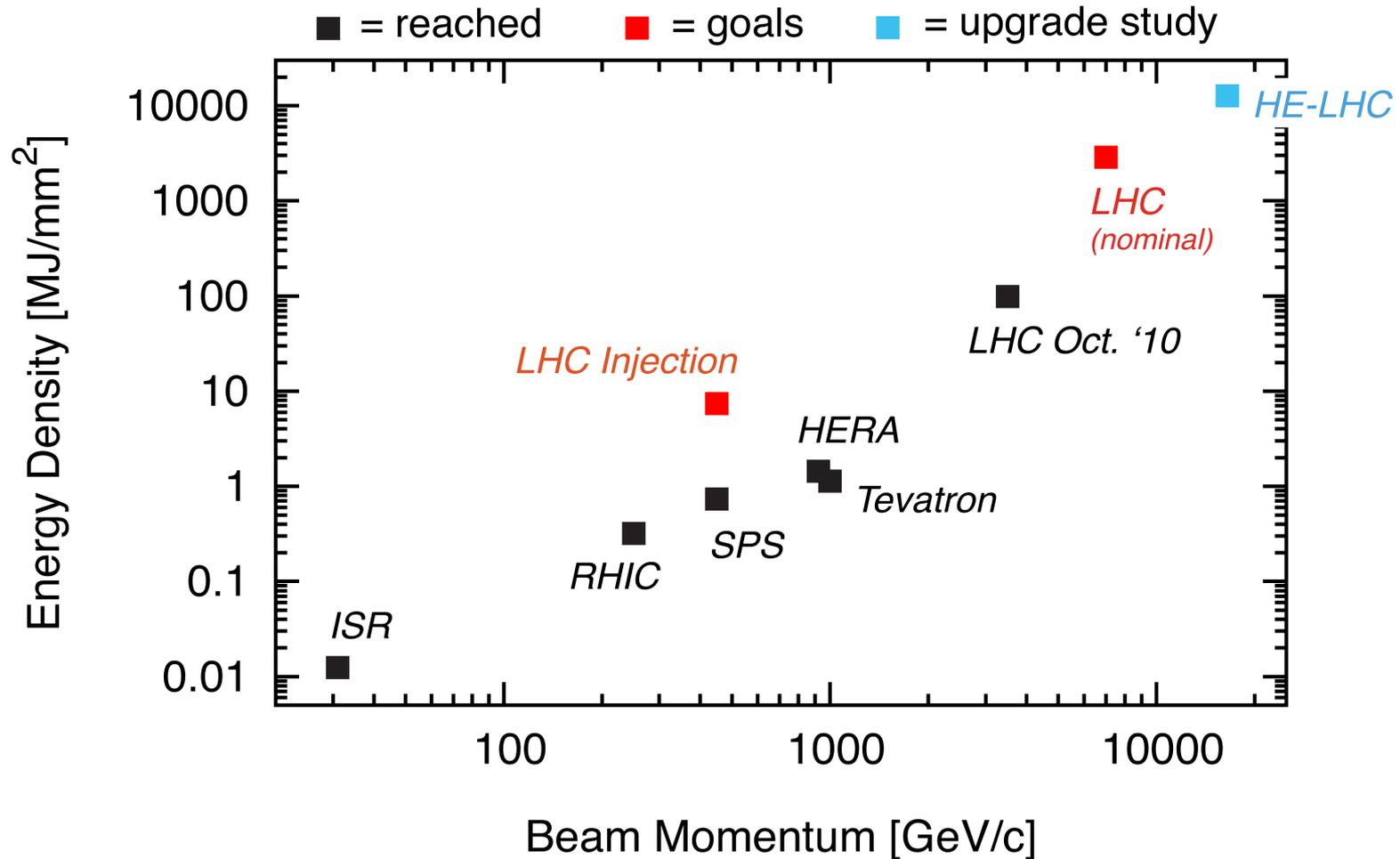
## Main issues:

	Nominal	Upgrade
E	7.0 TeV	16.5 TeV
$\gamma$	7461	17587
$\epsilon$	0.5 nm	<b>0.15 nm</b>
$E_{\text{stored}} (\text{tot})$	362 MJ	482 MJ
$\rho_e (\text{tot})$	2.9 GJ/mm <sup>2</sup>	15.4 GJ/mm <sup>2</sup>
$E_{\text{stored}} (1\text{b})$	128 kJ	242 kJ
$\rho_e (1\text{b})$	1.0 MJ/mm <sup>2</sup>	<b>7.7 MJ/mm<sup>2</sup></b>

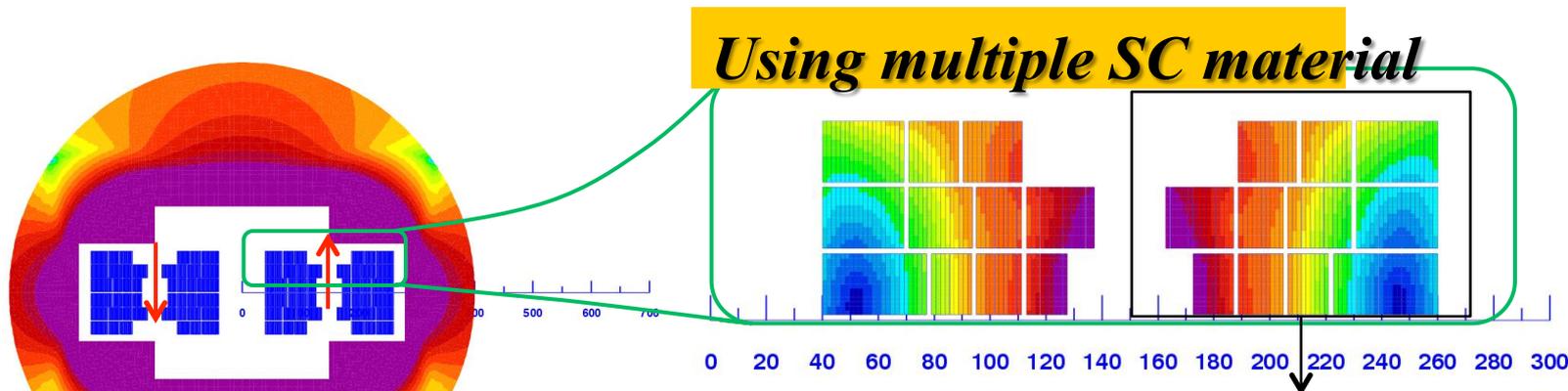
# Stored Energy



# Energy Density



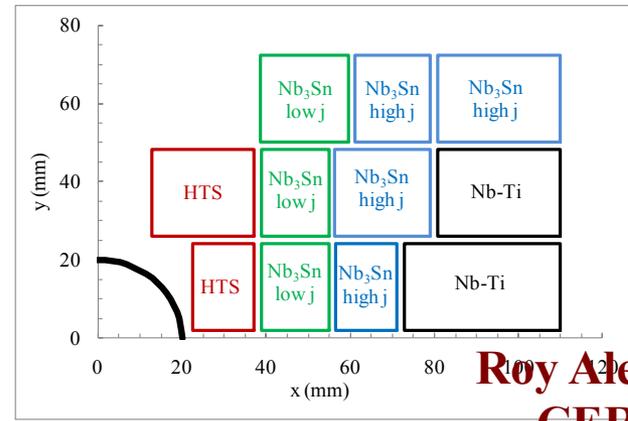
# First consistent conceptual design



L.Rossi

Material	N. turns	Coil fraction	Peak field	$J_{\text{overall}}$ (A/mm <sup>2</sup> )
Nb-Ti	41	27%	8	380
Nb3Sn (high Jc)	55	37%	13	380
Nb3Sn (Low Jc)	30	20%	15	190
HTS	24	16%	20.5	380

**20 T field!**



**Roy Aleksan  
CERN  
Feb. 22, 2013**

Magnet design: 40 mm bore (depends on injection energy: > 1 Tev)  
 Approximately 2.5 times more SC than LHC: 3000 tonnes! (~4000 long magnets)  
 Multiple powering in the same magnet for FQ (and more sectioning for energy)  
 Only a first attempt: cosθ and other shapes needs to be also investigated

# Some Magnet Background to Establish a Baseline

# Accelerator Magnet Design Drivers



- **Performance**
  - **Field Quality – higher order poles on order of  $10^{-4}$  of primary field**
    - Precise placement of conductor
  - **Field – higher fields usually desirable in most all applications**
    - Especially for LHC Energy Upgrade (Fixed tunnel circumference)
    - High stress – support structures
  - **Large number of magnets with highly reproducible characteristics**
- **Cost**
  - **Typically dominant component of facility**
    - **Magnets for SSC > 60% of total**

**Leads to . . .**

# Magnet/System Cost



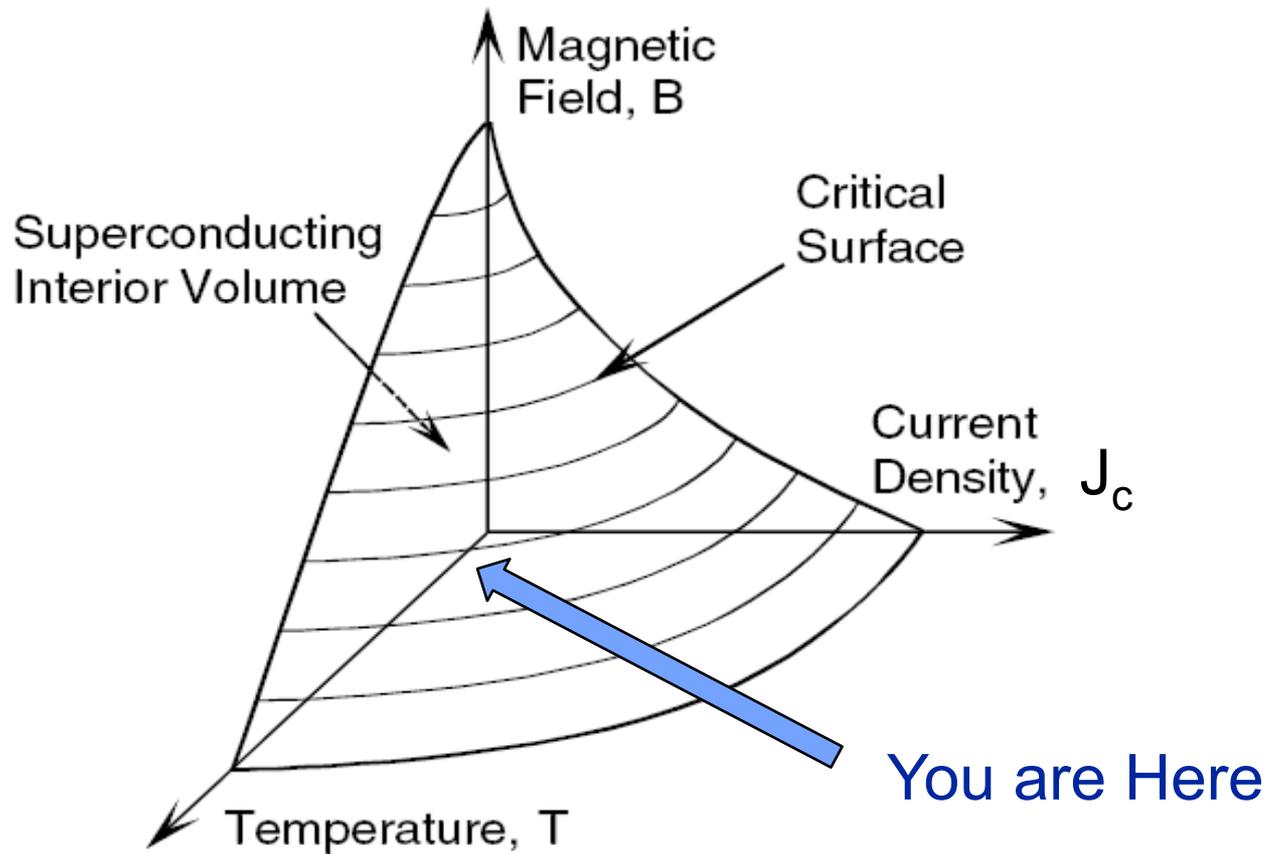
- Number of magnets (fewer, longer)
- Quantity of conductor (> 30% of cost) **Keep an eye on this!**
  - **Small Bore (compact design) order of 10' s of mm**
    - Very high current density
- Stored energy in MJ' s, but strings of magnets raise total
  - **Require active quench protection**
    - Design for quench (heaters, by-pass diodes)
- Operating currents
  - **10 – 30 kA**

# Conductors for Accelerator Magnets

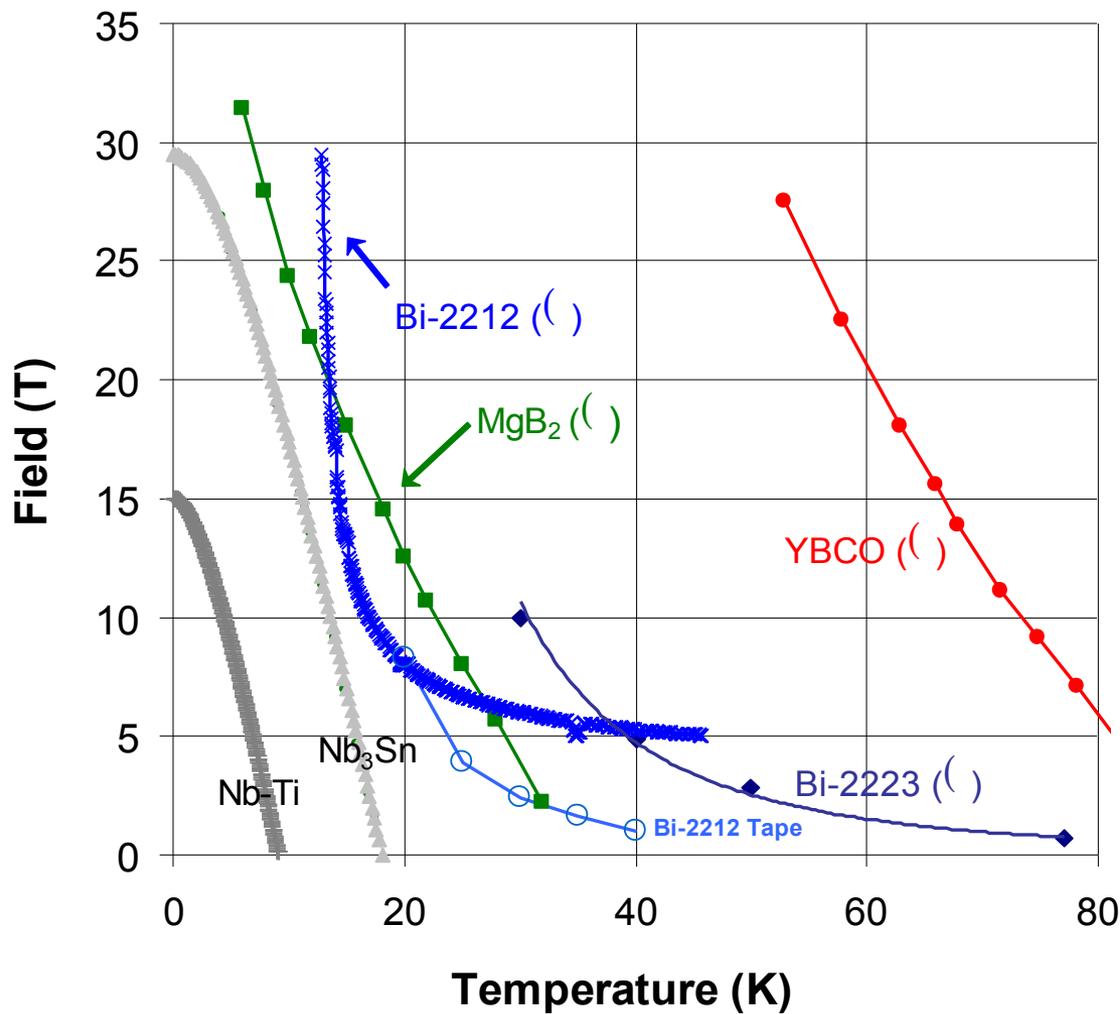


- **Conductor ultimately determines magnet performance**
  - You can't do any better than the virgin conductor
  - But . . . you can do worse!
- **With few exceptions all accelerator magnets use Rutherford-style cables**
  - Multi-strand – reduce strand length, fewer turns (lower inductance)
  - High current density
  - Precise dimensions – controlled conductor placement (field quality)
  - Current redistribution – stability
  - Twisting to reduce interstrand coupling currents (field quality)

Let's start with the materials . . .

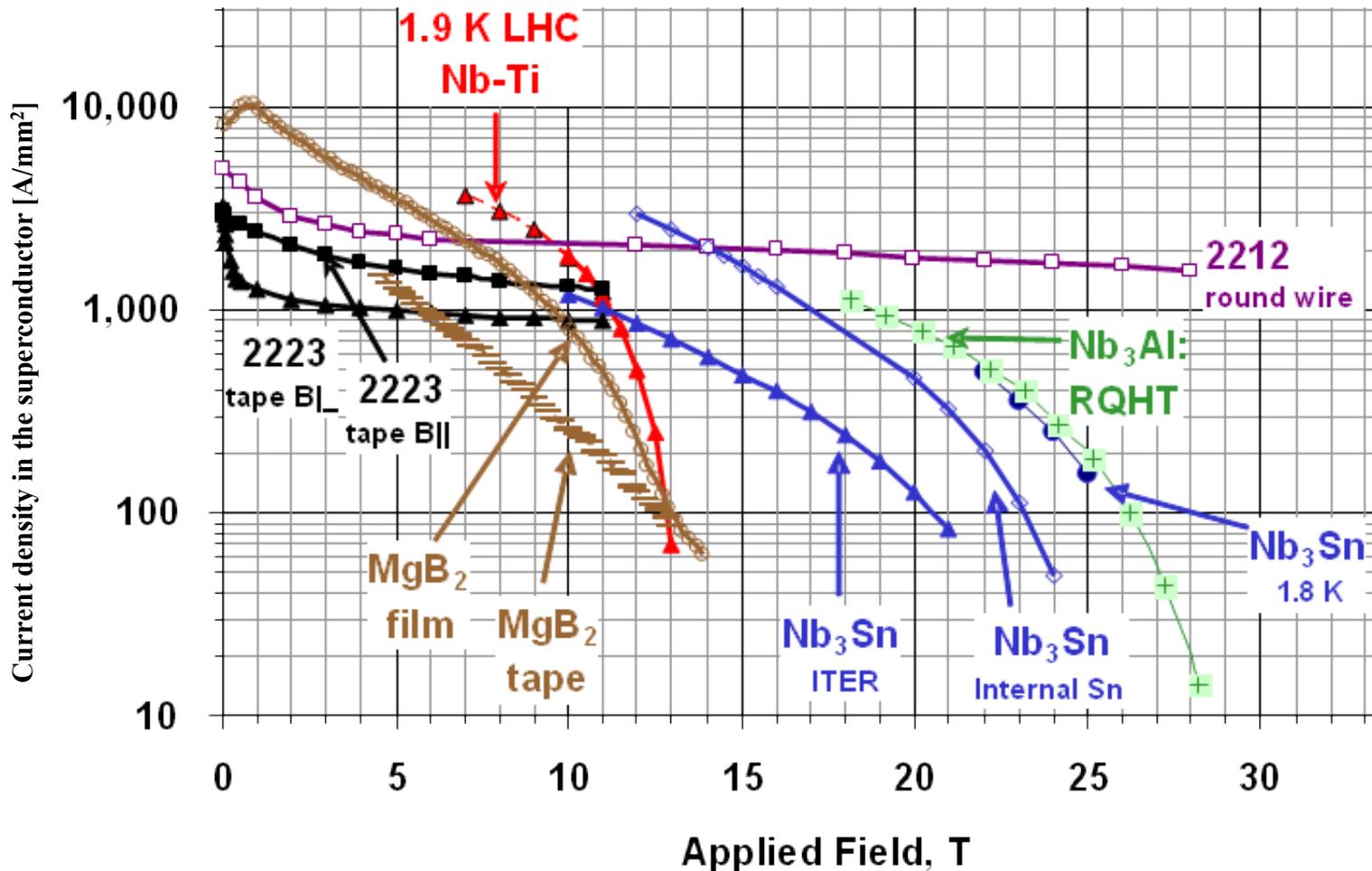


# Field vs Temperature



Courtesy D. Larbalestier, Applied Superconductivity Center  
at the National High Magnetic Field Laboratory, FSU

# Critical Current Density ( $J_c$ ) vs Field



Courtesy of P.J. Lee, Applied Superconductivity Center  
at the National High Magnetic Field Laboratory, FSU

# Options for Fields above 18T



YBCO: Looks great on paper but . . .

