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## **Physics 198, Spring Semester 1999 Introduction to Radiation Detectors and Electronics**

Problem Set 11: Due on Tuesday, 20-Apr-99 at begin of lecture. Discussion on Wednesday, 21-Apr-99 at 12 – 1 PM in 347 LeConte. Office hours: Mondays, 3 – 4 PM in 420 LeConte

- 1. Consider a spectroscopy system whose resolution is determined by electronic noise.
  - a) Find a quiet place and clearly recite 100 times "Noise contributions add in quadrature."
  - b) The current noise contribution is 120 eV and the voltage noise contribution is 160 eV. What is the total noise?

$$Q_n = \sqrt{Q_{ni}^2 + Q_{nv}^2} = \sqrt{120^2 + 160^2} = 200 \,\mathrm{eV}$$

c) After cooling the detector the current noise is 10 eV and the voltage noise remains unchanged at 160 eV. What is the total noise?

$$Q_n = \sqrt{Q_{ni}^2 + Q_{nv}^2} = \sqrt{10^2 + 160^2} = 160.3 \,\mathrm{eV}$$

i.e. in practice the current noise contribution is not discernible.

2. If the overall resolution of a system is determined by the convolution of multiple Gaussian distributions, the individual resolutions add in quadrature.

In a time-of-flight system the start detector has a time resolution of 100 ps and the stop detector has 50 ps resolution. What is the overall time resolution?

$$\Delta t = \sqrt{\Delta t_1^2 + \Delta t_1^2} = \sqrt{100^2 + 50^2} = 112 \text{ ps}$$

3. Calculate the properties of a simple transistor amplifier. A small-signal silicon transistor is used with a current gain of 100 with an Early voltage >100 V. The supply voltage  $V_+$  = 12 V.



a) The transistor is to operate at a collector current of 5 mA. What is the required value of the base bias resistor  $R_1$ ? (Assume  $V_{BE} = 0.6 \text{ V}$ )

To establish a collector current with a current gain of 50, the required base current is

$$I_B = \frac{I_C}{\beta_{DC}} = \frac{5 \cdot 10^{-3}}{100} = 50 \,\mu\text{A}$$

The only path for the base current is  $R_{\rm 1}.$  The voltage difference across  $R_{\rm 1}$  is  $V_+ - V_{BE},$  so

$$R_1 = \frac{V_+ - V_{BE}}{I_B} = \frac{12 - 0.6}{50 \cdot 10^{-6}} = 228 \,\mathrm{k}\Omega$$

b) What value of the collector resistor  $R_2$  is required to obtain 6 V at the collector?

The voltage drop across  $R_2$  is  $V_+$  -  $V_C$  with a current flow if  $I_C$ , so

$$R_2 = \frac{V_+ - V_C}{I_C} = \frac{12 - 6}{5 \cdot 10^{-3}} = 1.2 \text{ k}\Omega$$

c) The output of the amplifier is measured using a high-impedance probe, so the load resistor  $R_L=1 M\Omega$ . If the coupling capacitances  $C_1$  and  $C_3$  are sufficiently large to be irrelevant at the measurement frequency (and neglecting  $C_2$ ), what is the voltage gain for a sinusoidal input?

The output resistance of the transistor and the resistances  $R_L$  and  $R_2$  are in parallel for AC, so the effective load resistance

$$\frac{1}{R_{L,eff}} = \frac{1}{R_0} + \frac{1}{R_2} + \frac{1}{R_L}$$

Since the Early voltage > 100 V,  $R_0 = V_A/I_C > 100/0.005 = 20 \text{ k}\Omega$ . Since both  $R_0$  and  $R_L >> R_2$ , the effective load resistance is about equal to  $R_2$  and the voltage gain

$$A_V = g_m R_2$$

The transconductance of a bipolar transistor

$$g_m = \frac{q_e}{k_B T} I_C$$

so, using  $k_B T/q_e = 26 \text{ mV} (T = 300 \text{ K})$ 

$$A_V = g_m R_2 = \frac{q_e}{k_B T} I_C R_2 = \frac{1}{0.026} \cdot (5 \cdot 10^{-3}) \cdot 1200 \approx 230$$

d) What is the small signal input resistance measured at the base of the transistor?

As derived in the lecture, the input resistance of the transistor

$$R_i = \frac{k_B T}{q_e} \cdot \frac{\beta}{I_C} = 0.026 \cdot \frac{100}{5 \cdot 10^{-3}} = 520$$

The base bias resistor  $R_1$  is effectively in parallel with  $R_i$ , but since  $R_1 >> R_i$ , the effective input resistance is  $R_i$ .

e) The lower cut-off frequency of the amplifier is to be 160 kHz. What is the required value of C<sub>1</sub>? Assume that the signal source has zero source resistance.

C<sub>1</sub> together with the input resistance R<sub>i</sub> form a low-pass filter with the time constant

$$\tau = R_i C_1 = \frac{1}{2\pi f_L}$$

so

$$C_1 = \frac{1}{2\pi f_L R_i} = \frac{1}{2\pi \cdot (160 \cdot 10^3) \cdot 520} = 1.9 \text{ nF}$$

e) The capacitance to ground at the output of the amplifier  $C_2$  is 133 pF. What is the upper cutoff frequency?

The effective load resistance  $R_2$  in parallel with the shunt capacitance  $C_2$  when driven by a current source (the transistor) forms an integrator (low-pass filter) with the time constant

$$\tau = R_2 C_2 = \frac{1}{2\pi f_U}$$

and

$$f_U = \frac{1}{2\pi R_2 C_2} = \frac{1}{2\pi \cdot 1200 \cdot (133 \cdot 10^{-12})} = 997 \text{ kHz}$$

f) If the signal source provides a step impulse, what is the pulse shape at the output? (Assume that  $C_3$  is sufficiently large to be negligible.)

The capacitive coupling at the input forms a differentiator with the time constant

$$\tau_d = R_i C_1 = \frac{1}{2\pi f_L} = 1 \,\mu s$$

At the output the parallel combination of  $R_2$  and  $C_2$  forms an integrator with the time constant

$$\tau_i = R_2 C_2 = 160 \,\mathrm{ns}$$

so the output pulse shape (for a negative input step, since the amplifier inverts)



i.e. the amplifier is a simple CR-RC shaper. The peak signal will be inverted and 160 times larger than the input (voltage gain from c) times 0.7 shaper attenuation).