Tape only, low engineering current density,

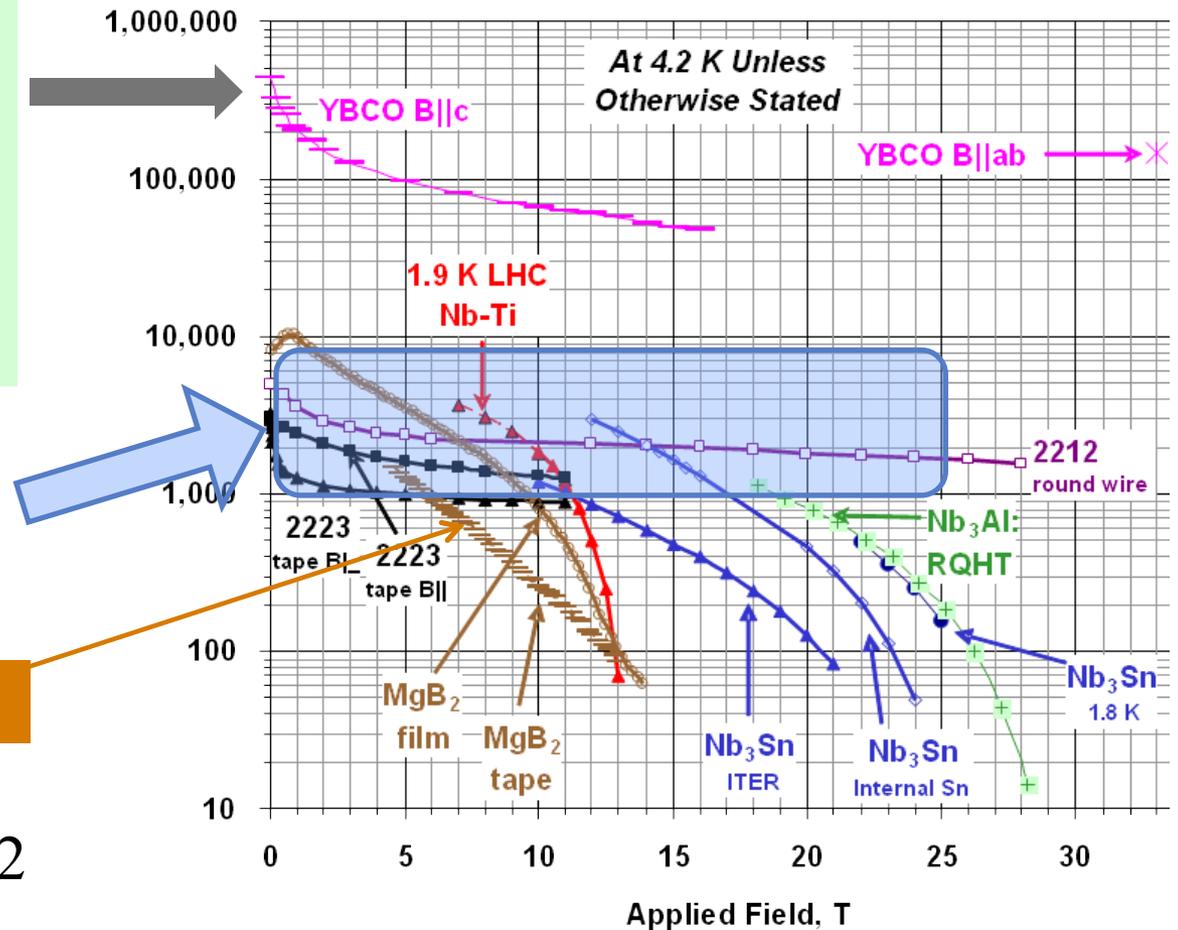
really, really expensive

Maybe in the next talk

Region of interest is where  $J_c > 1000 \text{ A/mm}^2$

Forget  $\text{MgB}_2$  (for 3-5 years)

Best candidate is Bi-2212



# Materials for Accelerator Magnets



Application/performance



material properties and engineering

## • NbTi

- $B_{c2} (0K) \sim 14 \text{ T}$
- $T_c (0K) \sim 9.5 \text{ K}$ 
  - Max practical field at 4.2 K is 7 T (9 T @ 1.8 K)
  - Excellent mechanical properties

## • Nb<sub>3</sub>Sn

- $B_{c2} (4.2 \text{ K}) \sim 23 - 24 \text{ T}$
- $T_c (0T) \sim 18 \text{ K}$ 
  - Max practical field 17 – 18 T?
  - Brittle and strain sensitive

## • Nb<sub>3</sub>Al

- High  $J_c$  in magnetic field  $< 15 \text{ T}$
- Mechanical toughness
- Actively pursued in Japan
  - National Institute for Materials Science (NIMS)
  - Rapid-quench process requires later addition of stabilizer

# Materials for Accelerator Magnets



Application/performance



material properties and engineering

- **Bi-2212**

- Round strands in long lengths
- Requires 900 °C heat treatment
- Strain sensitive

- **Bi-2223**

- Tapes in long lengths
- Applications for high temperature

- **YBCO**

- High critical current but length is a problem
- Tapes (not wires!)
- Lousy engineering current density
- Really Expensive

- **MgB<sub>2</sub> (not so HT HTS)**

- Better at T < 25K
- Anisotropic
- Low J<sub>c</sub> (so far)
- Stabilization

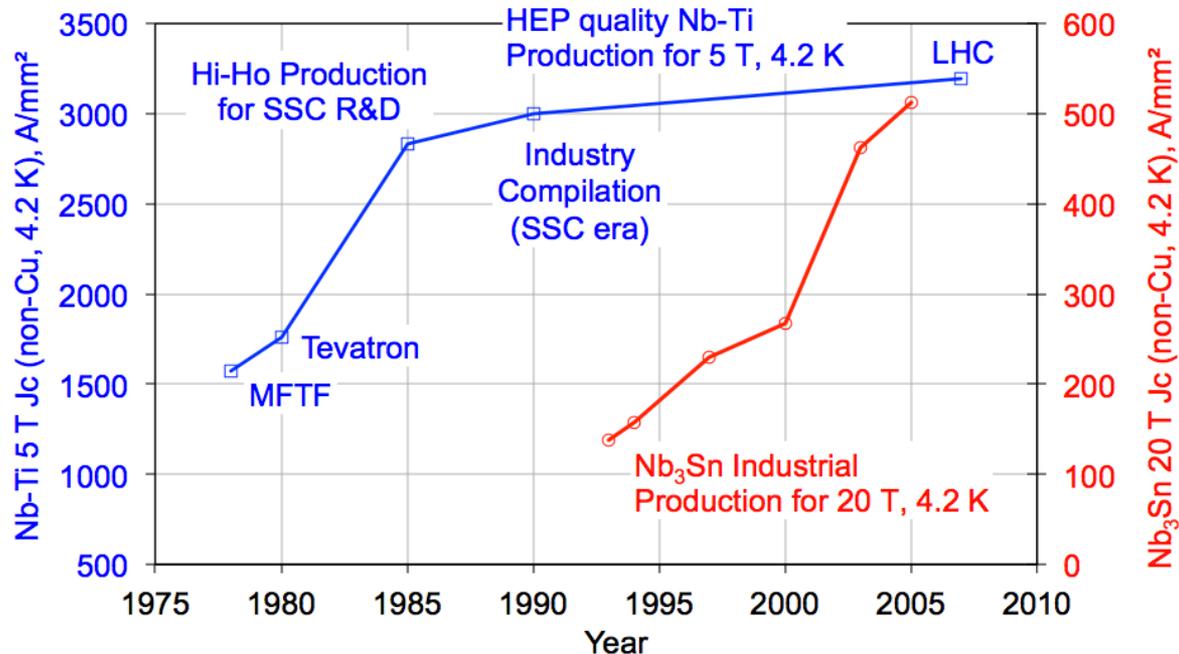
But . . .

- Potential to exceed H<sub>c2</sub> of Nb<sub>3</sub>Sn
- Low cost materials
- Leading candidate for LHC Lumi upgrade (SC cables)

# Where are we with Nb<sub>3</sub>Sn?



- Nb<sub>3</sub>Sn performance has greatly improved (doubled in ten years)
- Can we expect more?

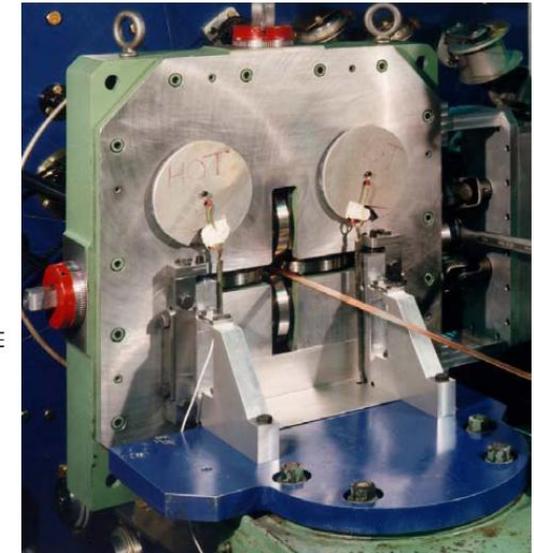
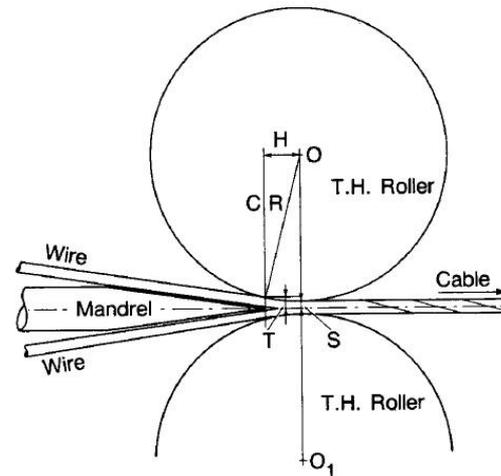
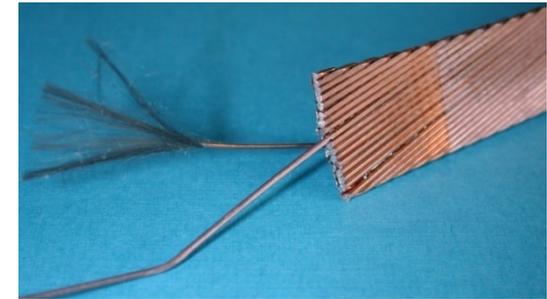


An historical view on the improvement of Nb-Ti and Nb<sub>3</sub>Sn performance [L. Bottura, ASC 2012]

# Rutherford Cables

- Cable cross-section is rectangular or trapezoidal
- Packing Fraction (PF) ranges from 85% - 92%
  - Too much compaction – damage to filaments
  - Too little compaction – mechanically unstable

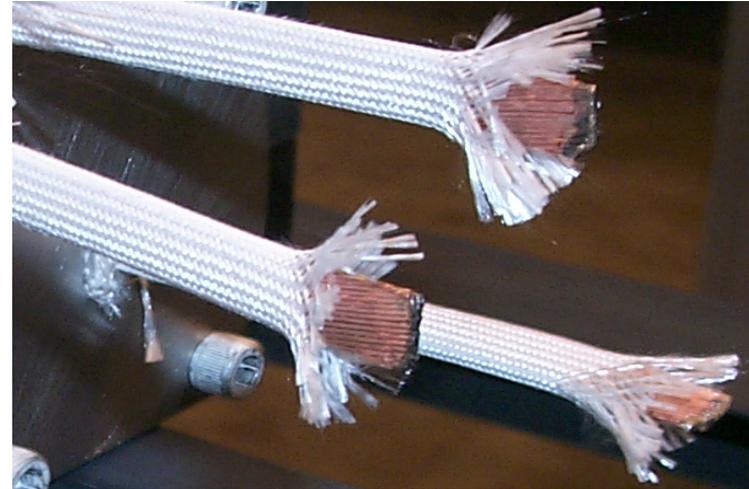
$$PF_{cable} = \frac{N_{wire} \pi d_{wire}^2}{4w_{cable} t_{cable} \cos \psi_{cable}}$$



# Engineering Current Density

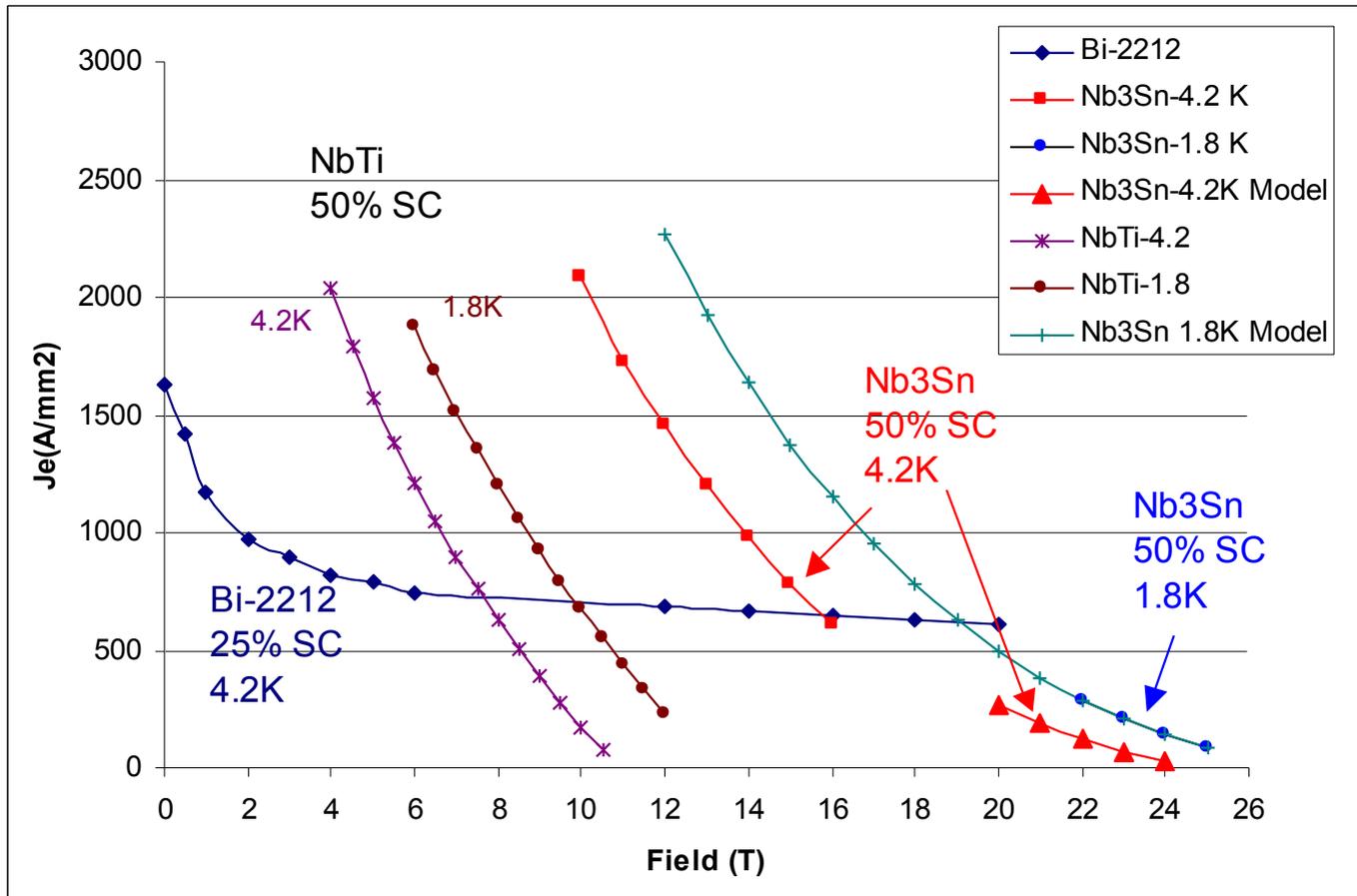


- **Start with  $J_c$  of Superconductor**
  - NbTi ~ 3,000 A/mm<sup>2</sup> @ 5T and 4.2K
  - Nb<sub>3</sub>Sn ~ 3,000 A/mm<sup>2</sup> @ 12T and 4.2K
- **Add copper/non-Superconductor**
  - Typically ~50%
- **Cable compaction ~88%**
- **Insulation – order of 100 microns (X2) compared to ~2 mm cable thickness**
- **Filling factor ( $\kappa$ ) =  $(N_{wire} A_{sc})/A_{ins\_cable}$**
- **Engineering current density defined as  $J_e = \kappa J_c$** 
  - Typically on the order of 1,000 A/mm<sup>2</sup>



# Magnet Conductor Comparison

## $J_e$ is what counts



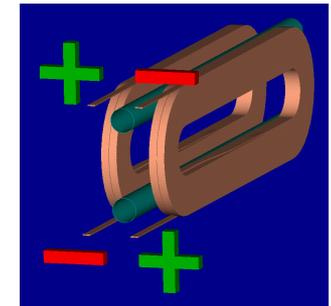
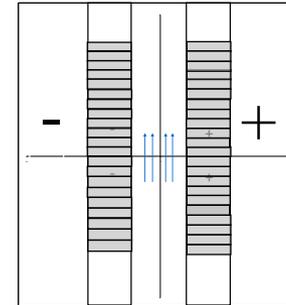


# Electromagnetic design

# Start with Ideal Case for Dipole Field

- **Uniform current walls**

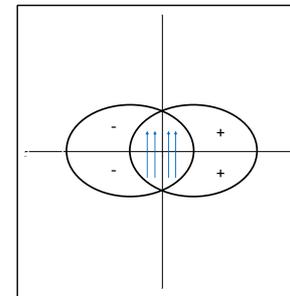
- Easy to wind but the height is infinite
- Practical implementation requires . . .
  - High aspect ratio
  - Modification of ends



BNL “Common Coil”

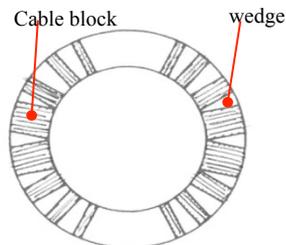
- **Intersecting Ellipses**

- Non-circular aperture
- Requires internal support structure

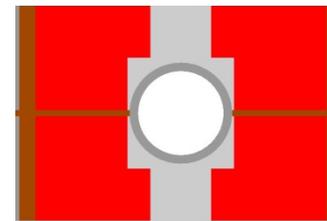


- **Cos $\theta$  current distribution**

- Circular aperture, self-supporting
- Reasonably easy to reproduce in practical configurations



A practical winding with one layer and wedges  
[from M. N. Wilson, pg. 33]



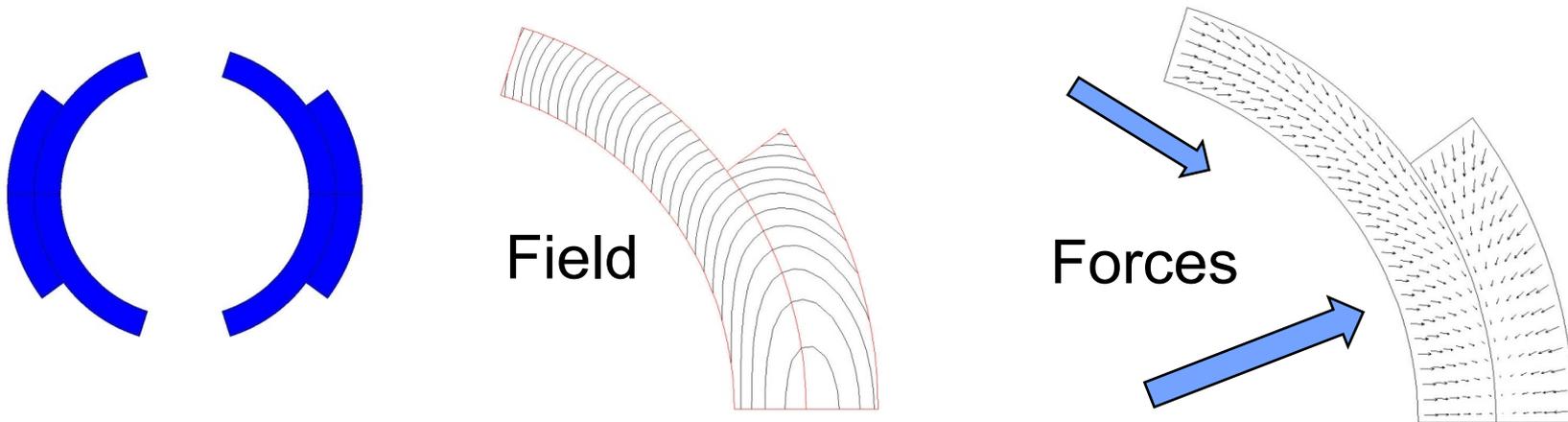
Block Coil Implementation  
LBNL “HD-2”

# Forces, Stresses and Structures

# Lorentz Forces in Dipoles



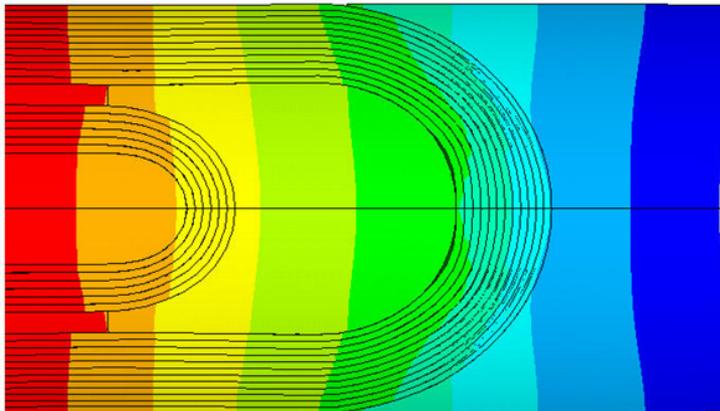
- Coils are subjected to large forces due to high current densities and high fields
  - **Must prevent coil motion/deformation**
    - Field quality good to  $\sim 1$  part in  $10^4$  (conductor positioning to 25 microns)
    - Restrict motion to prevent conductor going normal (“Quench”)



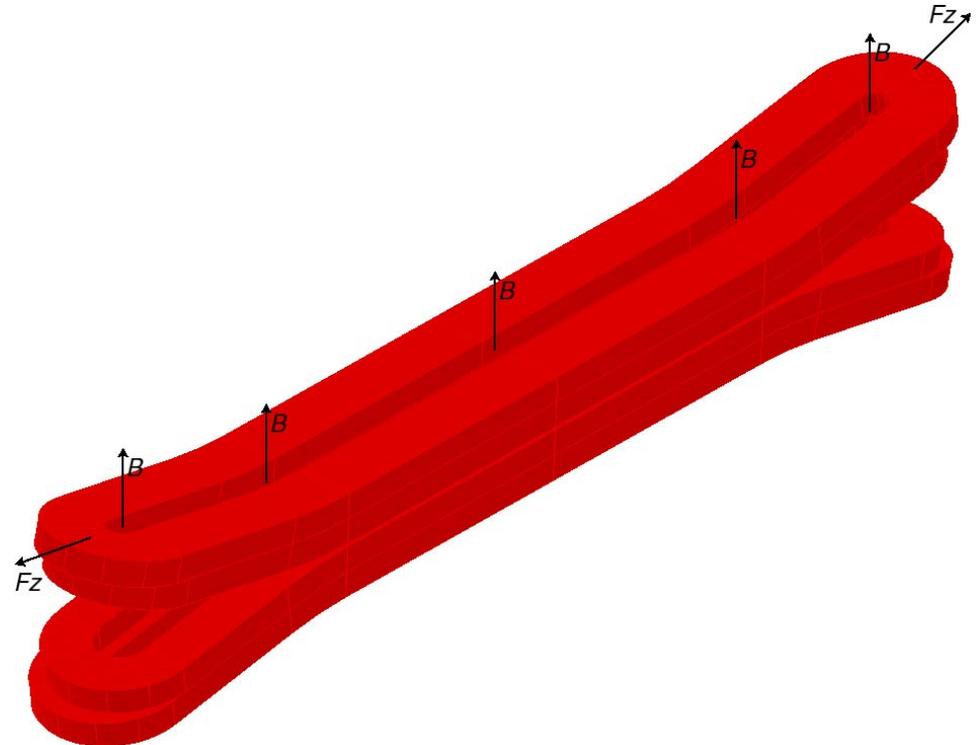
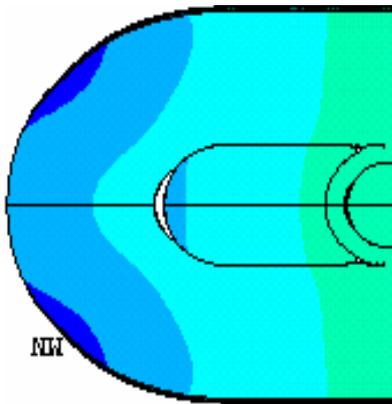
- Forces are outward in radial direction and towards the mid plane in the azimuthal direction

# Ends

- Lorentz forces creates an axial tension, pushing the coil ends outward (not unlike a solenoid)



Source of many design decisions and challenges



- The magnetic pressure,  $p_m$  acting on the winding surface element is given by

$$p_m = \frac{B_0^2}{2\mu_0}$$

similar to the pressure of a gas acting on its container

- In the example to follow we have 12 T

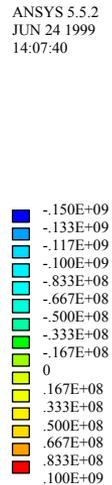
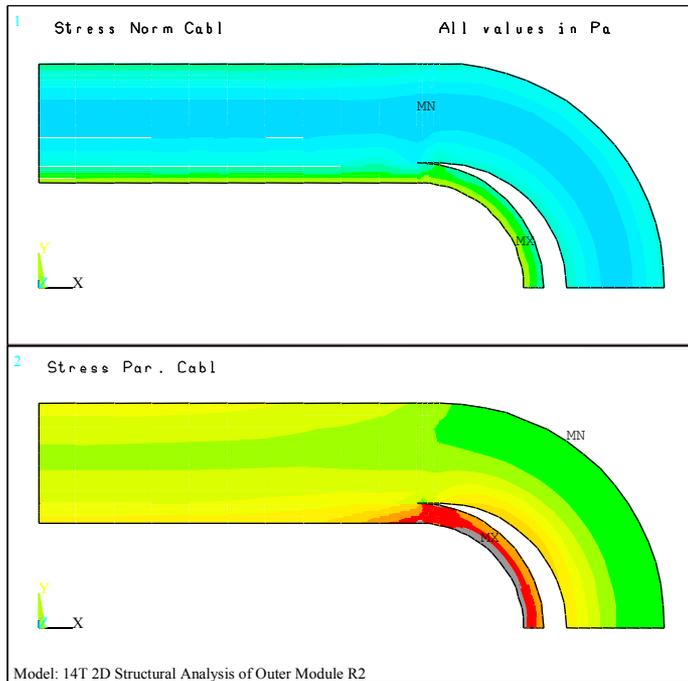
$$\text{so . . . } p_m = (12^2)/(2 \cdot 4 \pi \times 10^{-7}) = 5.7 \times 10^7 \text{ Pa} = 555 \text{ atm}$$

**General example of forces – at 5 T the force trying to separate the two coil halves is 100 Tons/m**

# Racetrack Coil Test (RT-1)

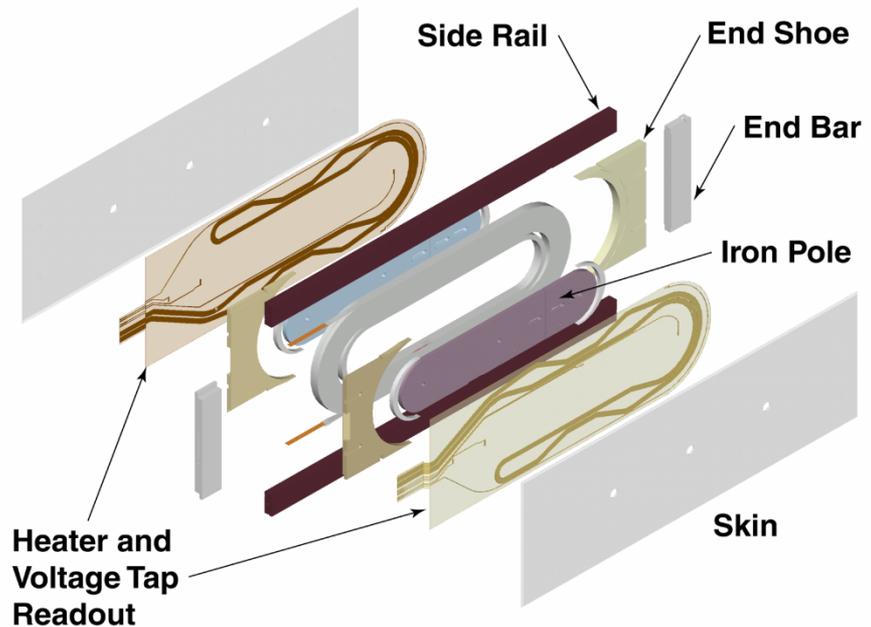


- **Two simple racetrack coils**
  - 50 cm long
  - 12 Tesla



Energize

## Outer Coil Module

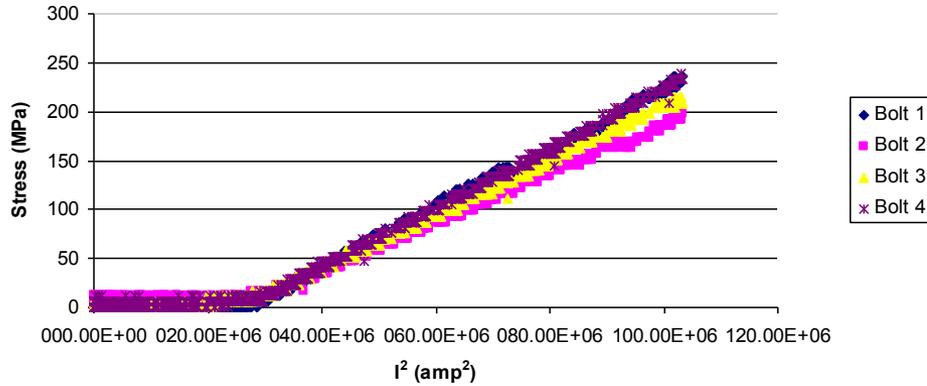




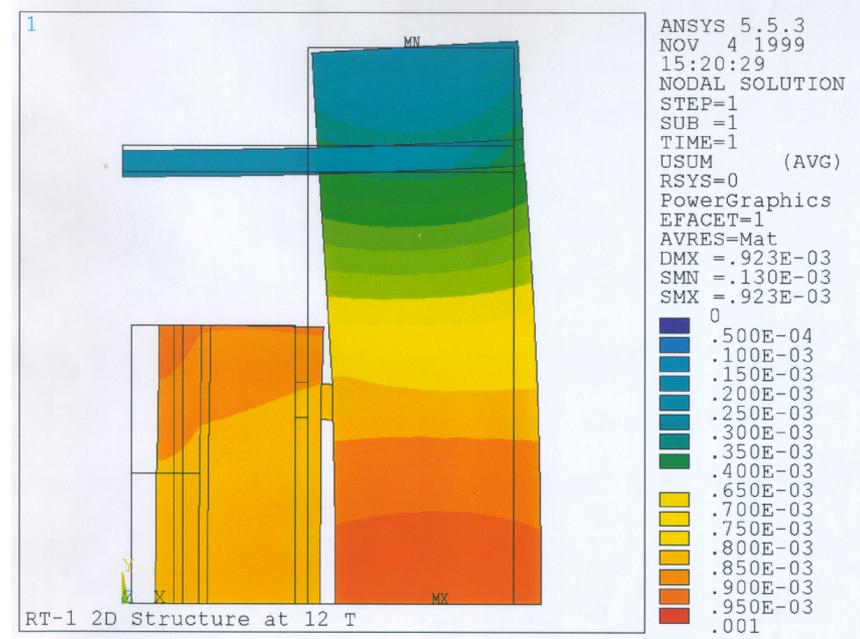
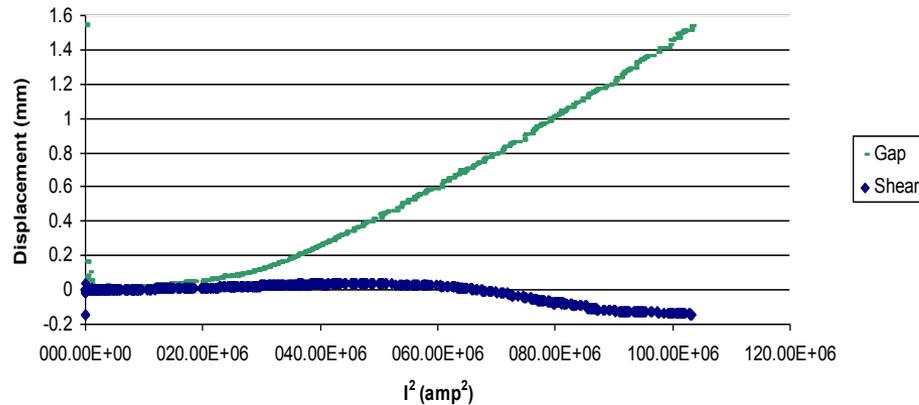
# Test Results



RT-1 Quench 4  
Bolt Stress



RT-1 Quench 4  
Optical Gauges



# Coil Fabrication



Consider NbTi (dominates use now) and Nb<sub>3</sub>Sn

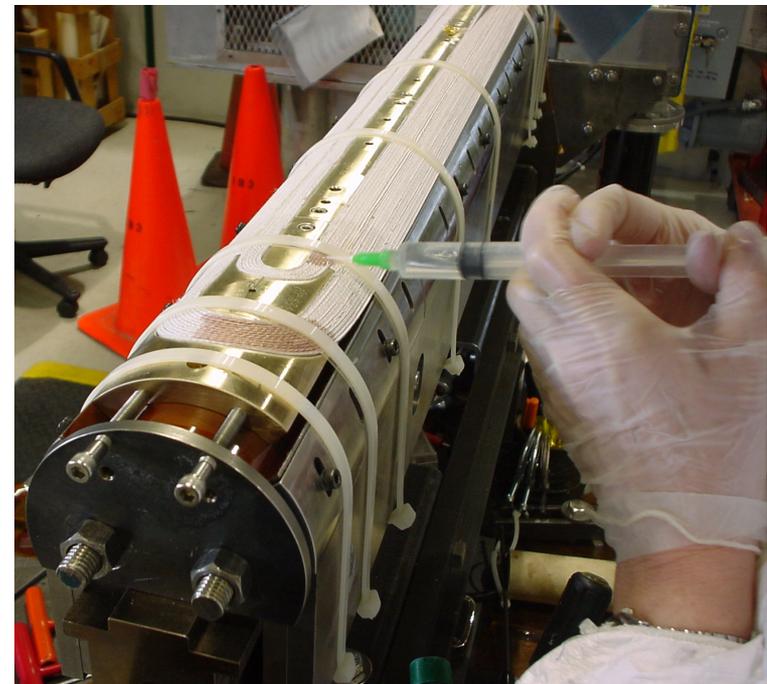
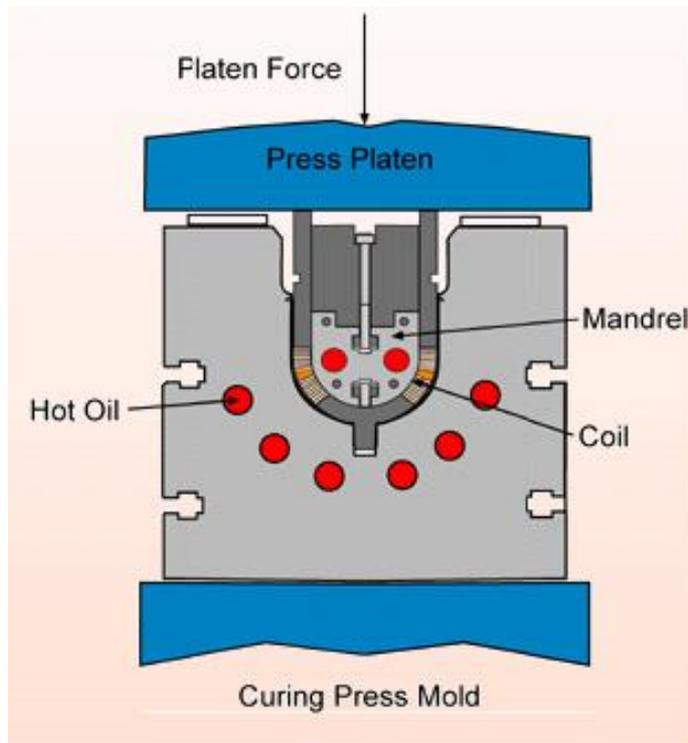
- **Winding**
  - **Virtually the same process for both materials**
  - **Start with insulated cable**
    - NbTi – 1 or 2 layers of polyimide wrap
    - Nb<sub>3</sub>Sn – S-2 glass “sock” – really not insulator but matrix for later epoxy impregnation



# Coil Fabrication

- **Curing/Reaction**

- NbTi coils “cured” in fixture to set dimension and aid handling
- Nb<sub>3</sub>Sn coils “cured” with ceramic binder and reacted (650 – 700 °C)

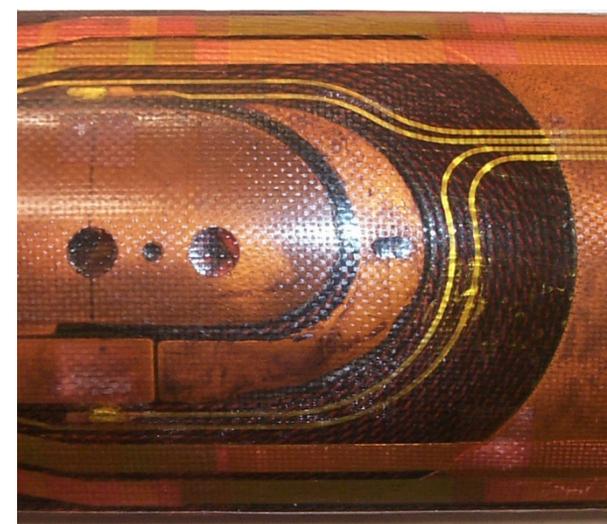
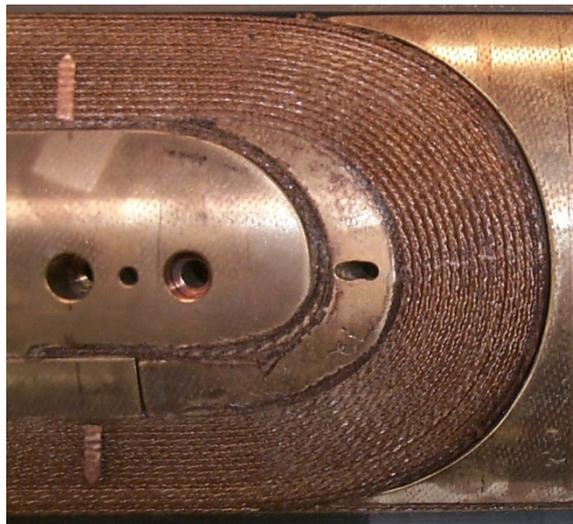
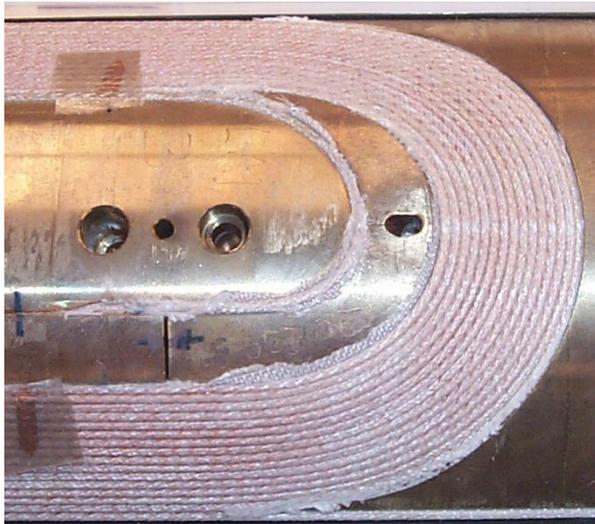


# Reaction Fixture for Nb<sub>3</sub>Sn Coils



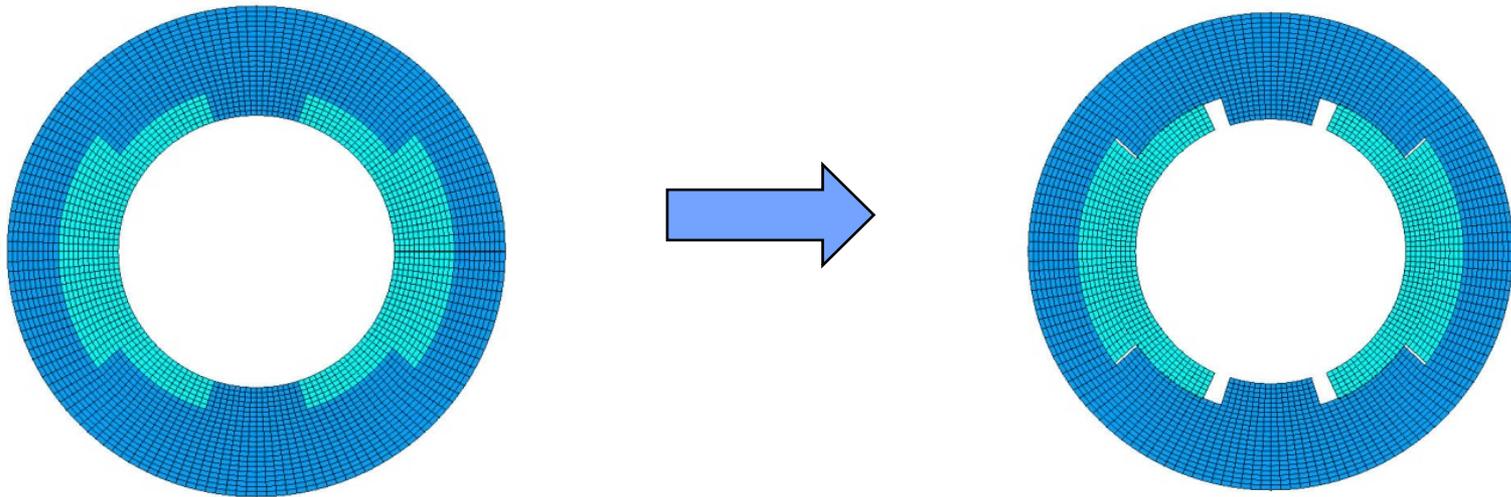
# Coil Fabrication

- **Epoxy impregnation of Nb<sub>3</sub>Sn Coils**
  - In US CTD-101 is used for impregnation (looking at cyanate esters)
  - Two-fold purpose -
    - Provide insulation
    - Distribute load between strands to reduce stress points



# Structures and Pre-Stress

- Due to character of Lorentz forces, a simple rigid structure is not sufficient.
- “Pre-stress” is required to prevent conductor from losing contact with the structure



- Due to uncertainties, some margin is allowed, ~ 20 MPa

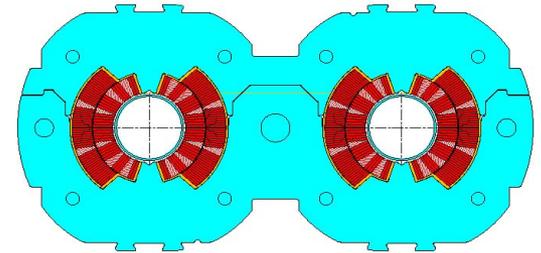
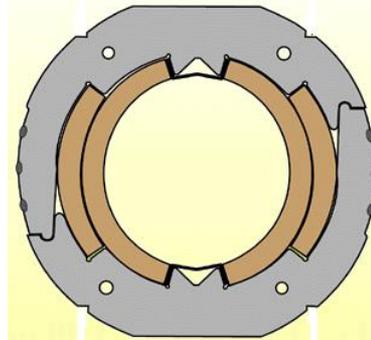
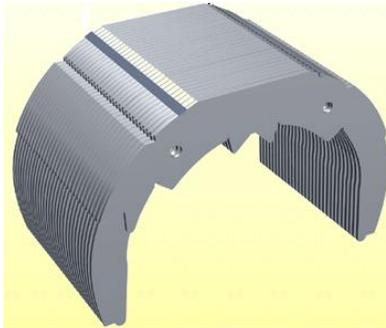
# Support Structure



- **Provides**
    - **Precise positioning and alignment**
      - Prevents changes in coil shape that could affect field quality
    - **Pre-stress and prevents movement under Lorentz loading**
      - Conductor displacement that could release frictional energy
  - **But must prevent over-stressing the coil**
    - **Insulation damage at about 150-200 MPa**
    - **Possible conductor degradation of Nb<sub>3</sub>Sn magnets at 150 – 200 MPa.**
    - **Yielding of structural components**
- Remember this!
-

# Collars

- **First introduced in the Tevatron**
  - Since used in most accelerator magnets



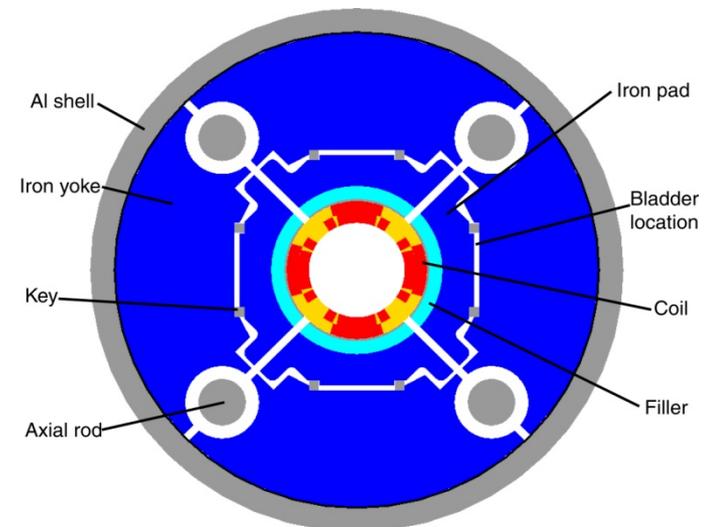
LHC

- Provide some or all of the pre-stress
- Precise cavity ( $\sim 20$  microns)
- Composed of Al or stainless steel laminations

# Final Assembly



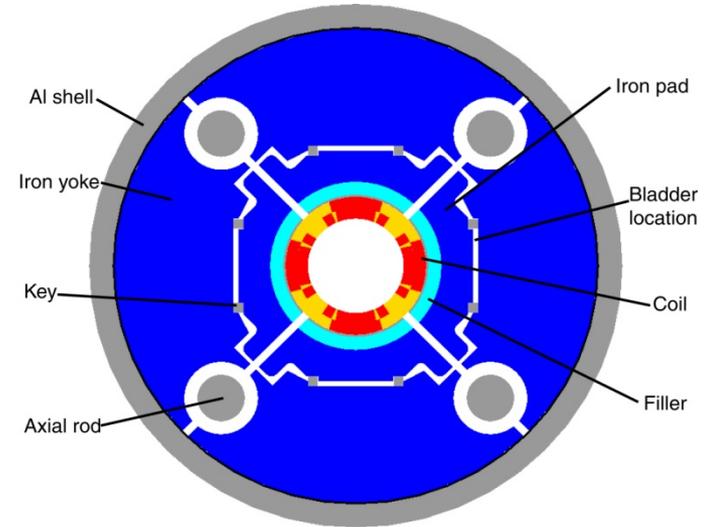
- **Iron yoke**
  - Shields and enhances field
  - In some cases provides additional preload
- **“Skin” or shell**
  - Yoke is contained within two welded half-shells of stainless steel (the “skin”) or a shrinking cylinder of aluminum
    - Outer shell contributes to coil rigidity and provides helium containment
- **End support or loading**
  - Thick plates provide axial support



# Key and Bladder (LARP/LBNL TQS Quad)

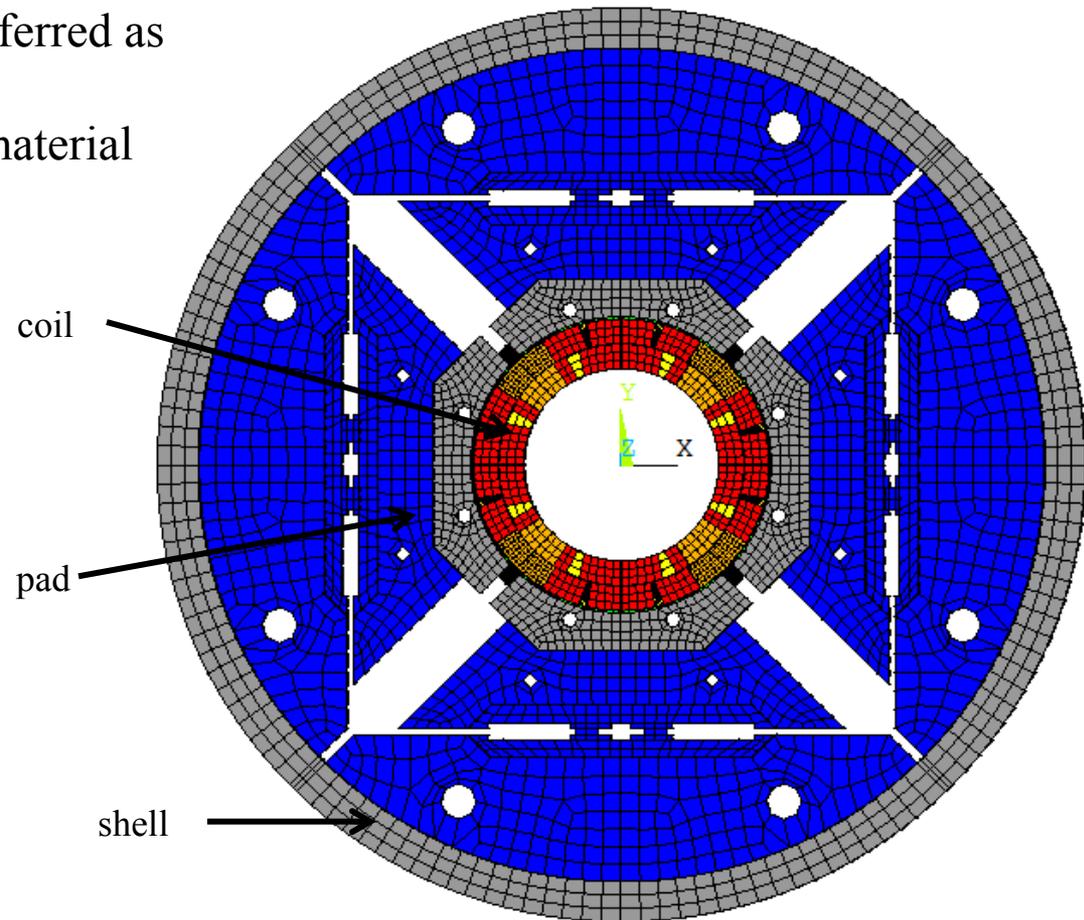
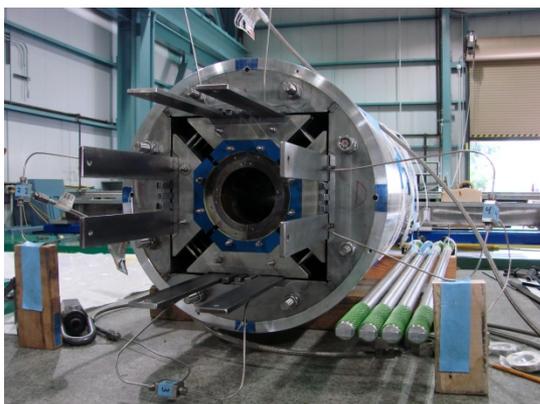
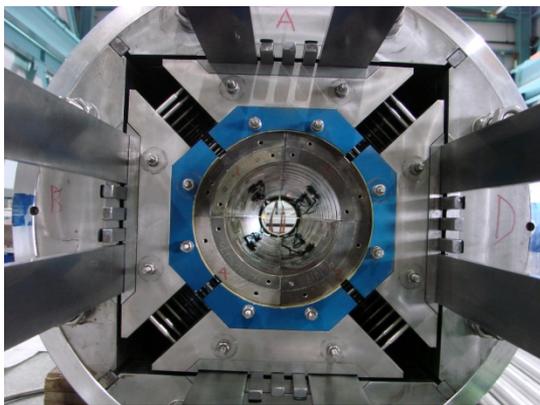


- Four pads or collars transfer load to coils
- Yoke is contained by aluminum shell
- Preload provided by inflating bladders and held via keys
- Coil pre-stress increases during cooldown due to the high thermal contraction of the aluminum shell.



# Magnet Design Support Structure

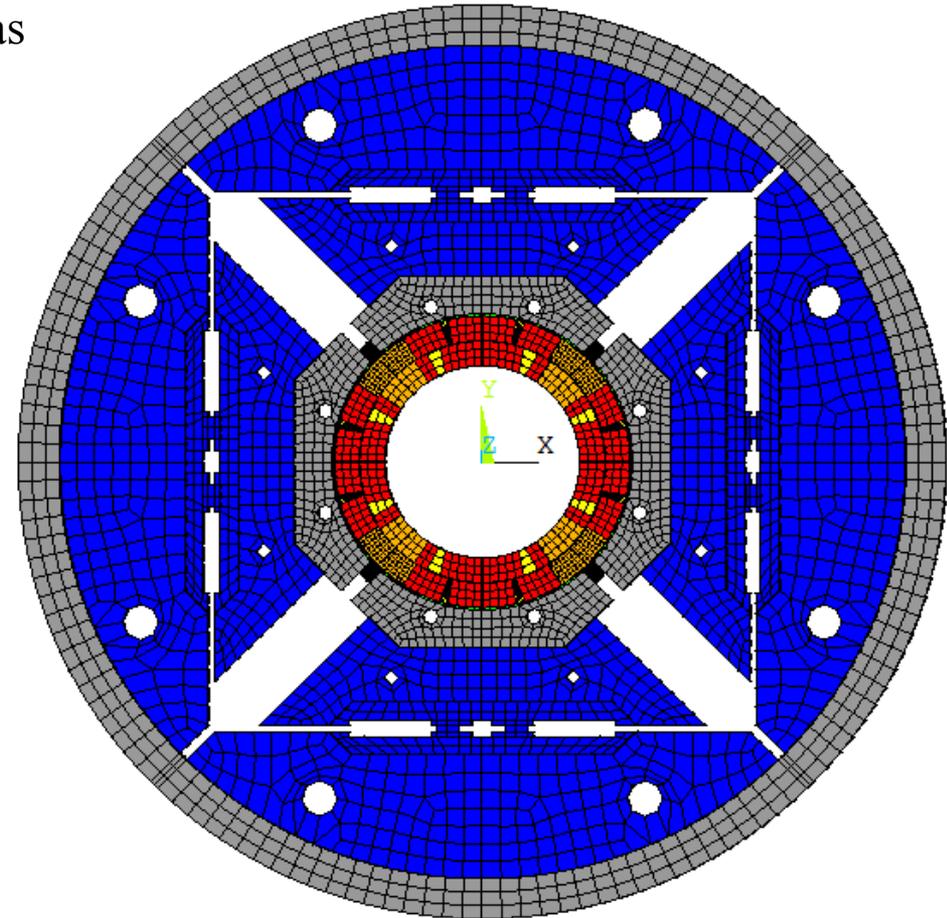
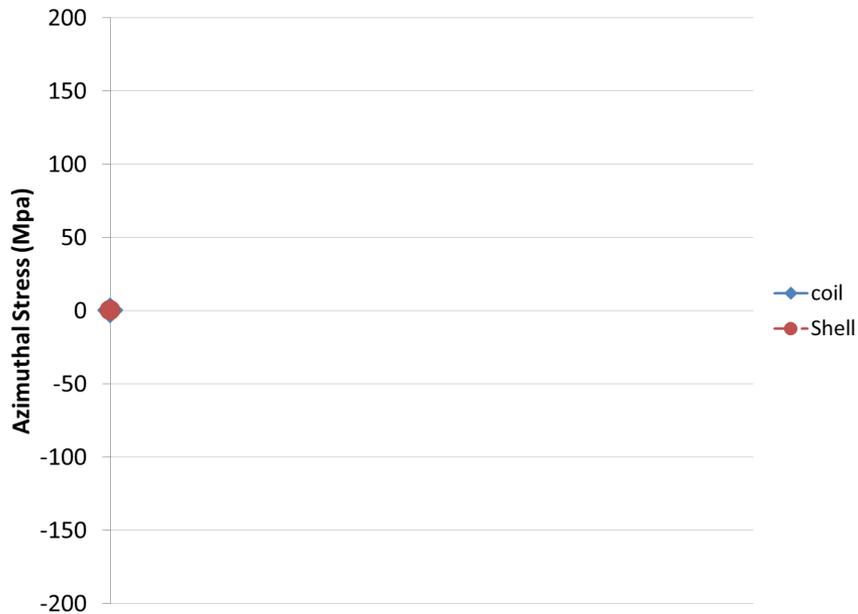
- Shell-based support structure often referred as “bladder and keys” structure developed at LBNL for strain sensitive material



Courtesy Helene Felice

# Magnet Design Support Structure

- Shell-based support structure often referred as “bladder and keys” structure developed at LBNL for strain sensitive material

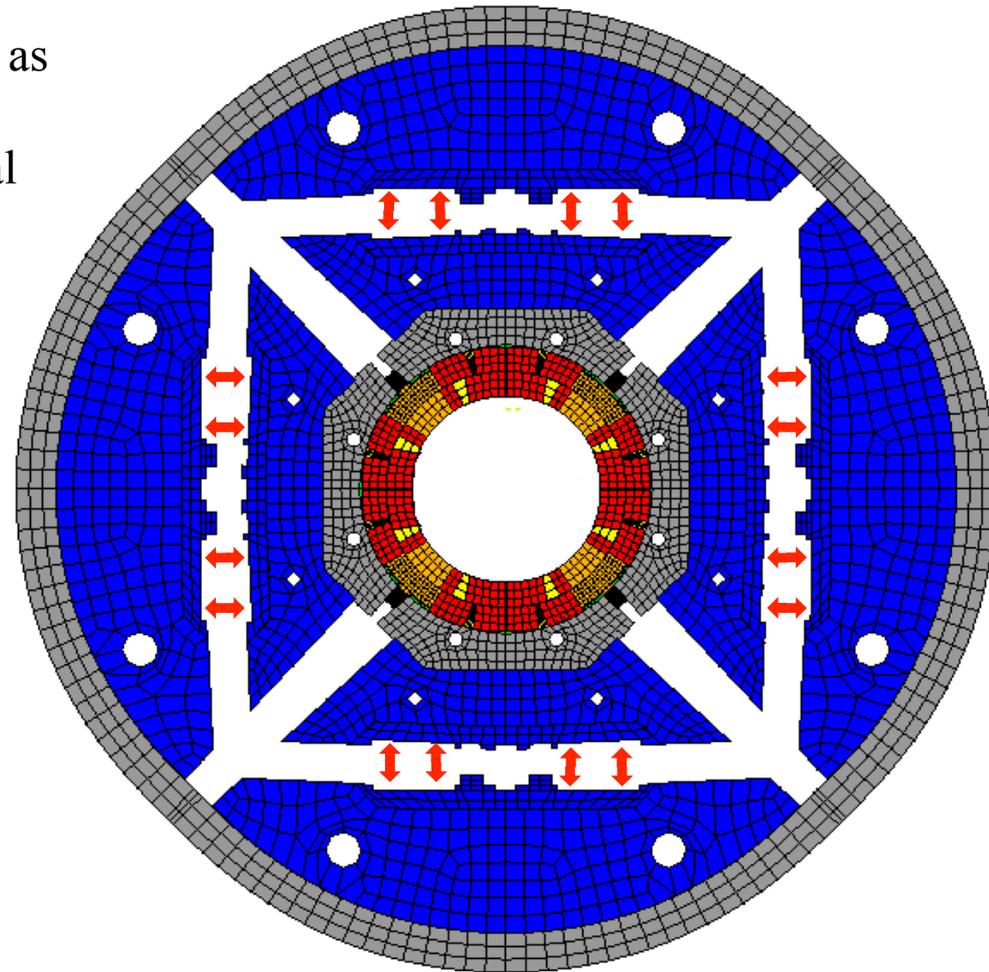
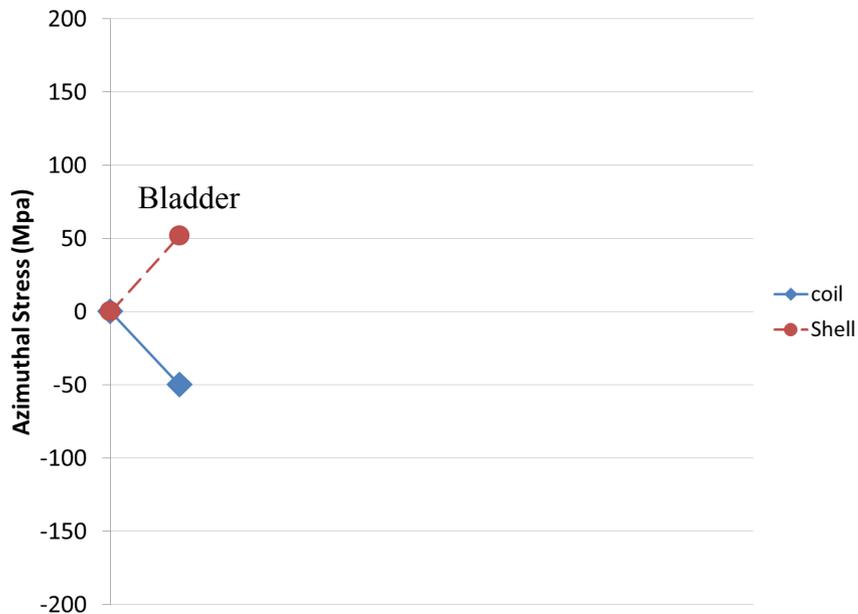


Courtesy Helene Felice

# Magnet Design Support Structure

Inflated Bladders

- Shell-based support structure often referred as “bladder and keys” structure developed at LBNL for strain sensitive material

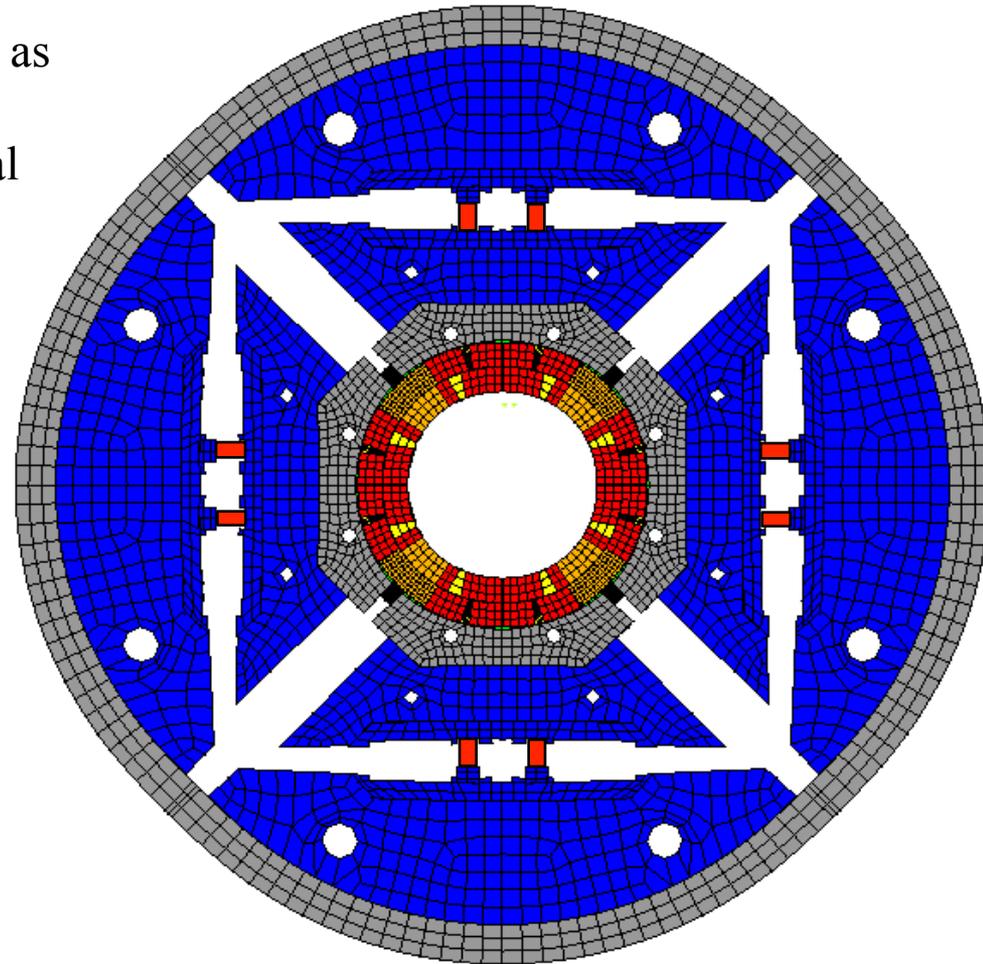
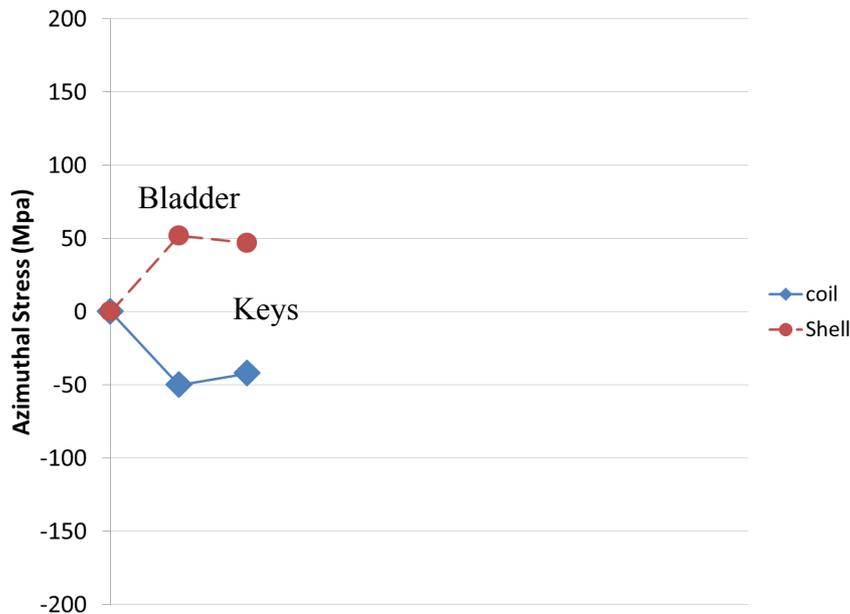


Courtesy Helene Felice

# Magnet Design Support Structure

Shimming of the load leys

- Shell-based support structure often referred as “bladder and keys” structure developed at LBNL for strain sensitive material



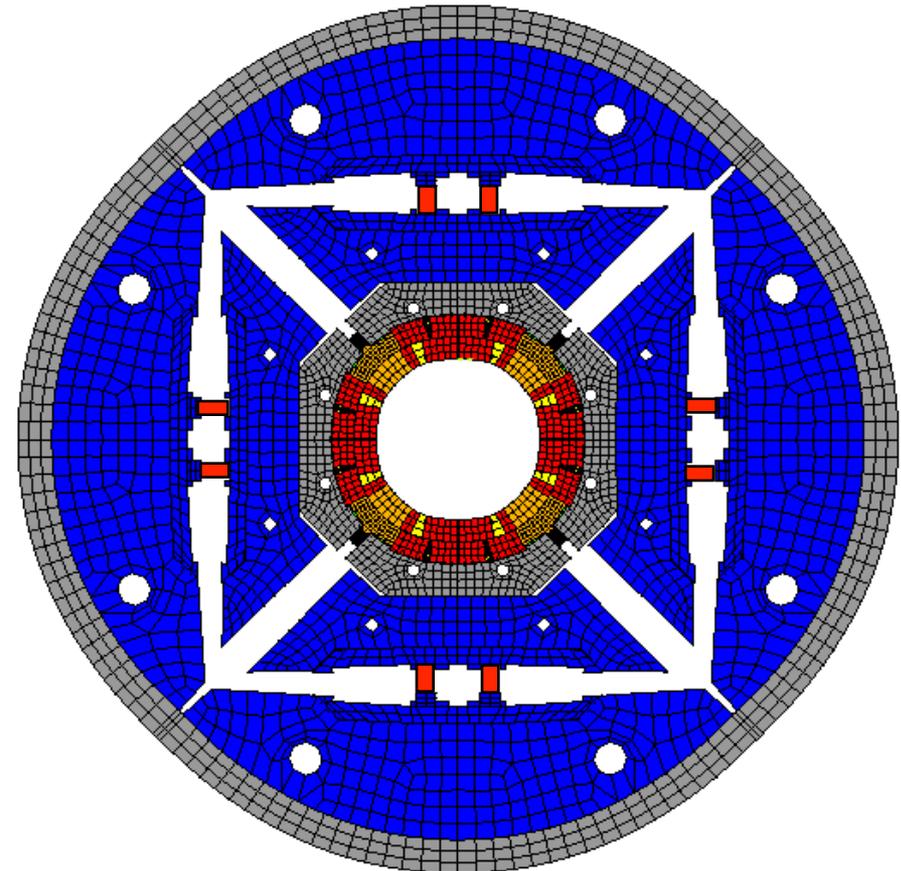
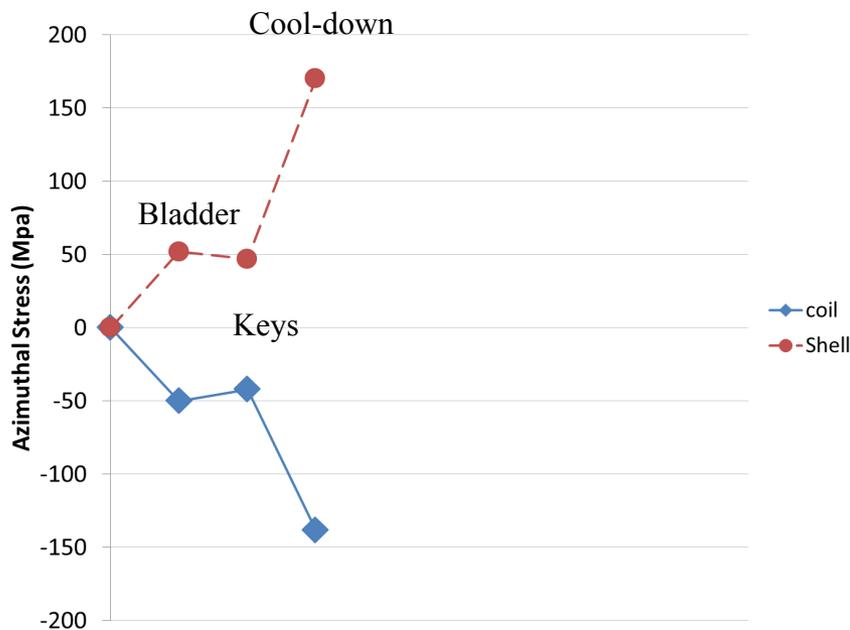
Courtesy Helene Felice

Displacement scaling 30

# Magnet Design Support Structure

Cool-down

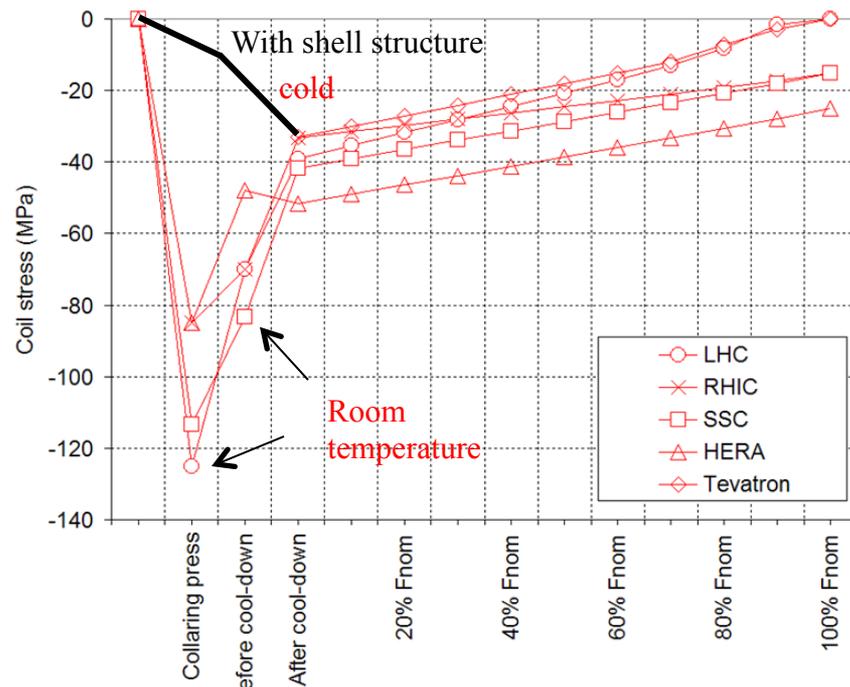
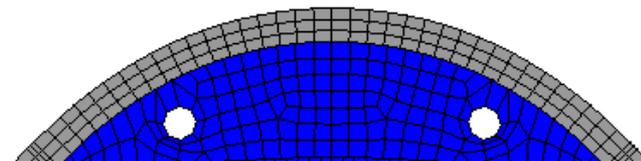
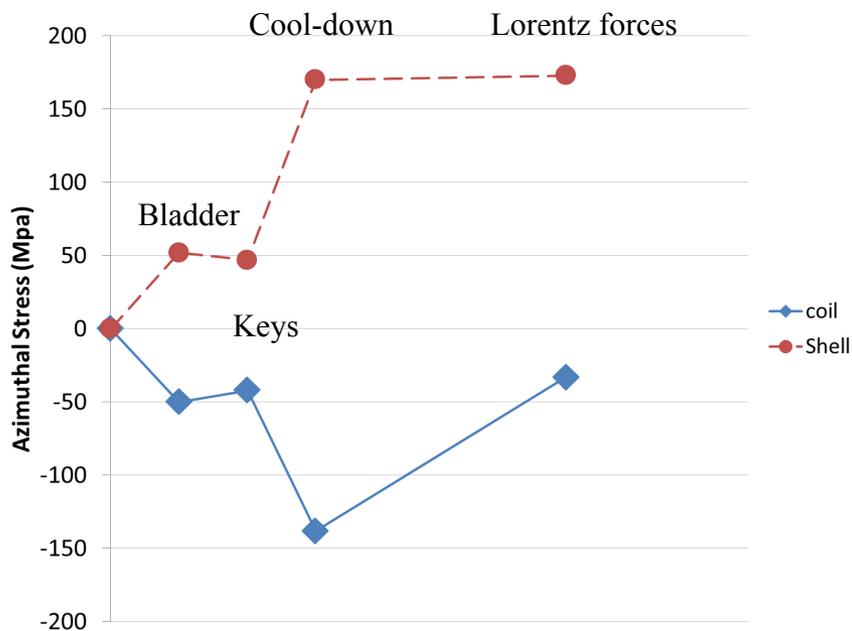
- Shell-based support structure often referred as “bladder and keys” structure developed at LBNL for strain sensitive material



Courtesy Helene Felice

Energized

- Shell-based support structure often referred as “bladder and keys” structure developed at LBNL for strain sensitive material



Collaring process- Courtesy of Paolo Ferracin

Displacement scaling 30

Courtesy Helene Felice



# US Magnet Programs

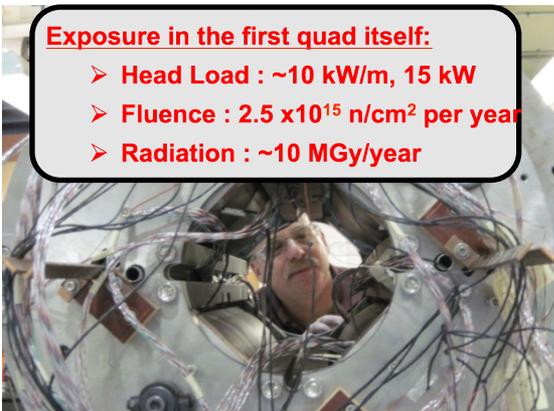
# BNL Magnet Program



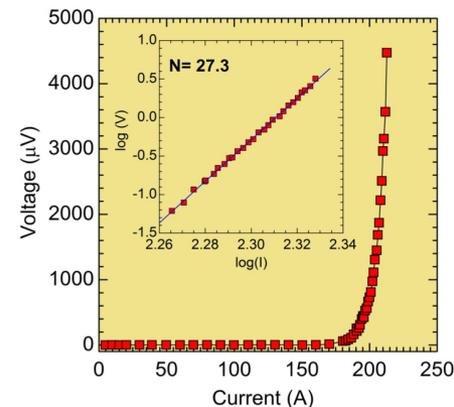
- Accelerator dipole and quadrupole magnet programs
  - HTS magnet is now part of the baseline design of a major proposed facility – Facility for Rare Isotope Beams (FRIB)
    - This is a significant 1st – perhaps a major milestone
  - High field magnets in a hybrid design for LHC upgrade
- High field solenoid programs
  - For Muon Collider and Energy Storage

## Exposure in the first quad itself:

- Head Load : ~10 kW/m, 15 kW
- Fluence :  $2.5 \times 10^{15}$  n/cm<sup>2</sup> per year
- Radiation : ~10 MGy/year



*Courtesy Ramesh Gupta*



- ❖ **The mission** of the High Field Magnet Program at Fermilab is the development of advanced superconducting **accelerator** magnets and baseline technologies for present and future particle accelerators.
- ❖ **At the present time the focus** is on the development of high-field accelerator magnets with operating fields up to 15 T based on Nb<sub>3</sub>Sn superconductor.
- ❖ **In the longer term** the program will support the development of accelerator magnets with operating fields above 20 T.

*Courtesy Sasha Zlobin*

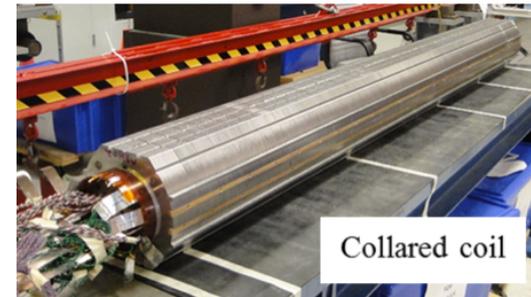
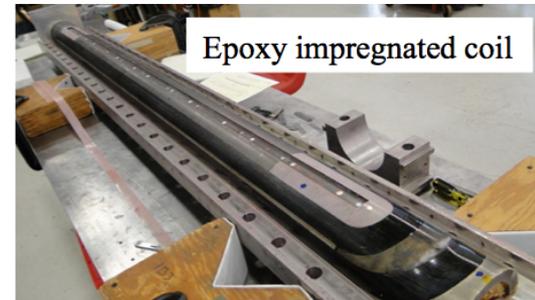
# FNAL: Twin-aperture 11 T Nb<sub>3</sub>Sn Dipole

## ❖ Collaboration with CERN for possible use in LHC

- 2012: 2-m long single-aperture demonstrator
  - Magnet assembled and tested,  $B_{\max}=10.4$  T at 1.9K
- 2013: 1-m long twin-aperture model
  - First aperture assembled and being tested
  - Fabrication of the second aperture has started
- 2014: 2-m long twin-aperture demonstrator
- 2015: 5.5-m long prototype

Parameter	Single-aperture	Twin-aperture
Aperture	60 mm	
Yoke outer diameter	400 mm	550 mm
Nominal bore field @11.85 kA	10.86 T	11.25 T
Short-sample bore field at 1.9 K	13.6 T	13.9 T
Margin $B_{\text{nom}}/B_{\text{max}}$ at 1.9 K	0.80	0.81
Stored energy at 11.85 kA	473 kJ/m	969 kJ/m
$F_x$ per quadrant at 11.85 kA	2.89 MN/m	3.16 MN/m
$F_y$ per quadrant at 11.85 kA	-1.57 MN/m	-1.59 MN/m

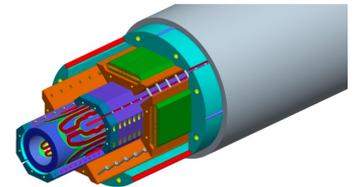
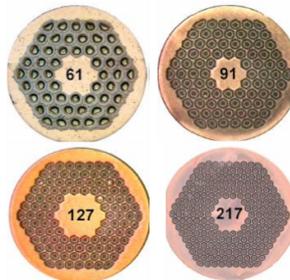
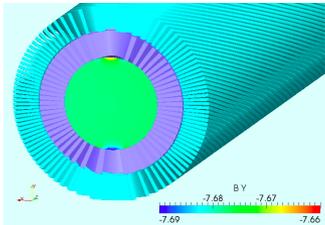
40-strand keystoneed cable



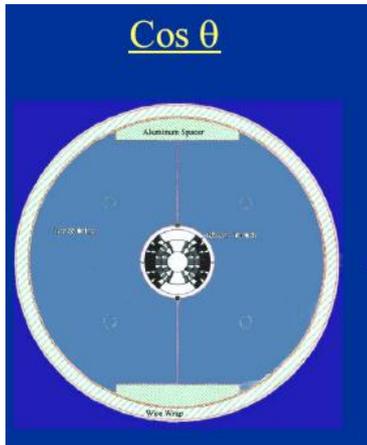
# LBNL Superconducting Magnet Program



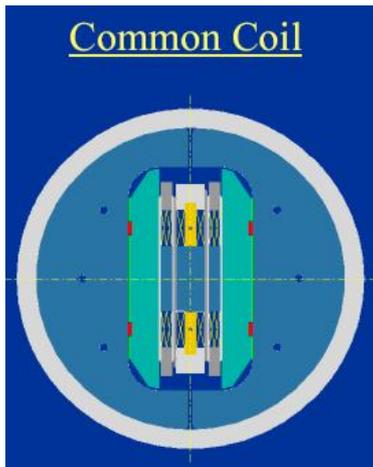
- **World-leading R&D program in high field accelerator magnets beyond 11T**
- **Integrated program from material, through analysis, fabrication and test**
  - Hierarchical modeling: micro to macro
- **Strategy**
  - **Innovative ideas to push the limits of high field accelerator magnets**
    - **Next breakthrough: 20 T**
      - Combine materials development with innovative structures
  - **Strong support of ongoing and future HEP programs/projects**
    - LARP, MAP (MICE)
  - **Our technology is a key component of the Stewardship Program**



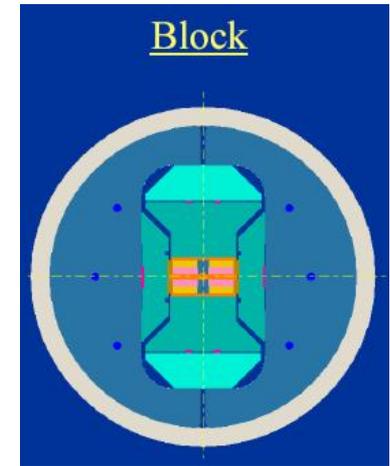
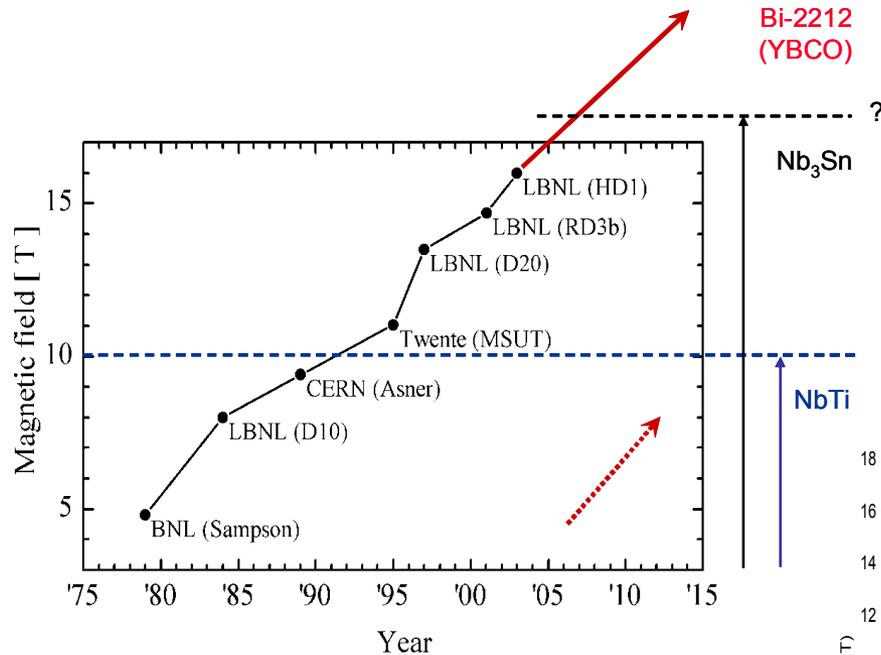
# High field superconducting dipoles ....



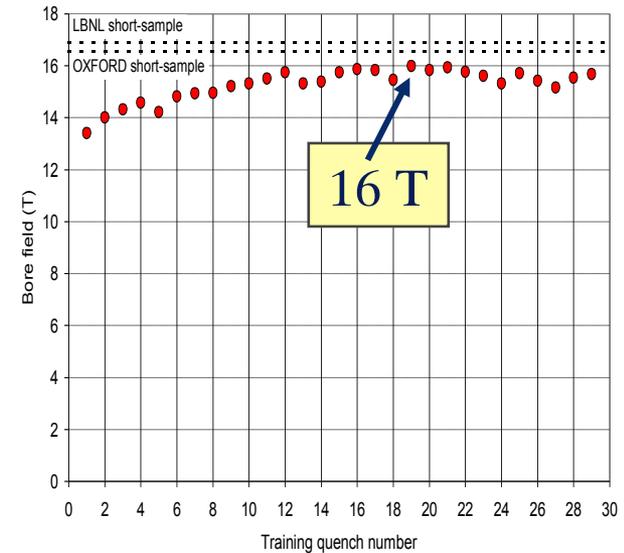
D20



RD



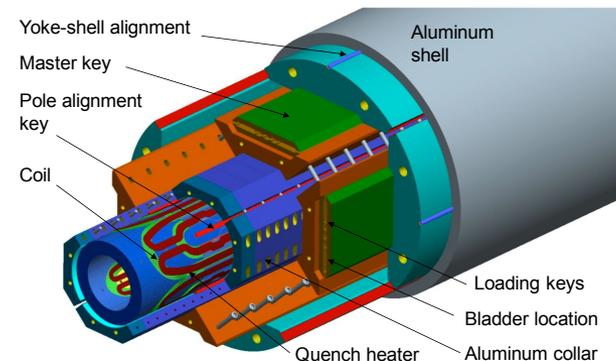
HD



# LBNL has a major role in the LHC Accelerator Research Program (LARP)



- Phase 1 of LARP magnet program completed
  - TQ – technology development and reproducibility
    - *surpassed LARP target gradient*
  - LQ – handling, fab, protection of long magnets (~ 4m)
    - *achieved 220 T/m*



- Technology development (dipoles and quads) for LHC upgrades and future accelerators
- Fairly new to Nb<sub>3</sub>Sn technology – Process, structures
- Initial focus on conductor development (Nb<sub>3</sub>Sn PIT and YBCO)

## First step (2004 – 2012):

- Conductor technology : NED 1.25 mm, Fresca2 1 mm (2010), 11 T 0.7 mm (2011)
- Magnet technology : Short Model Coil (2011)
- Personnel training on existing technologies : test TQ & HQ @ CERN (2009)

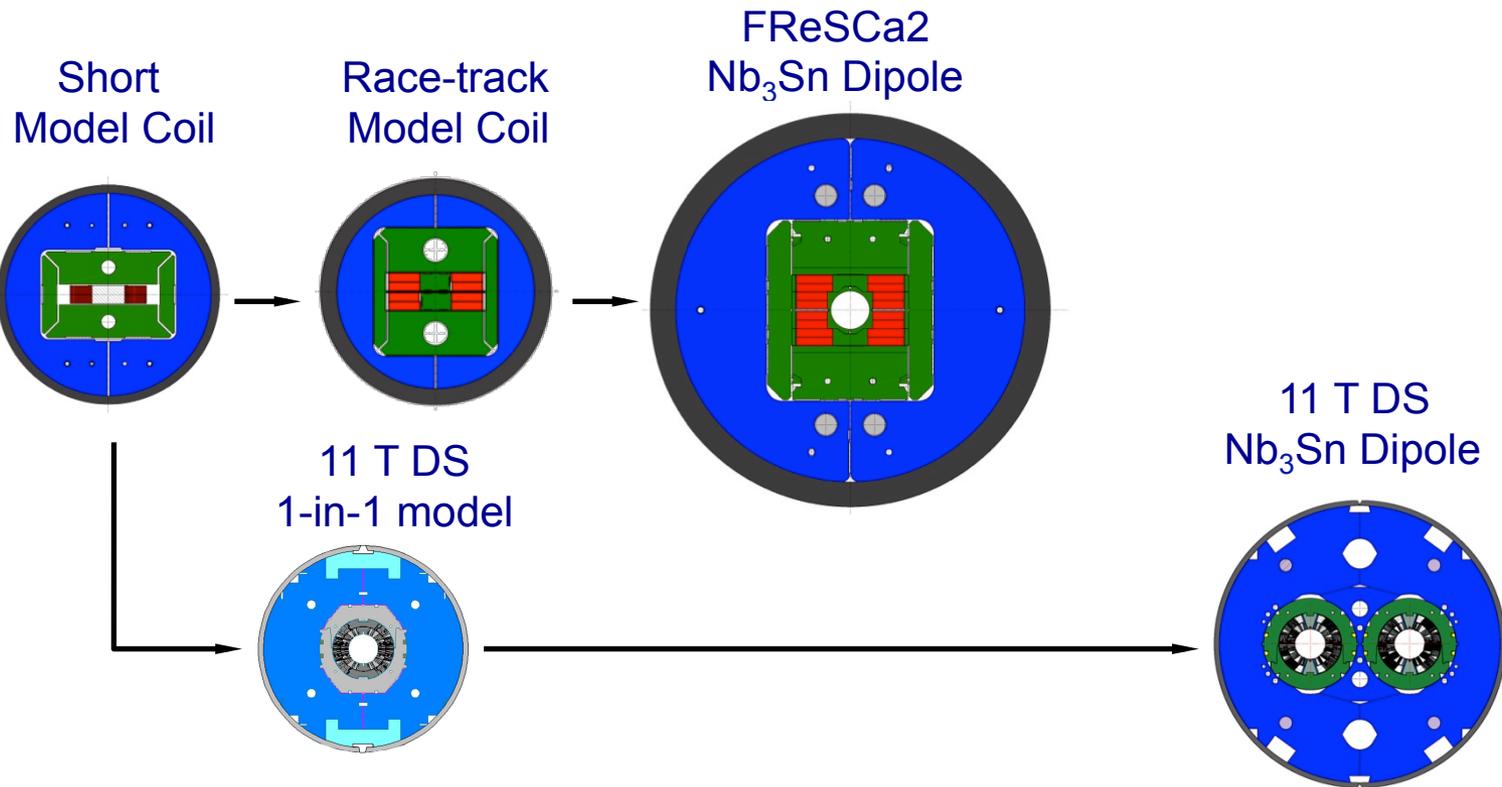
## Second step (2009 – 2014):

- Magnet models : Fresca2 (2013), IR quad model (2013), 11 T dipole model (2013)
- Conductor test facilities upgrade to 15 T test station (2014-2015)
- Radiation hardness studies for Nb<sub>3</sub>Sn and coil insulation (2010-2014)
- Magnet concepts from 15 T to 20 T : EuCARD 6 T insert (2013), EuCARD2 (2016)

## Third step (2014 – 2016):

- LHC Dispersion Suppressor dipole prototype (2015)
- LHC Inner triplet quadrupole prototype (2016)

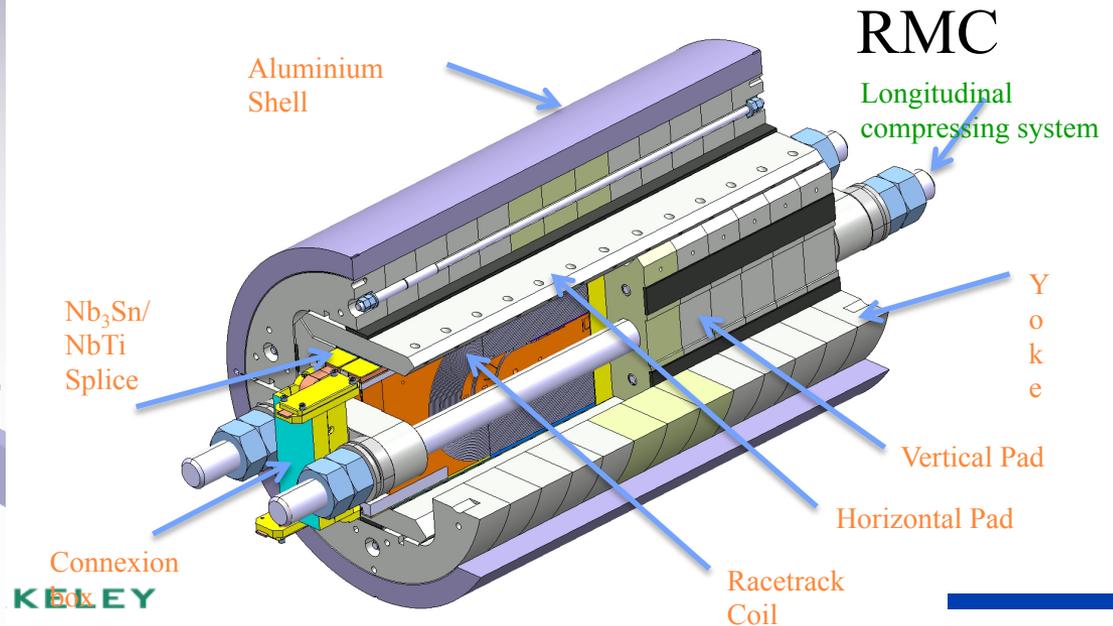
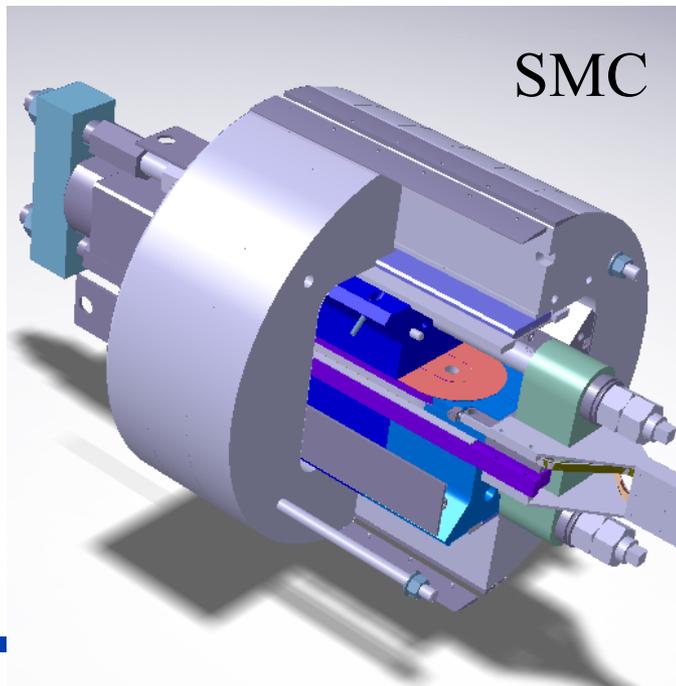
# High Field Magnet R&D



# Short Model Coil and Racetrack Model Coil



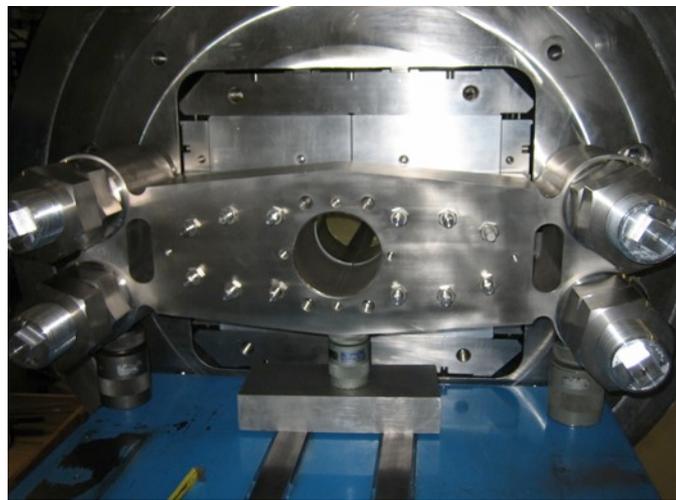
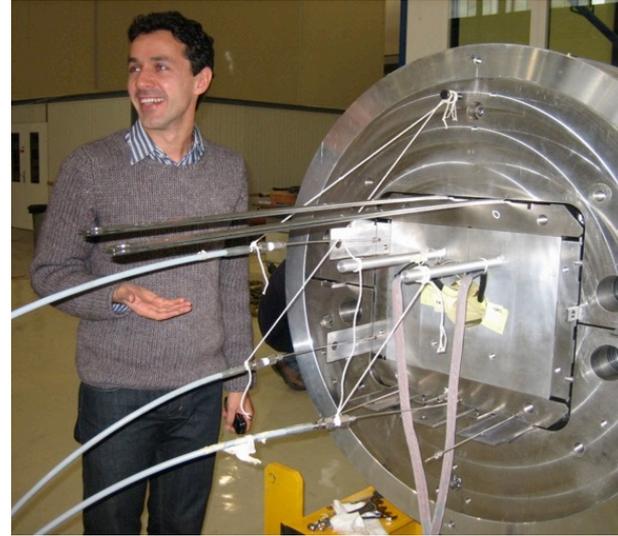
- SMC : test  $\text{Nb}_3\text{Sn}$  conductor and coil technology with a small 10 mm cable
  - 1 coil set tested
  - 2<sup>nd</sup> coil set reacted: to be tested in spring 2013
- RMC: test the Fresca2 conductor and coil technology with the 21 mm Fresca2 cable
  - 1<sup>st</sup> coil set being manufactured: to be tested end spring 2013



# Fresca2 structure, mounting with dummy Al coil blocks



- Mounting Last week,
- LN2 test end of March to study mechanical behaviour



- Start with field
  - LHC will (hopefully) operate at 8.33 T (7 TeV) with about a 20% margin
  - A factor of 2 gives us ~ 17 T (operating)
    - Same situation as above implies > 21 T
    - Given current status of conductors, this means HTS is required
- Other factors
  - Must fit in the tunnel
    - 570 mm diameter for the cold mass in the LHC
    - We assume 800 mm diameter for the HE-LHC
    - Coil must be reasonably compact
  - Cost
    - Magnet has to rely on Nb<sub>3</sub>Sn and on HTS
    - Cost of Nb<sub>3</sub>Sn: 4 times Nb-Ti
    - Cost of HTS: 4 times Nb<sub>3</sub>Sn
    - **grading of material is necessary**

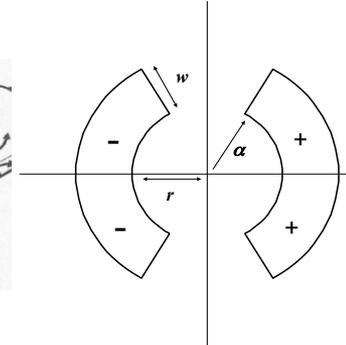
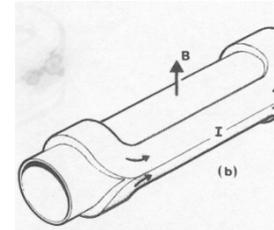
# Getting to High Fields



- Field is proportional to current density and coil thickness

$$B \text{ [T]} \sim 0.0007 \times \text{coil width [mm]} \times \text{current density [A/mm}^2\text{]}$$

LHC:  $8 \text{ [T]} \sim 0.0007 \times 30 \times 380$

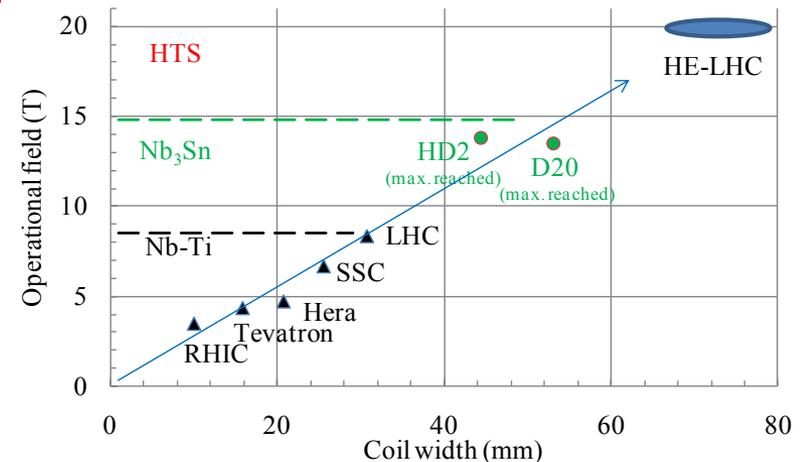


— Accelerators use current density of the order of 350-400 A/mm<sup>2</sup>

- This provides **~2.5 T for 10 mm thickness**
- 80 mm needed for reaching 20 T

— Grading the material:

- 30 mm of Nb-Ti to get 7.5 T
- 30 mm of Nb<sub>3</sub>Sn to get another 7.5 T
- 20 mm of HTS to get the last 5 T



Operational field versus coil width in accelerator magnets

# High field magnets – status and challenge

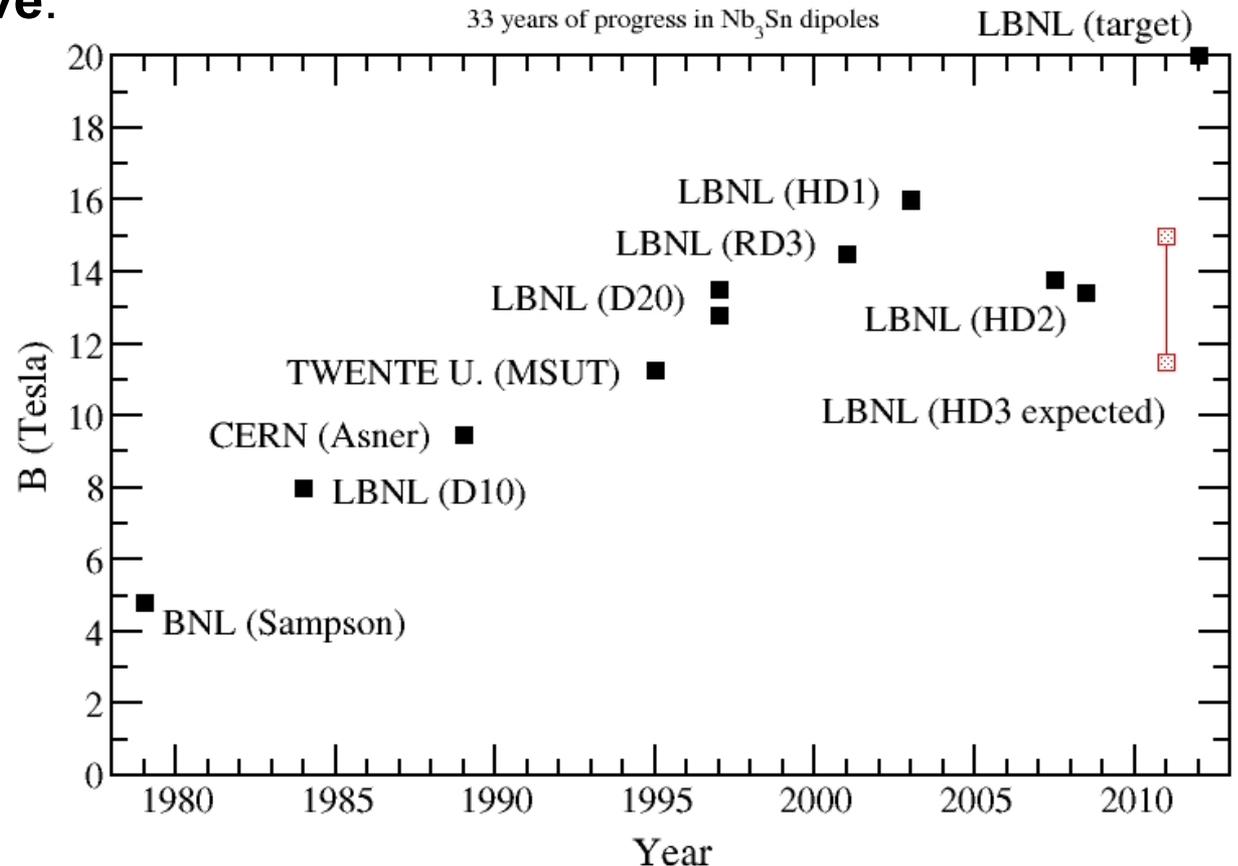


## An historical perspective:

### 1979-2012

#### 20T - Nb<sub>3</sub>Sn

- Brittle coils
- Magnet and bore size
- Coil stress > 200 Mpa
- Structure ~20 MN/m
- Delicate assembly
- Protection
- **Next –**
  - new design?
  - revised design ?



Courtesy S. Caspi, LBNL

# New Application of an Old Idea



## Published paper by D.I. Meyer and R. Flasck in 1970

(D.I. Meyer, and R. Flasck "A new configuration for a dipole magnet for use in high energy physics application", Nucl. Instr. and Methods 80, pp. 339-341, 1970.)

### **A NEW CONFIGURATION FOR A DIPOLE MAGNET FOR USE IN HIGH ENERGY PHYSICS APPLICATIONS\***

D. I. MEYER and R. FLASCK

*Physics Department, University of Michigan, Ann Arbor, Michigan 48104, U.S.A.*

Received 16 December 1969

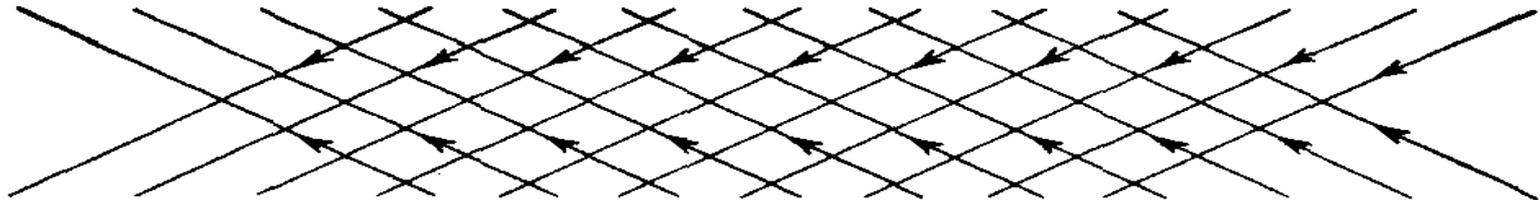


Fig. 2. Two superimposed coils with opposite skew.

Renewed interest during the past decade

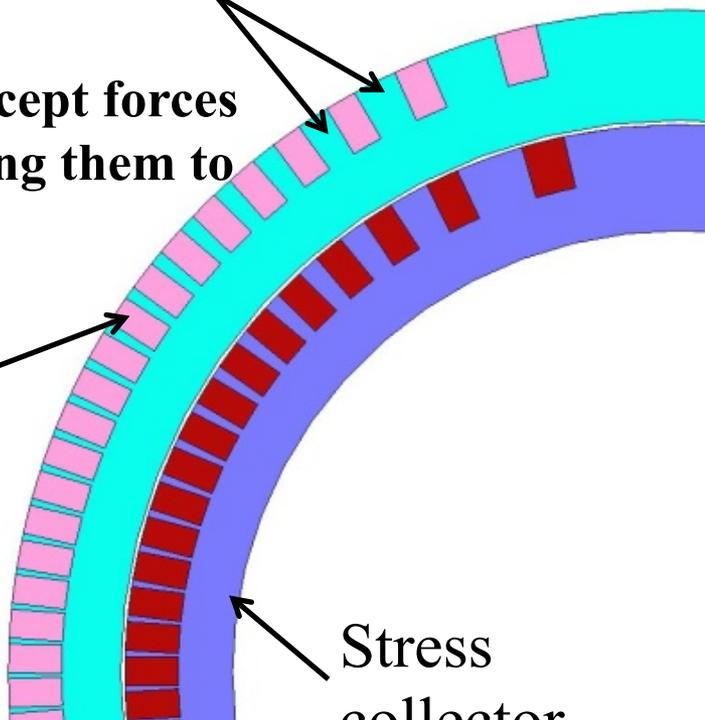
Courtesy S. Caspi, LBNL

# The Canted Cosine-Theta-Magnet (CCT)

Individual turns are separated by **Ribs**

**Ribs intercept forces transferring them to the spar**

Individual turn



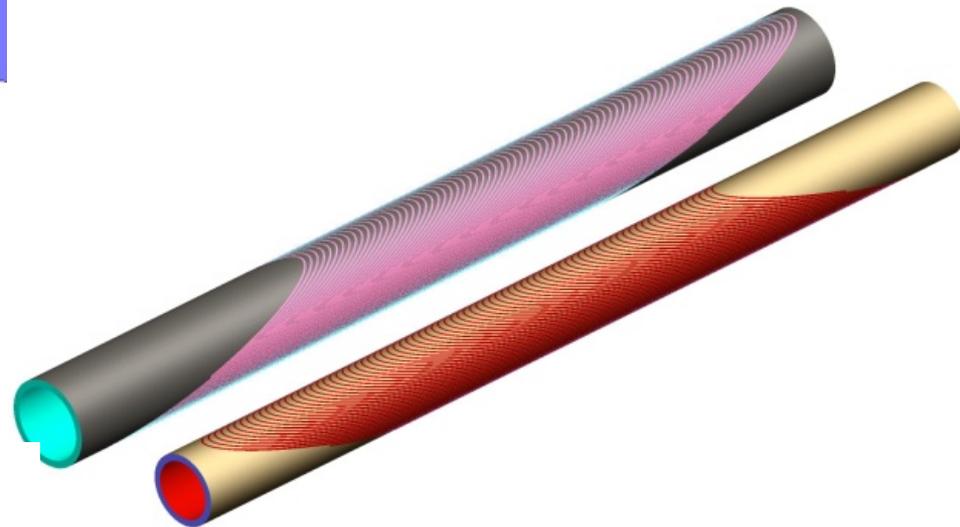
Stress collector

Unique turns distribution (**Spar**)

$$J_z \sim \cos \vartheta$$

Canted right:

Field - up dipole + right solenoid



Canted left:

Field - up dipole + left solenoid

Courtesy S. Caspi, LBNL

# The CCT Basics



## Geometry

- Single turns are placed into machined channels.
- Layers are nested “pipes” (no assembly, no collars)

## Magnetics

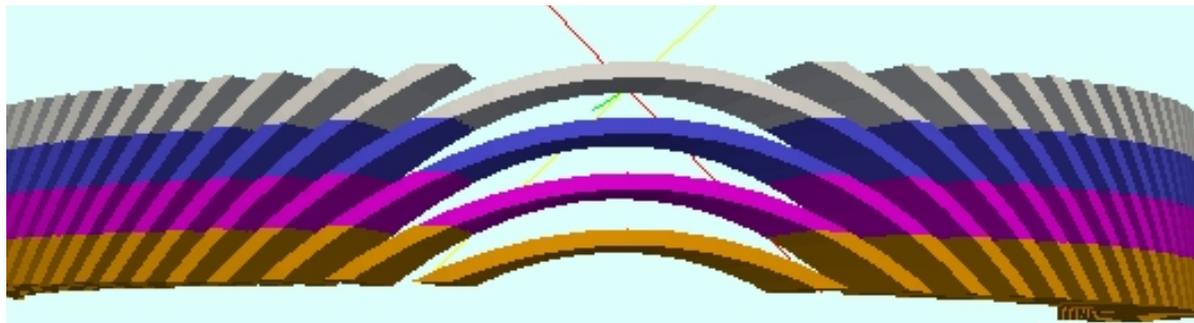
- Field quality over cross-section without optimization
- Field quality over “ends” without optimization
- ~20% more conductor, some recovery through grading

## Structural

- Transverse Lorentz forces intercepted (accumulated in the spar)
  - Applicable to High fields
  - Applicable to Large bores
  - No experience

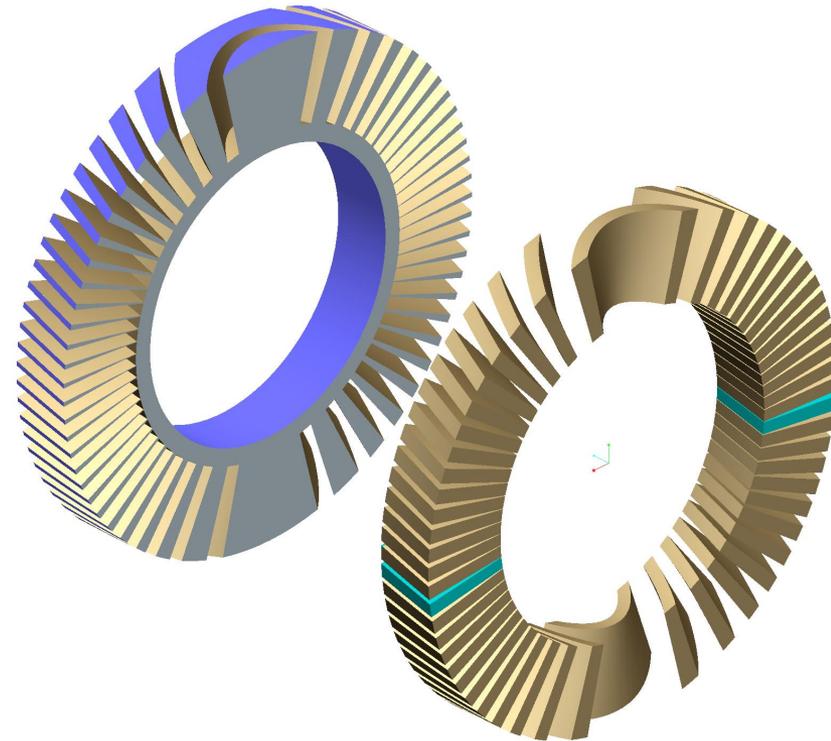
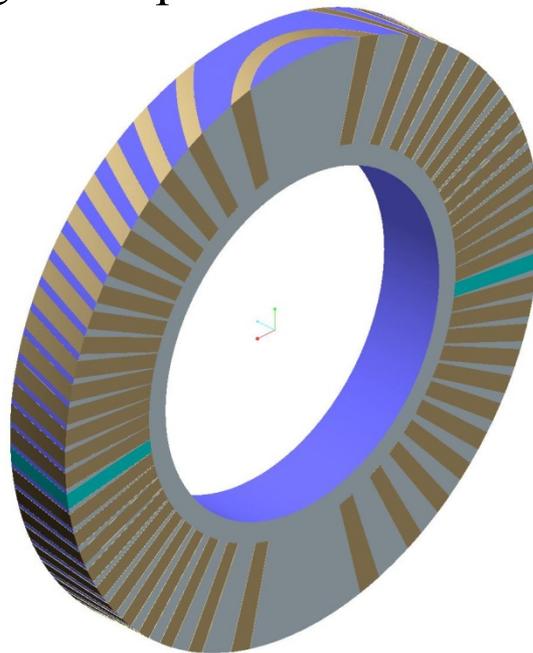
Courtesy S. Caspi, LBNL

# Repeated Lamination - 10.05 mm thick



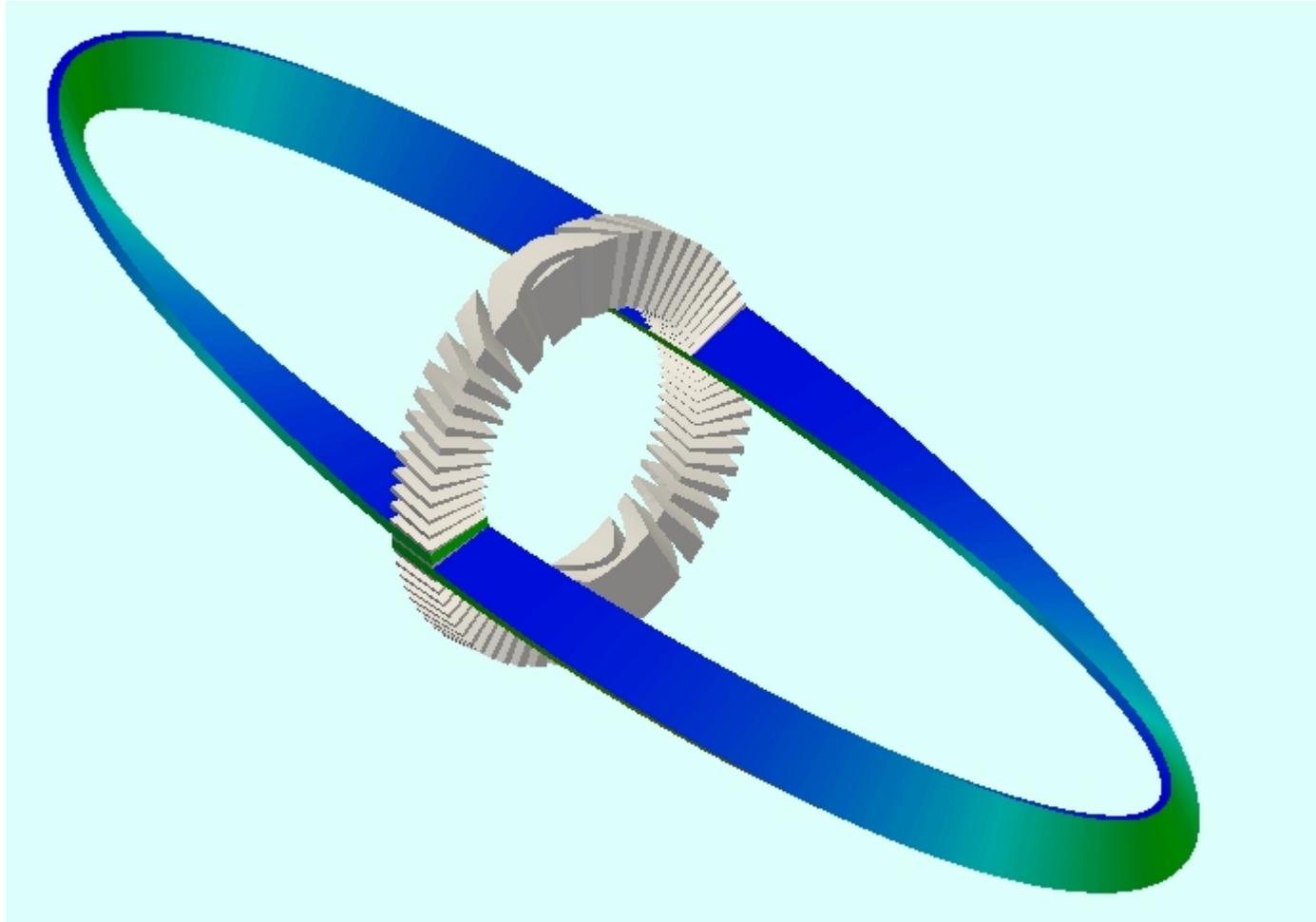
A slice of a pitch-length is repeated

Impacts:  
Construction  
Computation



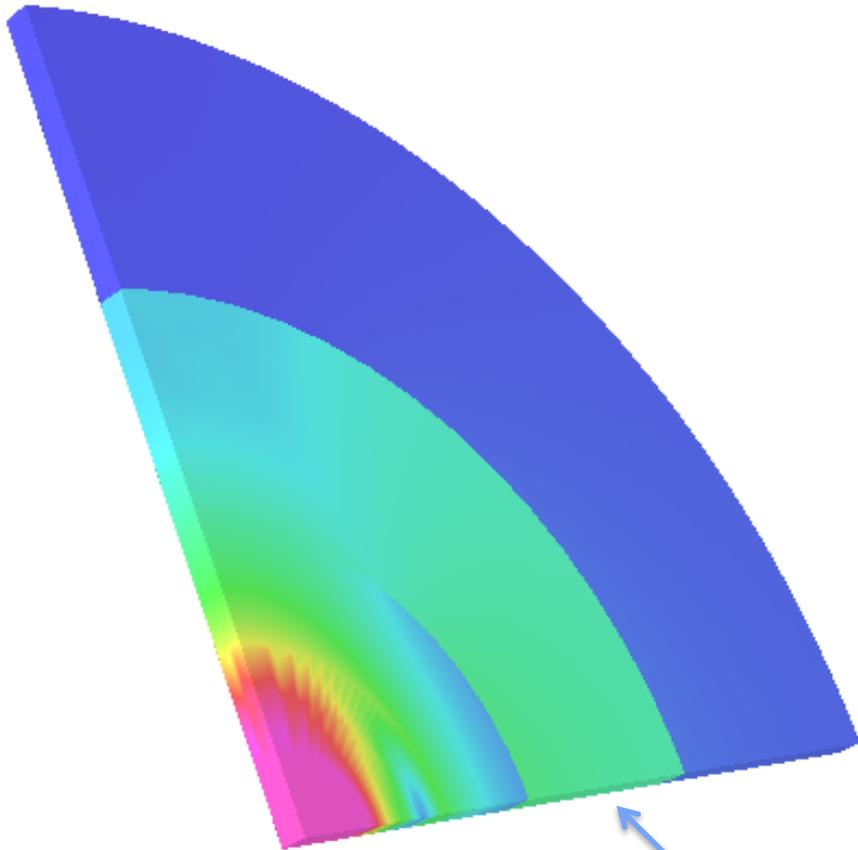
Courtesy S. Caspi, LBNL

# A complete turn is a Lamination

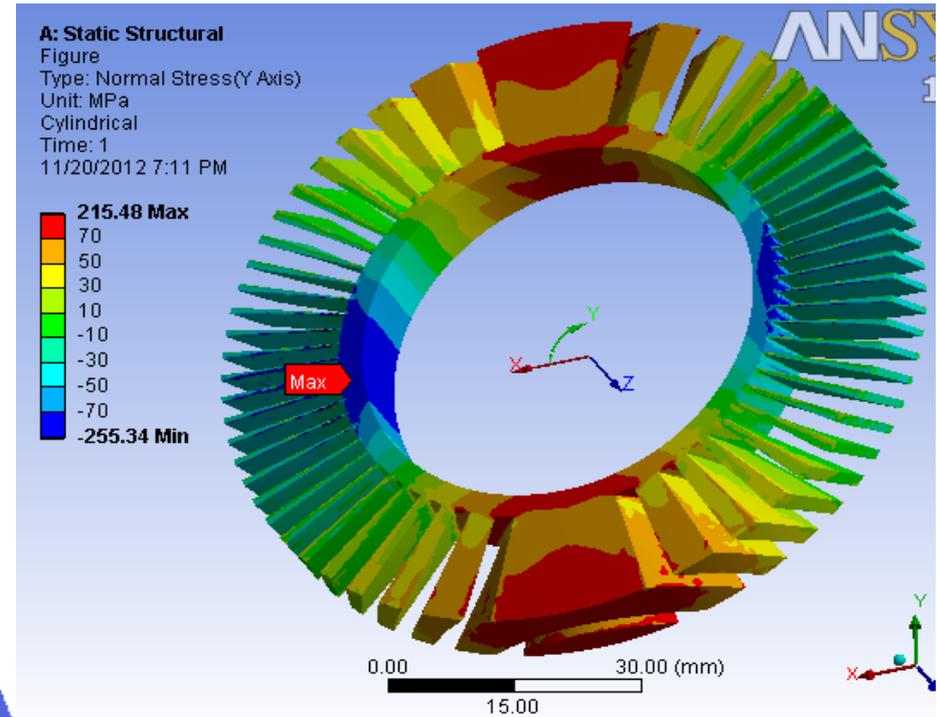


Courtesy S. Caspi, LBNL

# Simplify “2D” Analysis



Magnetic –  
TOSCA



Structural - ANSYS

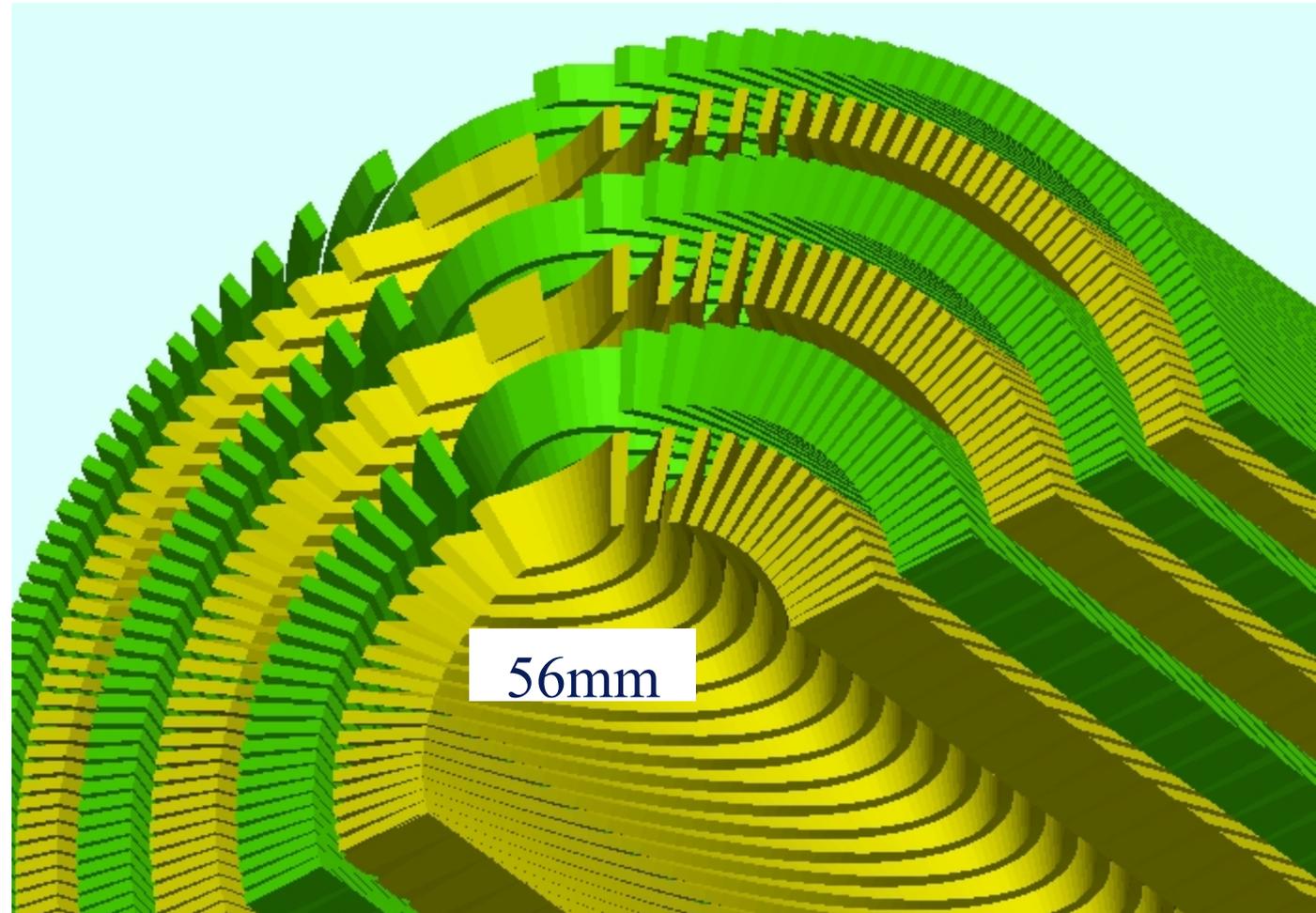
Courtesy S. Caspi, LBNL

# Example – 18T dipole with a 56mm bore



Layer 1, 30 strands  
Layer 2, 26 strands  
Layer 3, 22 strands  
Layer 4, 18 strands  
Layer 5, 14 strands  
Layer 6, 12 strands

- 6 layers, graded
- Conductor 60mm thick
- Current 10.5 kA
- 10.5 kA 18 T at 1.9K
- Intercepted stress



Courtesy S. Caspi, LBNL

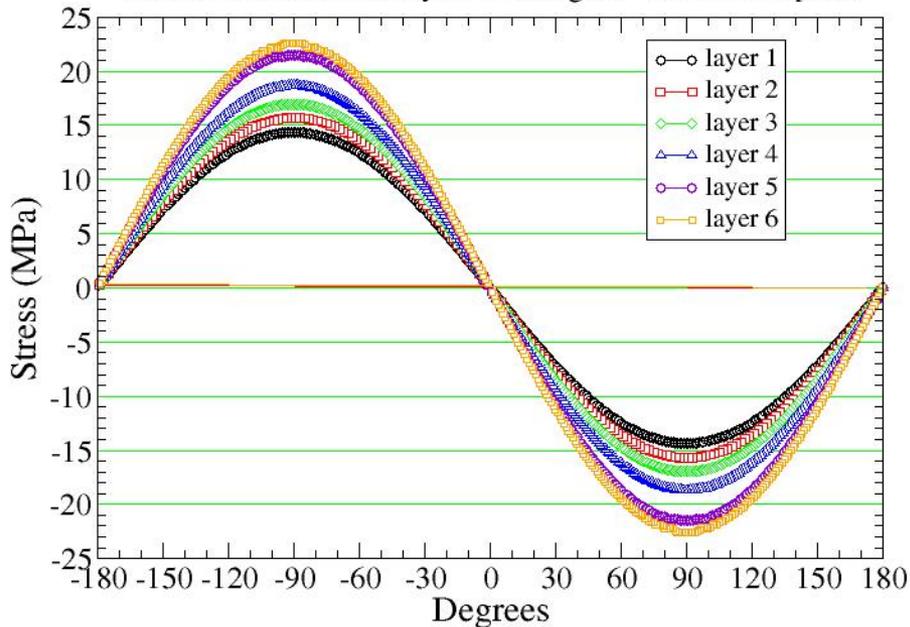
# Conductor Stress – with/without interception



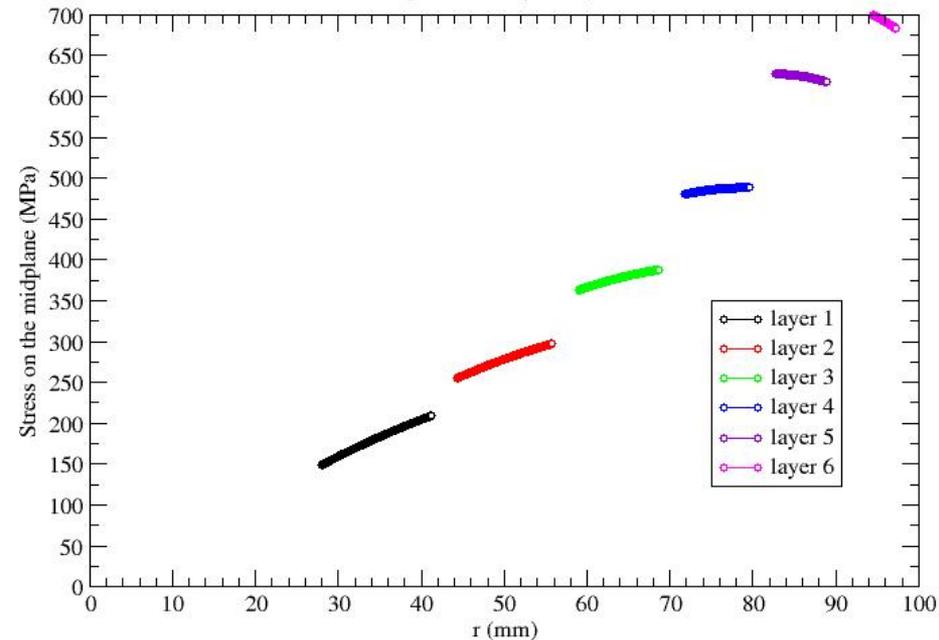
With stress interception the Lorentz stress in conductor  $< 25\text{MPa}$

Without stress interception the Lorentz mid-plane stress in conductor  $200\text{-}700\text{MPa}$

Normal Stress on ribs layers 1 through 6 - with interception



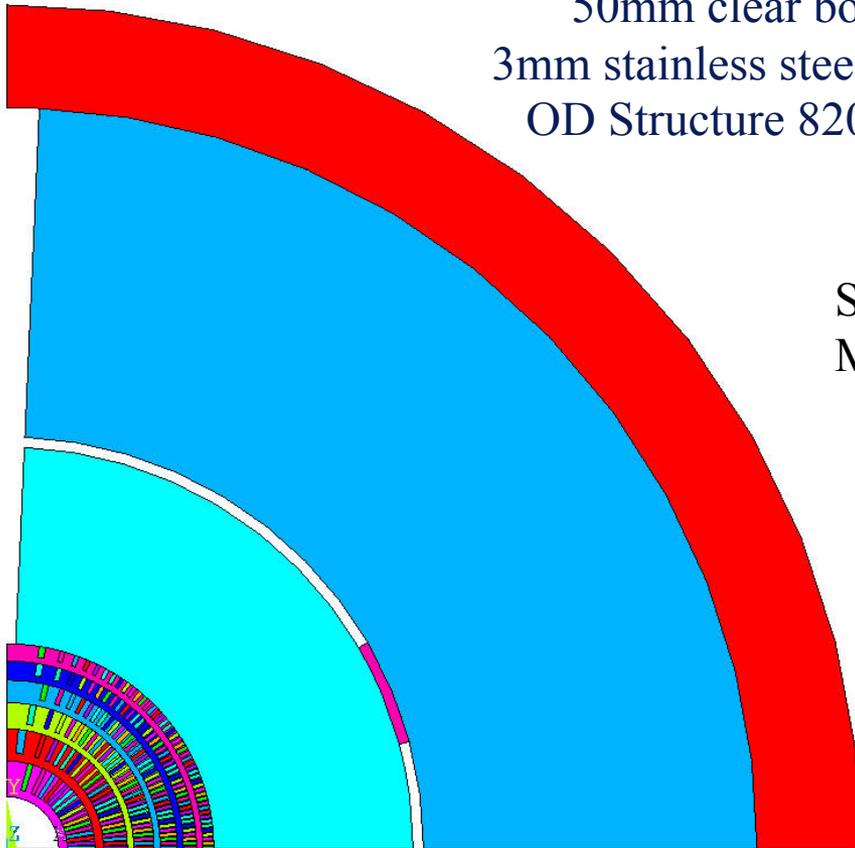
High Field 6 layers dipole



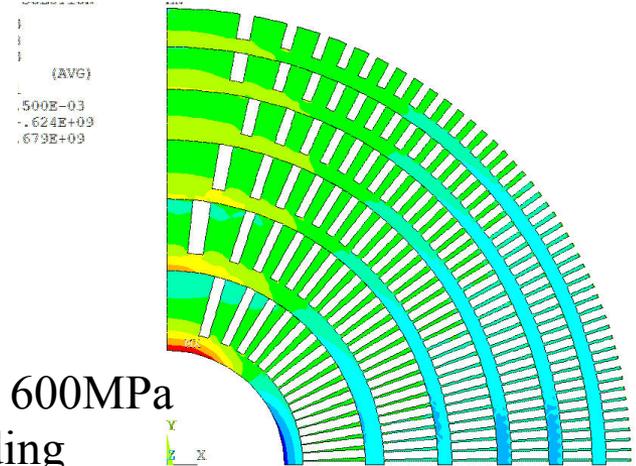
Courtesy S. Caspi, LBNL

# Structure - 2D ANSYS

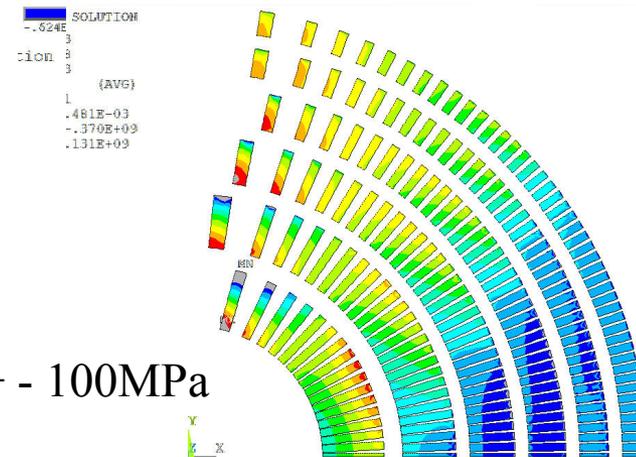
6 layers, graded 10.5kA, 19.4T  
50mm clear bore  
3mm stainless steel spars  
OD Structure 820mm



Spars at 20T + - 600MPa  
Mostly do to bending



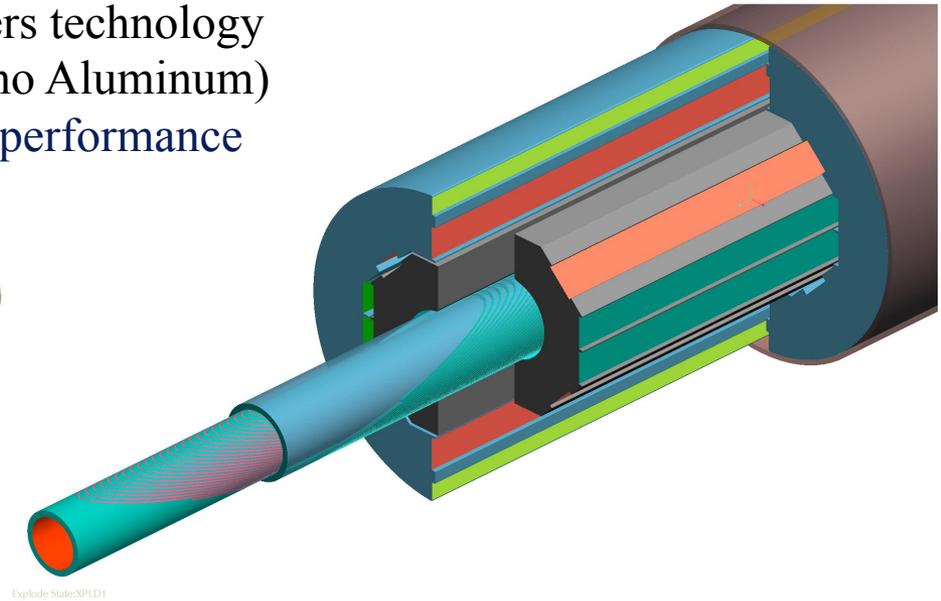
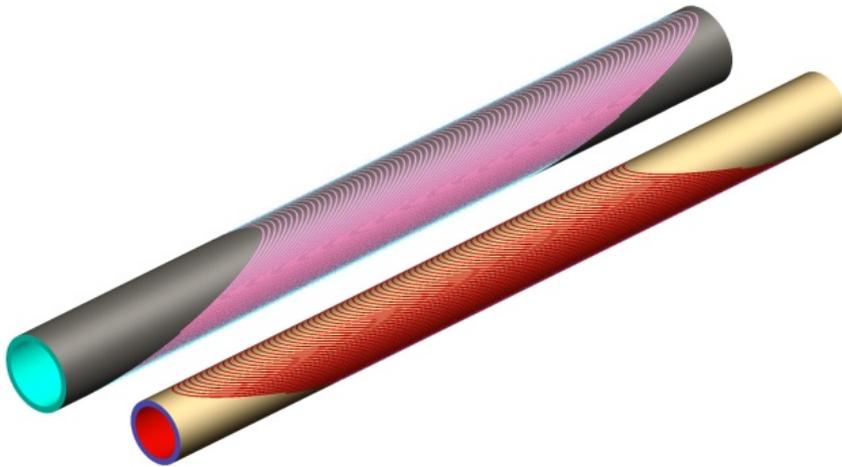
Turns at 20T + - 100MPa



Courtesy S. Caspi, LBNL

# Future Plans

1. Wind and test a 2 layer NbTi dipole – 50mm clear bore, 3T - CCT1
  - Pads and yoke using key and bladders technology
  - Stainless steel spars and outer shell (no Aluminum)
  - Evaluate manufacturing, test magnet performance



2. Wind and test a 2 layer Nb<sub>3</sub>Sn dipole – 50mm clear bore, 10T
3. Modular multi-layer Nb<sub>3</sub>Sn dipole - 50mm clear bore, 15T-20T
4. Explore a HTS insert >20T

Courtesy S. Caspi, LBNL

- Doubling the energy of the LHC is feasible
  - Another 10 years of R&D is required unless funding increases dramatically
    - Improve  $J_c$  of  $Nb_3Sn$  and reduce cost (scale-up)
    - Demonstrate viability of Canted Cosine-Theta concept or something equally acceptable
    - Quench protection
    - Need rad hard materials for impregnation
    - I'm not betting on HTS
- Machine issues are at least as challenging (but feasible)
  - Machine protection
  - Vacuum
  - Injection ( X2 in energy but same real estate)